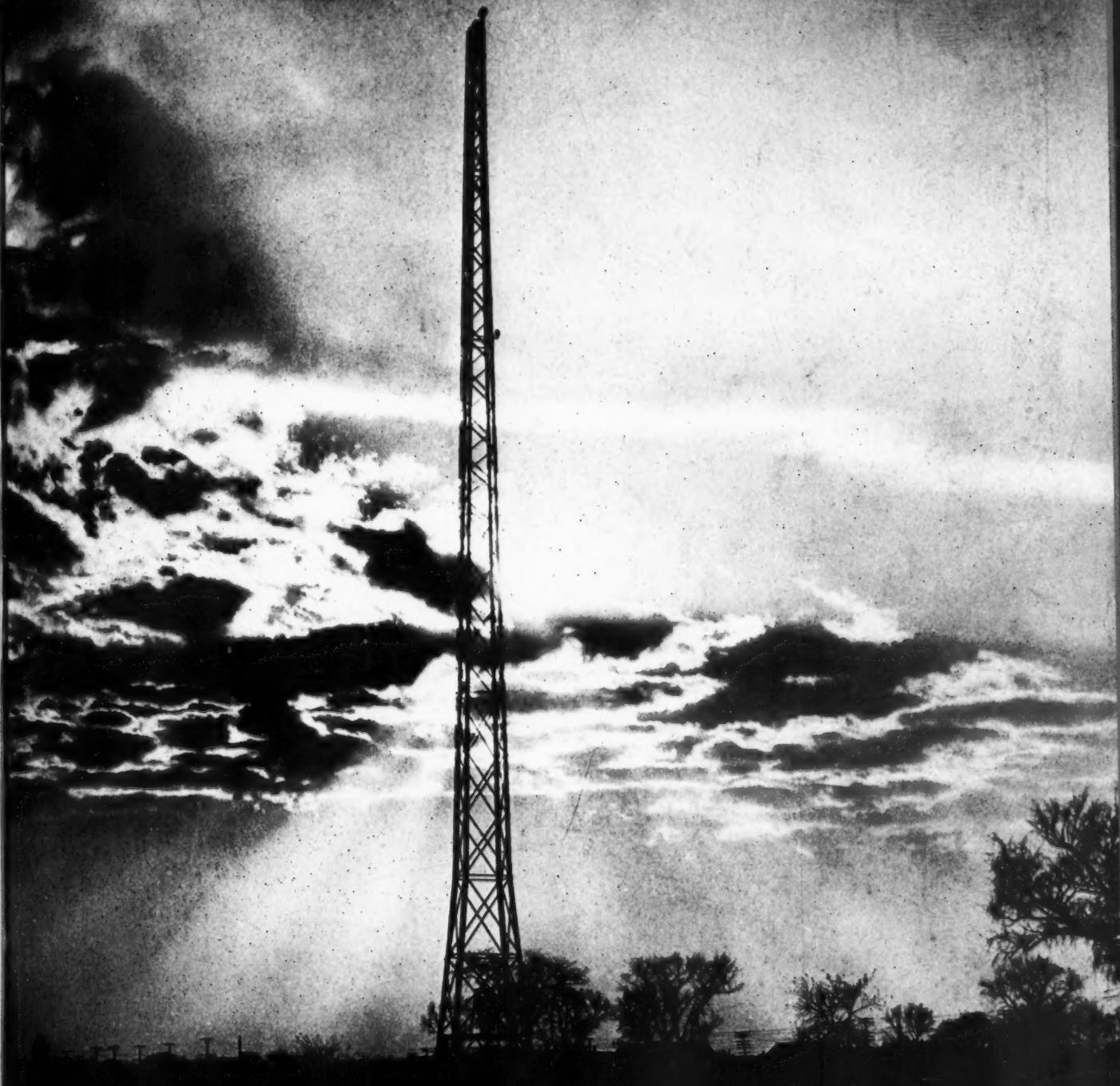


# RADIO

JULY, 1945

WITH  
FREQUENCY ALLOCATION  
CHART

Design • Production • Operation



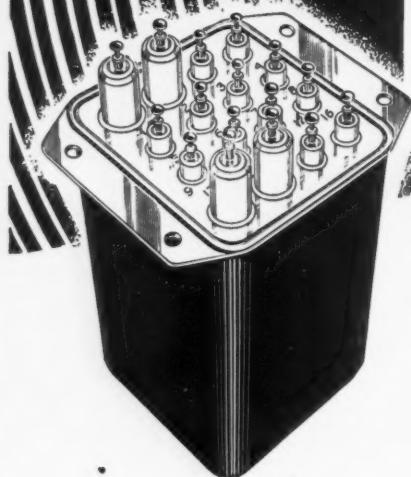
K  
in  
et  
y.

N

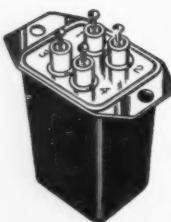
The Journal for Radio & Electronic Engineers

# KYLE TRANSFORMERS

# KY



Engineered to take  
advantage of latest  
trends in radio design



New products, new ways of doing things will require transformers engineered to take advantage of the latest trends in electronic equipment design and manufacture... Kyle Transformers built to meet exact specifications. ¶ Kyle engineers have constantly met and solved ever changing problems involving application of transformers to the wartime fields of radio communication, radar detection and electronic controls. ¶ Kyle Transformers are hermetically sealed to function perfectly under conditions they are designed to meet... whether for use in cold, temperate, or tropical climates. ¶ This alert, young-thinking organization is at power distribution equipment. Kyle engineering, manufacturing, and plant facilities are top notch. It will pay you to send your transformer specifications to Kyle.

K Y L E  C O R P O R A T I O N

SOUTH MILWAUKEE, WISCONSIN

# New! L-A-R-G-E-R Size Sheets of

**MYKROY**

PERFECTED MICA CERAMIC INSULATION

**Make Possible Many  
Additional Uses for this  
Superior Insulation**

### Now You Can Use MYKROY For:

- Large Terminal Boards
- Switch Board Panels
- Large Inductance Bars and Strain Insulators up to 29 inches long
- Switch Connecting Rods
- Transformer Covers
- Large Meter Panels
- Bases for Radio Frequency and Electrical Equipment assemblies requiring large one-piece sheets

HERETOFORE the largest sheet of glass-bonded mica insulation available measured 14½" x 19¼". By doubling the size, Electronic Mechanics, exclusive manufacturers of Mykroy, now afford Design and Production Engineers many important, new application and fabricating advantages.

Lower Cost per square inch affects savings as high as 33% depending upon work piece size, greatly reducing the cost per fabricated part. Better Cutting efficiency lowers cost still further extending the use of Mykroy to a longer list of electronic applications where formerly cost prohibited its use.

Get the full facts about this versatile dielectric now. Ask for a copy of the new MYKROY BULLETIN 102 which describes the new, larger 19¼" x 29¾" sheets.

MADE EXCLUSIVELY BY

**ELECTRONIC  
MECHANICS  
INC.**

70 CLIFTON BLVD., CLIFTON, N. J.

CHICAGO 47; 1917 N. Springfield Ave., Tel. Albany 4310  
EXPORT OFFICE: 89 Broad Street, New York 4, New York

MYKROY IS SUPPLIED IN SHEETS AND RODS — MACHINED OR MOLDED TO SPECIFICATIONS

19½  
x  
29¾



Supplied in thicknesses ranging from  $\frac{1}{8}$ " —  $1\frac{1}{4}$ "



### MECHANICAL PROPERTIES\*

MODULUS OF RUPTURE.....18000-21000psi

#### HARDNESS

Mohs Scale 3-4 BHN, BHN 500 K9 Load, 63-74

IMPACT STRENGTH.....ASTM Charpy .34-.41 ft. lbs.

COMPRESSION STRENGTH.....42000 psi

SPECIFIC GRAVITY.....2.75-3.8

THERMAL EXPANSION.....000006 per Degree Fahr.

APPEARANCE.....Brownish Grey to Light Tan

### ELECTRICAL PROPERTIES\*

DIELECTRIC CONSTANT.....6.5-7

DIELECTRIC STRENGTH ( $\frac{1}{8}$ ").....630 Volts per Mil

POWER FACTOR......001-.002 (Meets AWS L-4)

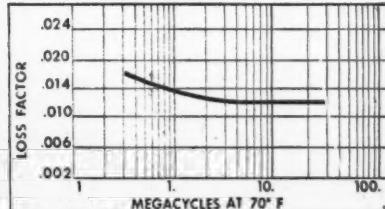
### \*THESE VALUES COVER THE VARIOUS GRADES OF MYKROY

GRADE 8 Best for low loss requirements.

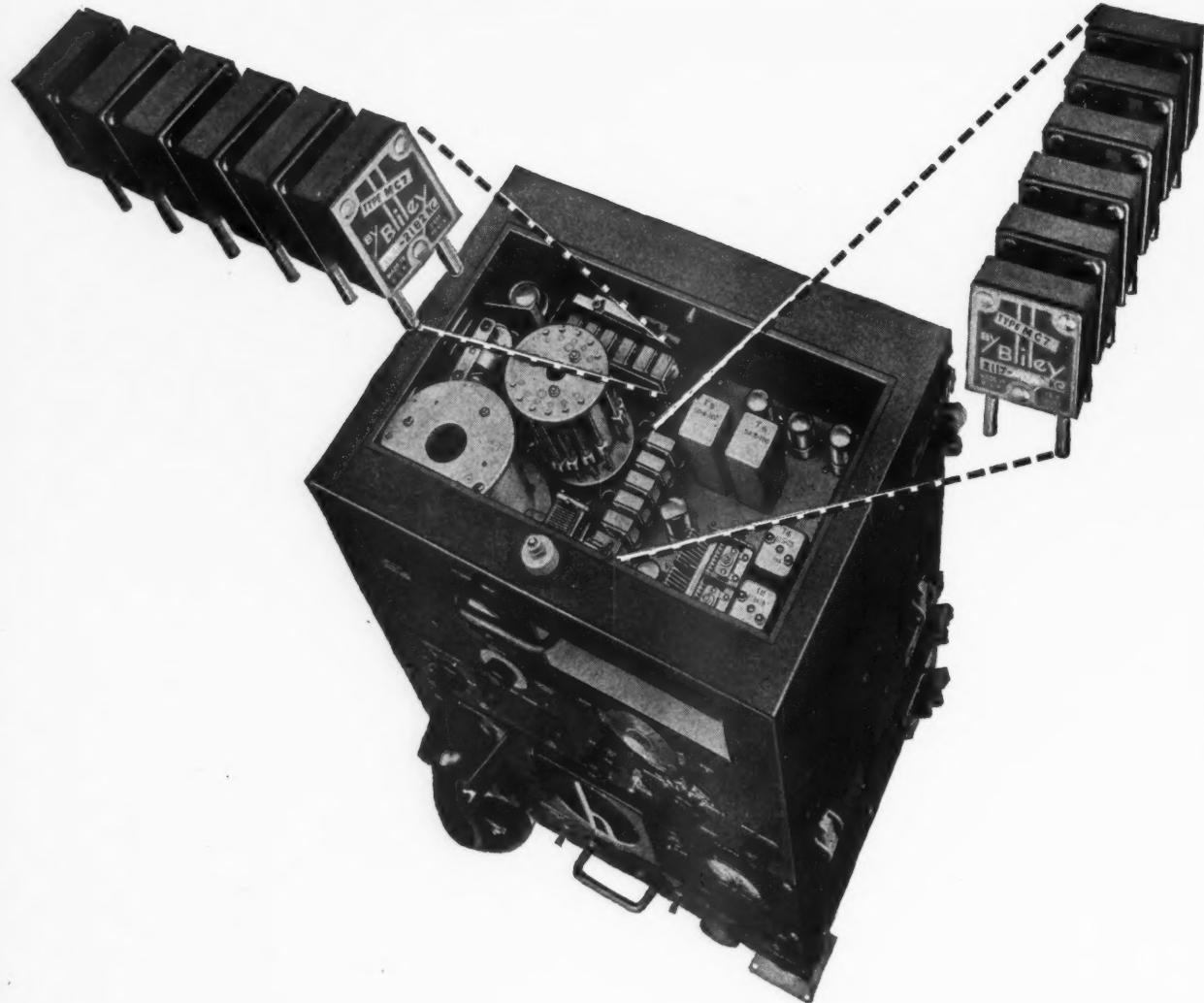
GRADE 36 Best for low loss combined with high mechanical strength.

GRADE 51 Best for molding applications.

Special formulas compounded for special requirements.



Based on Power Factor Measurements made by Boonton Radio Corp. on standard Mykroy stock.



## The 6 operating frequencies are BLILEY CRYSTAL-controlled

For dependable communications on the high seas here is a battle-tested set incorporating every modern feature that experience has shown to be most desirable for ship-to-shore and ship-to-ship radiotelephone service.

The six Bliley crystal-controlled operating frequencies permit instant and positive channel selection

in both transmitter and receiver. The Bliley *acid etched\** Crystals used in this Hallicrafters HT-14 set were designed to meet specific objectives in the operation of two-way radiotelephone communications. They, too, have been battle-tested.

It's a habit with most communications engineers to specify Bliley for all crystal requirements. This is par-

ticularly true today when new applications and complex designs require technical excellence in every component. There is no substitute for the 15 years of experience offered by Bliley craftsmen and engineers.

+ + +

\*Acid etching quartz crystals to frequency is a patented Bliley process.



Do more than before ...

buy extra War Bonds

BLILEY ELECTRIC COMPANY  
UNION STATION BUILDING • ERIE, PENN.

# RADIO

Published by RADIO MAGAZINES, INC.

John H. Potts.....Editor  
Sanford R. Cowan.....Publisher

JULY 1945

Vol. 29, No. 7

## CONTENTS

### COVER

Radio range tower (CAA photograph)

### ARTICLES

An Audio-Carrier-Frequency R-C Oscillator—Robert C. Paine ..	33
<i>This resistance-capacity oscillator covers a range from 20 to 200,000 kc and has many unusual features</i>	
The Application of Metals in Radio Receiver Design—A. C. Matthews ..	36
<i>Practical data for radio engineers on a subject with which many are unfamiliar</i>	
FCC Report on FM .....	41
<i>The Federal Communications Commission presents their case for assigning higher frequencies for FM</i>	
Frequency Allocation Chart .....	43
<i>A complete chart of final frequency allocations from 25 to above 30,000 mc</i>	
A Circuit for Phase Modulation—Bernard Grob .....	45
<i>This article describes a new method of phase modulation which has proved successful in a commercial FM transmitter</i>	
A CRL Impedance Bridge—Athanasios Cosmas .....	47
<i>Complete data on a laboratory bridge which is direct-reading</i>	
Radio Design Worksheet, No. 38: Image Suppression; Considerations Involved in the Choice of Intermediate Frequencies ..	50
Radio Bibliography: 18—Velocity Modulation, Part 2—F. X. Rettemeyer .....	52

### MISCELLANEOUS

Transients .....	6
TECHNICANA	
Spectrum Analysis .....	25
Ink Recorder Amplifier .....	26
Capacitors for Series Heaters .....	30
This Month .....	54
New Products .....	57
Advertising Index .....	75

John H. Potts.....President  
Sanford R. Cowan.....Sec'y-Treas.  
Charles H. Farrell.....Adv. Manager  
Elaine Wilson.....Adv. Production  
Miriam Birnbaum.....Circ'l. Manager

#### PACIFIC COAST REPRESENTATIVE

H. W. Dickow  
1387 40th Ave., San Francisco 22, Calif.

#### GREAT BRITAIN REPRESENTATIVE

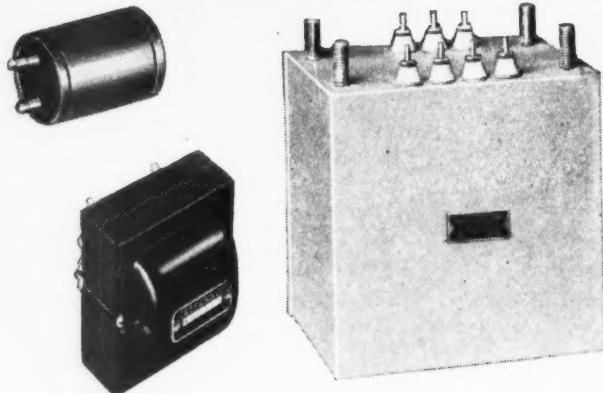
Radio Society of Great Britain,  
New Ruskin House, Little Russell St.,  
London, W.C. 1, England

# AIDING THE WAR TODAY . . . . .



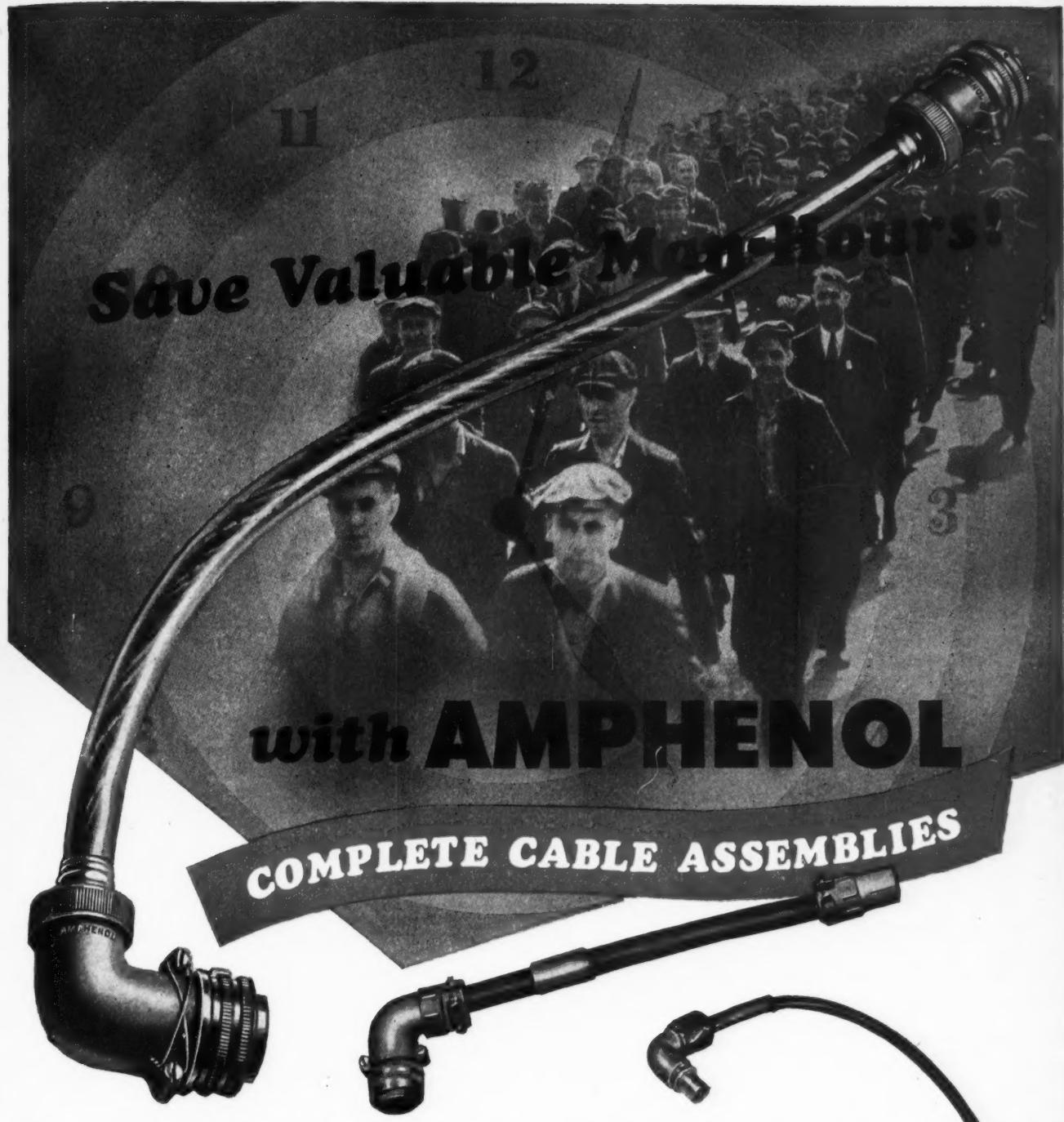
## .... SERVING THE PEACE TOMORROW

Tomorrow, when the tools of strife are turned to the ways of peace, Jefferson Transformers will serve with the same fidelity. Improved manufacturing techniques established under the stress of war will be turned to producing still better transformers for your post war needs. Let Jefferson engineers examine your particular requirements now and make suggestions that will save you time later . . . JEFFERSON ELECTRIC COMPANY, Bellwood (Suburb of Chicago), Illinois. *In Canada:* Canadian Jefferson Electric Co. Ltd., 384 Pape Avenue, Toronto, Ont.



In all theatres of war, on the invasion beaches, wherever allied forces march against aggression, Jefferson Electric Transformers establish records of dependable performance. Today—on radio, radar, "walkie-talkies," television communications systems, electronic and control applications,—Jefferson Transformers aid our war effort with a long-life reliability based on engineering skill and Jefferson's basic principle of "quality—with quantity" production.

JEFFERSON  
ELECTRIC



With Amphenol COMPLETE Cable Assemblies you have only one source of supply . . . issue only one purchase order . . . cut your procurement cost . . . reduce your labor and tool cost . . . eliminate production and assembly worries . . . all of these add up to a substantial savings in valuable man-hours and manufacturing cost.

Tremendous volume production has necessitated the creation of countless jigs, fixtures and special equipment with resultant lower assembly cost, pre-

cision and quality workmanship, and dependability that characterizes all Amphenol products.

. . . Engineered to your specifications . . . Efficiently assembled . . . Exacting precision in testing—three additional reasons why you should specify Amphenol complete, quality Cable Assemblies.

Your inquiry will receive prompt, careful and confidential consideration.

Depend upon AMPHENOL Quality.



AMERICAN PHENOLIC CORPORATION

Chicago 50, Illinois

In Canada • Amphenol Limited • Toronto

U.H.F. Cables and Connectors • Conduit • Fittings • Connectors (A-N,  
U.H.F., British) • Cable Assemblies • Radio Parts • Plastics for Industry

# Transients

## PATENT LICENSING

The announcement that RCA has arranged to continue licensing Philips U. S. patents clears up a potential threat to prompt resumption of civilian radio communications apparatus manufacturing. Under the previously announced arrangement, it would have been necessary for most radio manufacturers to take out new licenses from the Philips organization, thus complicating the patent setup, as was pointed out in our editorial in the May issue.

It is stated that RCA has informed its licensees that it is extending to them rights under the Philips' patents at no extra charge.

## A. T. & T. MOBILE RADIOTELEPHONE SERVICE

Expansion of the Bell Telephone System to include drivers of automobiles, trucks and other mobile units in a general mobile radiotelephone service is indicated, according to an announcement just issued by the American Telephone and Telegraph Company.

Applications have been filed with the Federal Communications Commission for authority to install radiotelephone stations in the following cities: Baltimore, Chicago, Cincinnati, Columbus, Denver, Houston, Milwaukee, New York, Philadelphia, Pittsburgh, St. Louis, Salt Lake City, and Washington, D. C. In addition, surveys are being undertaken to find out if this service is feasible and needed in many other cities.

The plan is to use transmitters of about 250 watts in metropolitan centers. The mobile units will have a power rating of about 15 watts. The assigned frequency range for urban mobile service is 152 to 162 mc.

Another type of mobile radiotelephone service which will be tried would furnish two-way voice communication to motor vehicles operating on intercity highways and to boats on adjacent waterways. This service would require transmitting and receiving stations along the highways to be served.

Inauguration of this service will tend to limit to some extent the field of application of the Citizens Radiocommunication Service, but there will still be plenty of potential customers for the latter type of service. And it promises to open a new field for radio engineers which will absorb a large number of trained personnel and thus benefit the industry as a whole.

## FCC FREQUENCY ALLOCATIONS

Now that the Federal Communications Commission has completed its frequency allocations for FM and other services in the 44 to 108 mc range, those factors in the radio industry which opposed moving FM to higher frequencies seem disposed to accept the allocations with good grace. The complete FCC report on which the action was based is published in this issue, and it must be admitted that they present a good case. With this matter definitely settled, it would be well if the radio industry should concentrate on other problems, such as component and tube allocations, pricing, etc., which are the only remaining obstacles to reconversion among those manufacturers not operating at capacity on war orders.

## THE RADIO INDUSTRY AND BRETON WOODS

According to a recent report issued by the Business and Industry Committee for Bretton Woods, many of the Latin American countries are now ripe for the development of their radio markets. The Department of Commerce recently made a study of conditions in Argentina and reported very favorably on its potential consumption of radio equipment and components from the United States. The industrial development which will be undertaken by these countries and the reconstruction projects of Europe and Asia will also create important markets.

The International Fund and Bank will assist radio manufacturers to expand their markets. It will help foreign countries to buy electronics equipment and will stabilize foreign exchange, previously one of the greatest impediments to expansion of our foreign markets.

Many American manufacturers in the radio/electronic field already realize the potentialities of foreign markets and plan to produce for export even before models for domestic consumption are made available.

For radio engineers, it would be a good idea to develop greater familiarity with the technical requirements of apparatus designed for export. Often these are far more exacting than for domestic apparatus, particularly in regions where line voltages vary widely and in tropical climates. Experience in production of apparatus for war use will help greatly in reducing the cost of production of apparatus for export. —J.H.P.

# SYLVANIA NEWS

## ELECTRONIC EQUIPMENT EDITION

JULY

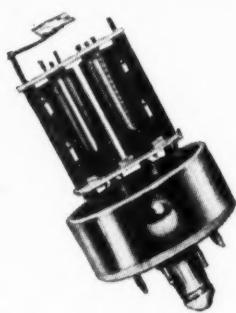
Published by SYLVANIA ELECTRIC PRODUCTS INC., Emporium, Pa.

1945

### NEW TUBE HAS SEPARATE CATHODES

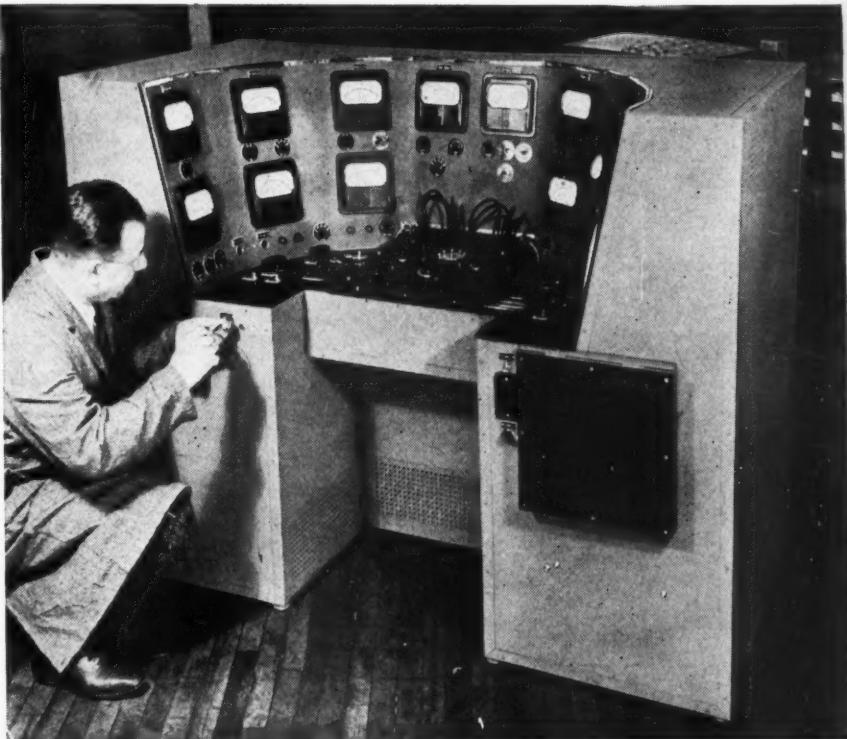
#### *Construction Permits Use As A Discriminator*

Sylvania Type 7K7 is a duo-diode high-mu triode differing from the usual diode-triode by having two separate cathodes, one for the triode and the other for the diodes.



This difference permits the tube to be used as a discriminator.

The cut-away view shows that although the construction looks like a duo-triode the second plate is really a shield around the two diodes.



### SYLVANIA RADIO TUBE BRIDGE SET INSURES PERFECT PERFORMANCE

#### *Measures Static And Dynamic Characteristics Of Vacuum Tubes*

As ultra-high frequencies and a very wide range of intricate electronic applications make strict demands on tube performance and circuit designs, an accurate testing of tube and circuit characteristics becomes of the greatest importance.

One of Sylvania Electric's latest essential radio vacuum tube bridge test sets for precision engineering data is pictured above. Manufactured at Sylvania's plant at Williamsport, Pa., this equip-

ment measures static and dynamic qualities of radio tubes, such as plate current, filament voltage and current, screen current, gas current, plate resistance, power output, mutual conductance, and amplification factor, as well as the characteristics of electronic devices.

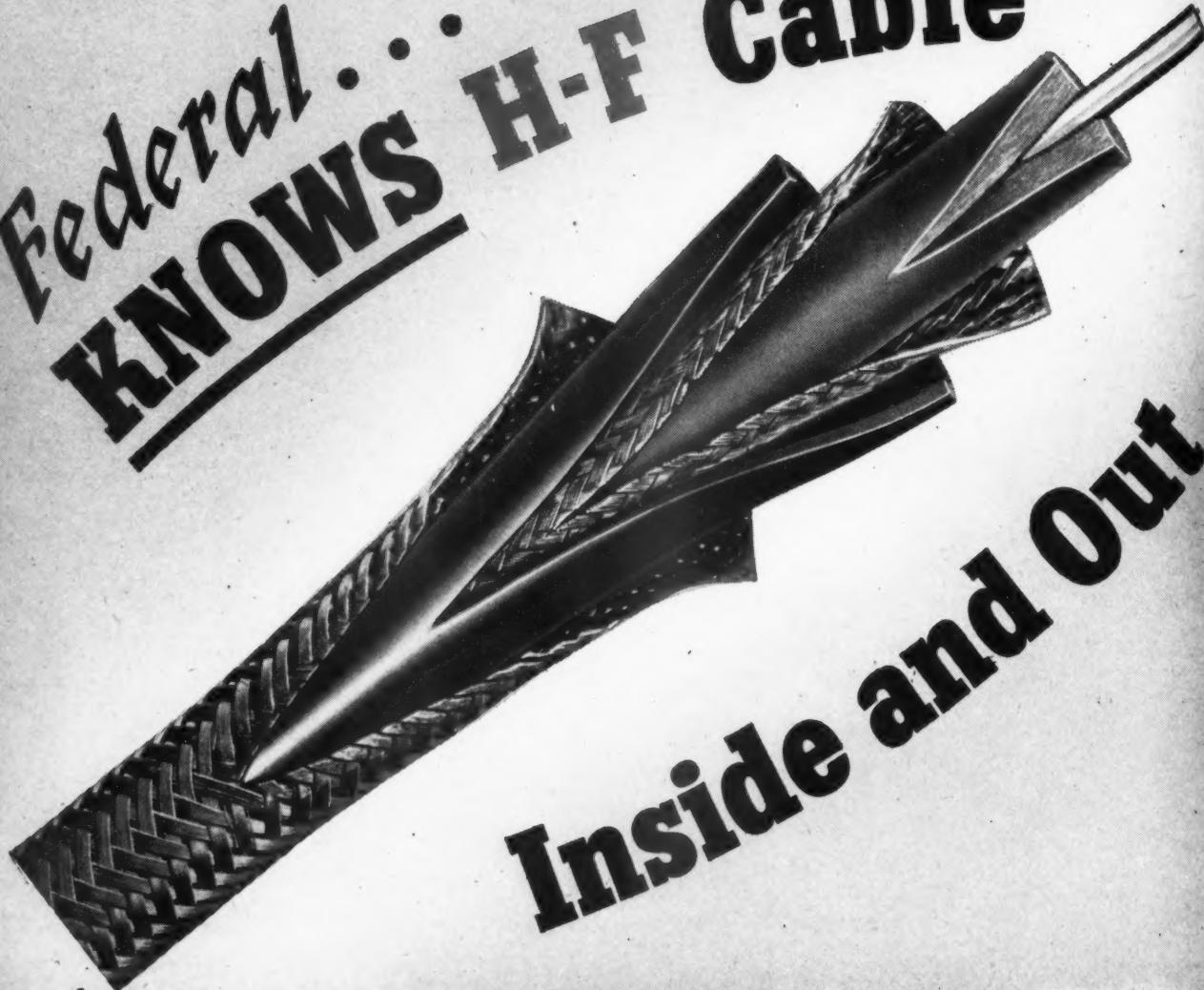
The set is compact, fully shielded, with well-filtered, self-contained power supplies, complete with voltage regulators except AC and DC filament voltages.

# SYLVANIA ELECTRIC

*Emporium, Pa.*

MAKERS OF RADIO TUBES; CATHODE RAY TUBES; ELECTRONIC DEVICES; FLUORESCENT LAMPS, FIXTURES, ACCESSORIES; ELECTRIC LIGHT BULBS

*Federal . . .*  
**KNOWS H-F Cable**



**Inside and Out**

From inner conductor to outer covering . . . Federal really knows high-frequency transmission lines.

And this knowledge was not easily won. As the pioneer in the field Federal not only developed over 80% of all h-f cable types in use today . . . but developed most of the equipment needed to test them.

Attenuation, high-voltage, dielectric and balance testing equipment, velocity of propagation, braid-resistance and elec-

cal length meters . . . were all Federal-engineered to fit specific requirements.

That's why it's logical to turn to the acknowledged leader in the field for the finest in h-f cables, specialty-engineered harnesses and cable assemblies.

Where requirements are critical . . . for transmission lines with special characteristics...for custom-built and engineered harnesses and cable assemblies . . . take your high-frequency transmission problems to Federal.



*Federal Telephone and Radio Corporation*



Newark 1, N. J.

# New Formica Grades



RESIST MORE  
HEAT!

PROGRESS has recently provided new resins and new fibre bases that have greatly increased the heat resistance of insulating grades of Formica. They will take without injury about 25 percent higher temperatures.

An example of this improvement is FF-1, produced to conform to Navy Grade GM-1, made with a glass fibre base and melamine resins. It withstands 440 degrees Fahrenheit for a short period, and 390 degrees continuously.

In this same material Arc resistance reaches a new level — by ASTM test D495-42, it is rated at 185 seconds.

The material is strong, and can, therefore, be used to take structural stresses when the design makes that desirable. Test figures: Tensile strength 25,000 P.S.I.; Compressive strength (flatwise) 90,000 p.s.i.; Flexural Strength (flatwise) 30,000 p.s.i.; Modulus of Elasticity in bending 3,000,000 p.s.i.; Izod impact, 12 ft. lbs. per inch of notch.

This is a new combination of useful qualities, not previously available in one material. Unlike some materials which possess some of these characteristics, the material can be easily punched and machined. It is suitable for rapid fabrication by production methods.

THE FORMICA INSULATION COMPANY, 4670 SPRING GROVE AVENUE, CINTI. 32, O.

# GIRDER CONSTRUCTION . . .



Notice how girder construction gives rigidity to the famous P-61 Black Widow Night Fighter. Structural view courtesy of Northrop Aviation, Inc.

## gives greater strength to *Gammatron Tubes*

The same type of construction which gives strength and rigidity to a modern airplane, skyscraper, or bridge has been successfully incorporated into the design of the HK-854 and HK-1054 triodes. Compare the girder construction of the P-61 with the plate and grid supports of the HK-1054—the structural principles are identical! Note particularly how the heavy tripod plate support is welded to large diameter tubing, which in turn is firmly secured to the copper plate cup.

Because of their girder construction, HK-854 and HK-1054 Gammatrons stand up exceptionally well even when subjected to the vibration and stresses which usually accompany their use in such industrial applications as dielectric heating.

This superior internal strength is important since it prevents internal shorts, and variations in the characteristics of the tubes due to movement of the elements.

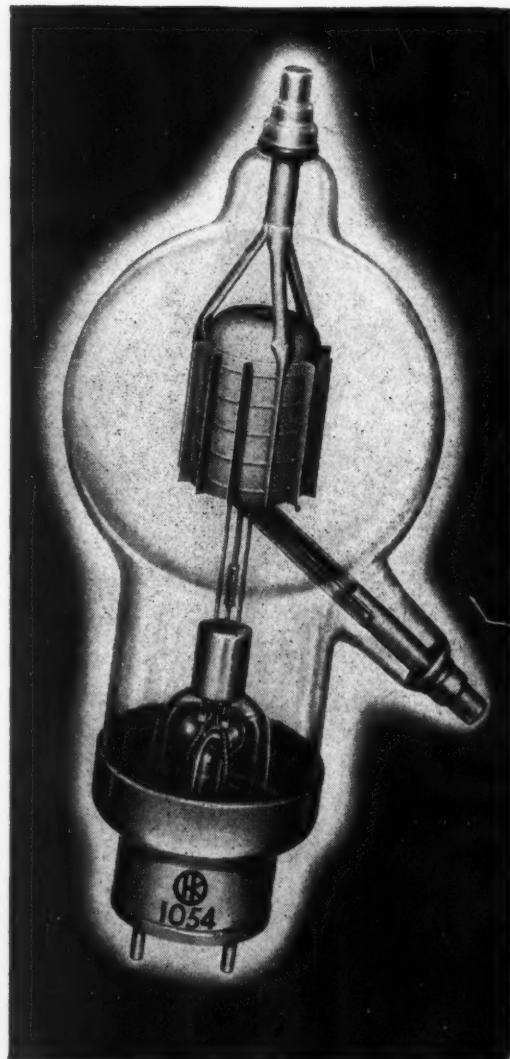
### NEW LOW PRICES NOW IN EFFECT

TUBE TYPE	NEW LIST PRICE
HK 854-H (High amplification factor) . . .	Now only \$60.00
HK 854-L (Low amplification factor) . . .	Now only 60.00
HK 1054-L (Low amplification factor) . . .	Now only 135.00

KEEP BUYING  WAR BONDS

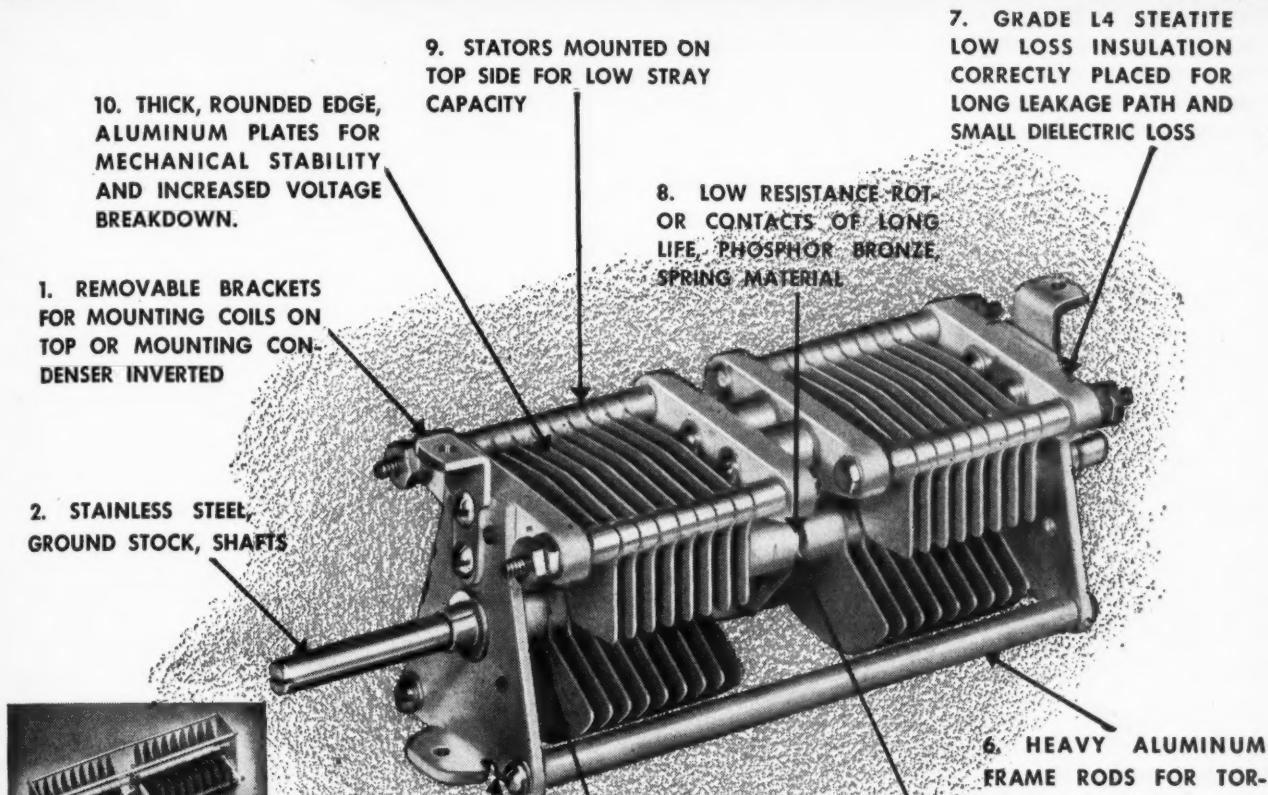
**HEINTZ AND KAUFMAN LTD.**  
SOUTH SAN FRANCISCO · CALIFORNIA

EXPORT AGENTS: M. SIMONS & SON,  
25 WARREN STREET, NEW YORK CITY, U. S. A.

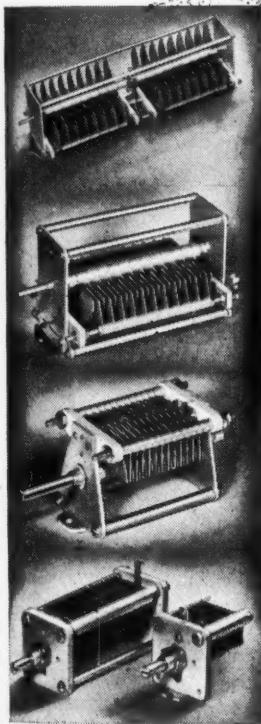


# 10

## POINTS OF *Superiority*



CATALOG NO. 100FD20



C - Plate spacing	.125" - .500"
Maximum frame dimensions	5½" x 5-13 32"
D - Plate spacing	.080" - .250"
Maximum frame dimensions	4½" x 4"
E - Plate spacing	.045" - .125"
Maximum frame dimensions	2½" x 2-19 32"
H - Plate spacing	.030" & .080"
Maximum frame dimensions	1½" & 1-9 16"

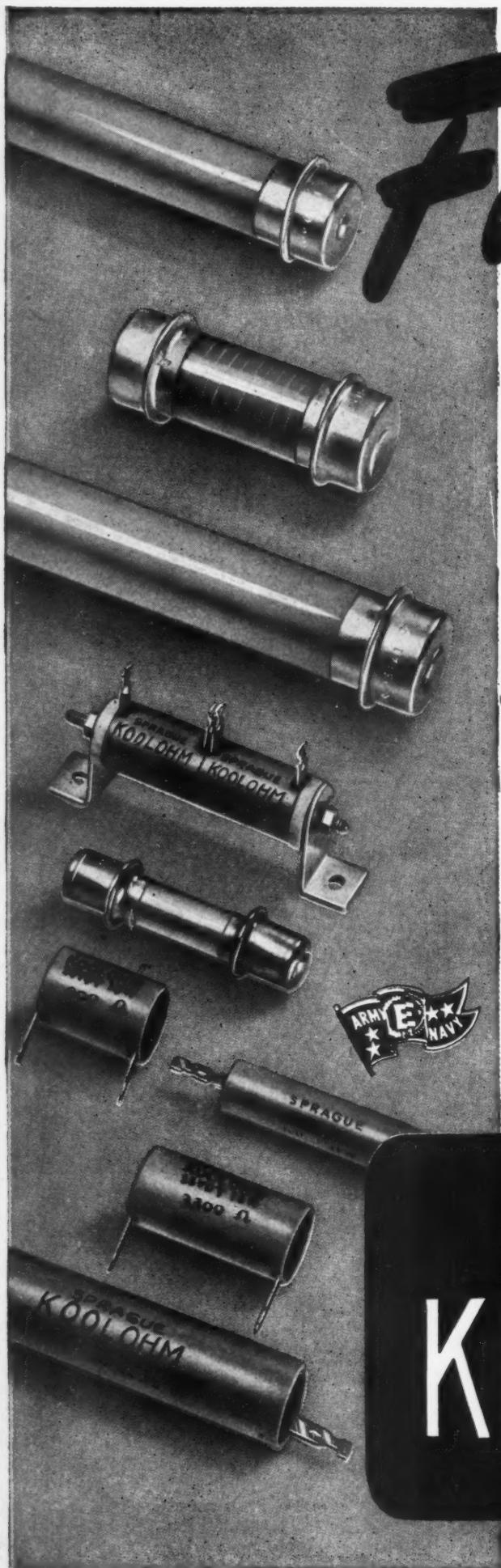
Type "E" single and dual condensers are stocked with plate spacings of .045 to .075" in 19 different models. Maximum capacity range is from 34 mmf. to 255 mmf. and the ratios of maximum to minimum run from 7:1 to 15:1. Maximum frame dimensions 2-1 16" by 2".

# JOHNSON

a famous name in Radio



E. F. JOHNSON COMPANY • WASECA • MINNESOTA



**First**

**with GRADE 1,  
CLASS 1 RESISTORS**

(First produced Dec. 1941—Millions made to date)

**First** with RESISTORS WOUND  
with CERAMIC INSULATED WIRE

(Pioneered and perfected by Sprague many years ago)

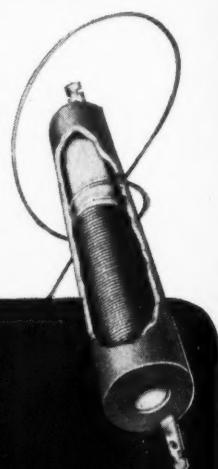
**First** with GLASS-TO-METAL SEALED  
RESISTORS (Pioneered by Sprague in 1941, now

produced commercially at the rate of thousands of  
seals per day)

**First** with GLAZED CERAMIC SHELLS  
and New Style End Seals for 5-, 10-, 25-, 50- and  
120-watt resistors. (One type of Koolohm—the stand-  
ard type—does the job under any climatic condition,  
anywhere in the world)

**First** and STILL EXCLUSIVE with MEGOMAX  
(The high-resistance, high-voltage resistors. Megohms  
of resistance operated at thousands of volts!)

One after another, Sprague Koolohm Resis-  
tors have established new performance  
records as proved indisputably by the record.  
One after another Koolohm Resistors have  
revolutionized traditional limitations to wire  
wound resistor usage—because radically dif-  
ferent Koolohm construction permits a higher  
degree of physical protection, better electrical  
characteristics, smaller sizes, and easier  
mounting arrangements than are possible with  
conventional resistor types. Write for catalog.



**KOOLOHM**

**SPRAGUE ELECTRIC COMPANY**  
(Resistor Division)      North Adams, Mass.



In  
War-  
In  
Peace..

# RADIART VIBRATORS (INDIVIDUALLY ENGINEERED FOR PROPER REPLACEMENT)

## GIVE Exceptional Service!

The high quality of RADIART VIBRATORS is well known to servicemen everywhere. That high quality has characterized all Radiart Products that have been and are being used by the Armed Forces on all fronts. As production for civilian users expands it will continue to increase the demand for RADIART VIBRATORS.

### LIMITED SUPPLY UNTIL V-J DAY

While production for civilian users may increase gradually, by far the greater part of our production will continue to be required for U.S. Armed Forces. We must and will meet all of their schedules on time.

### FEWER VIBRATOR TYPES SIMPLIFIES STOCK PROBLEM

By eliminating many little used types of vibrators Radiart has been able to increase production of all popular types. Now the dozen or so types of RADIART VIBRATORS necessary for over 7/8ths of all replacements are more readily obtainable.

Consult the Radiart Vibrator Catalog for complete information on all vibrators for all installations. The Radiart Line is the most complete for all replacement purposes.



## Radiart Corporation

3571 W. 62nd STREET • CLEVELAND 2, OHIO  
EXPORT DIVISION: 25 Warren Street • New York 7, N.Y.

# READ THE LATEST NEWS!...

## About **IRC** Type **BT** and **BW** **RESISTORS**

Here's a brand new file size Engineering Bulletin, just off the press! It offers you essential authentic information on IRC Type BT (Insulated Metallized) and BW (Insulated Wire Wound) Resistors. Concise, easy-to-read and an excellent ready-reference source, it contains eight pages of "meaty" material that will save you valuable time by quickly answering many of your resistance problems. Interesting construction facts, characteristics data, JAN Type Numbers, dimensional drawings, as well as a complete list of resistance values are compactly presented in this new BT-BW Bulletin. It should be in every Engineering and Design file. Write for your copy today. Address Dept. 7-G.



This Supplemental Bulletin supersedes all previous data on Types BT and BW Resistors in IRC Catalogs, pp. 1, 2, 3, 4 of Section II, Section III, and page 2 of Section III.

**TYPE BT METALLIZED INSULATED RESISTORS**  
IRC's Metallized filament principle and the unique construction of Type BT Resistors insures low operating temperatures, good wattage dissipation in small, thin body units, fully insulated. The BT design also provides exceptionally low noise level and maximum protection against humidity.

Three types—the Var watt BT, the Normal BTs and the Low watt BTs—have been developed for applications requiring Joint Army-Army Materiel Specification JAN-A-8-11.

The Type BT-A Auxiliary type RC10, now replaces the former Type BT-1, is recommended wartime production; however, requires use of all IRC production capacity on this item. The present Type BT-A production is supplied for RC10 requirements. Samples of Type BTs and available now for design of particular applications, and, because of its compact size and excellent characteristics, the Var watt unit is worthy of serious consideration for wartime production.

Type BTs, officially known for some time as a 1/2-watt Type BT-A, are now used for JAGC present Type BT-1/2. Although much smaller in size than the resistors they will replace, the characteristics of these resistors compare favorably with the larger standard resistors commonly used in the large field equipment. These resistor units due to their extreme compactness and ready availability.

Type BT-1 and BT-1/2 will be available as long as required for war use at these voltages, and Type BT-2, as described on page 4 of this Supplement.

**TYPE BW RESISTORS**  
The Type BW is a small, compact, insulated wire wound resistor similar in appearance and size to insulation-compensated resistors. BW units have been used in aircraft, military applications. BW units are highly reliable, inexpensive wire wound resistors. Typical uses are in motor starters, starters for low-voltage drop circuits, high-current starters, low-power ignition circuits, aircraft suppression coils and all low-range requirements in place of composition units.

The new Type BW-2, an extremely small Var watt unit, is a wartime development which will be available postwar for general use. Present production is devoted exclusively to a special War project, but samples will be supplied for the design and development of postwar equipment.

## INTERNATIONAL RESISTANCE CO.

401 N. Broad St. Phila. 8, Pa.

IRC makes more types of resistance units, in more shapes, for more applications than any other manufacturer in the world.

JULY, 1945 ★ **RADIO**

*Announcing the New*

# BALLENTEINE RECORD CHANGER

The BALLENTEINE Changer is engineered to provide trouble-free, dependable operation, safe from careless or accidental usage. It is the result of exhaustive research, expert technical design and skilled craftsmanship. The BALLENTEINE Record Changer assures complete customer satisfaction, free from mechanical annoyances so frequently found in ordinary record changers. Available in three models to fit your requirements.

**RUSSELL ELECTRIC COMPANY**

370 W. Huron Street, Chicago 10, Illinois

*Manufacturers of*

**BALLENTEINE RECORD CHANGER**

*Federal  
Tubes...*

**PERFECT  
VACUUM**



*Federal Telephone and Radio Corporation*



Newark 1, N. J.

# Again KAAR is FIRST!

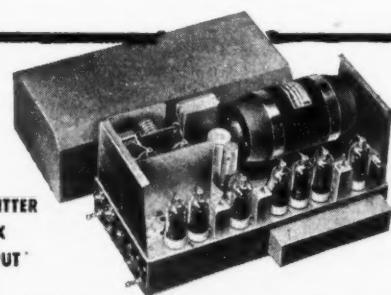


CARLTON D. MONK

## KAAR makes 50 and 100-watt mobile FM practical with instant-heating tubes

Kaar engineers—who pioneered instant-heating AM radiotelephones—have done it again! In presenting the new KAAR FM-50X and FM-100X, they now give you the advantages of FM *plus* instant-heating tubes... greater power and range

with lower battery drain! Standby current is zero. Yet the instant you press the button microphone, you are on the air with a full 50 or 100 watts output, improved voice quality, and minimum distortion—sending out a strong, clear message that insures excellent reception.

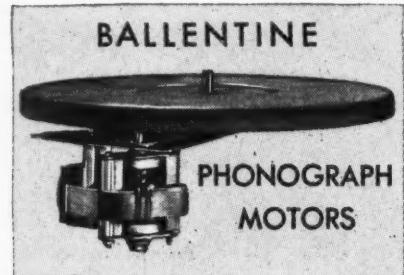


KAAR FM TRANSMITTER  
MODEL FM-50X  
50 WATTS OUTPUT

**KAAR**   
**ENGINEERING CO.**  
PALO ALTO • CALIFORNIA  
Export Agents: FRAZAR & HANSEN • San Francisco, California



# QUIET



In one expressive word you have the reason why so many phonographs will be powered by a **BALLENTINE** motor drive.

To the user, *quiet* means low background noise.

To the engineer, *quiet* means minimum vibration, dynamic balance, rigid adherence to close tolerances, modern manufacturing methods and equipment.

With **BALLENTINE** phono motor drives, you are assured of lowest rumble. Send today for descriptive folder on the *quiet* **BALLENTINE** phonograph motor drive.

**RUSSELL ELECTRIC CO.,** 370 W. HURON STREET, CHICAGO, ILLINOIS • MANUFACTURERS OF  
**BALLENTINE PHONOGRAPH MOTOR DRIVE**

# CONSOLIDATED VULTEE USES RAYTHEON TUBES

*in Electronic Recorder for Flight Testing*

No more tedious pencil notations . . . no more bulky camera equipment! An amazing "electric brain" developed by Consolidated Vultee Aircraft Corporation now helps this firm test its new planes electronically.

This remarkable device, consisting of a transmission unit in the plane and a receiving-recording station on the ground, employs a large number of famous Raytheon High-Fidelity Tubes.

It's just one of thousands of examples that prove an important point: where dependable performance is vital, you will find Raytheon Tubes. That means Raytheon Tubes can be relied upon to help you do your best service work and thus build your business steadily.

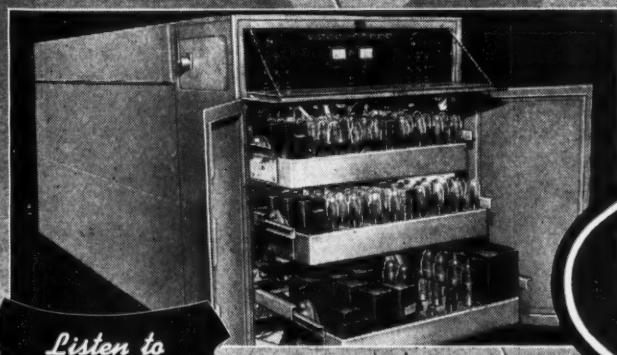
Switch to Raytheon Tubes now . . . and watch for a revolutionary merchandising program that Raytheon is developing for your benefit!

Increased turnover and profits, plus easier stock control, are benefits which you may enjoy as a result of the Raytheon standardised tube type program, which is part of our continued planning for the future.

## Raytheon Manufacturing Company

RADIO RECEIVING  
TUBE DIVISION  
Newton, Mass. • Los Angeles  
New York  
Chicago • Atlanta

**RAYTHEON**  
*Radio Tubes*



Listen to

"MEET YOUR NAVY"  
AMERICAN BROADCASTING CO.  
Every Monday Night  
Coast to Coast  
181 Stations

ALL FOUR DIVISIONS HAVE BEEN  
AWARDED ARMY-Navy "E" WITH STARS

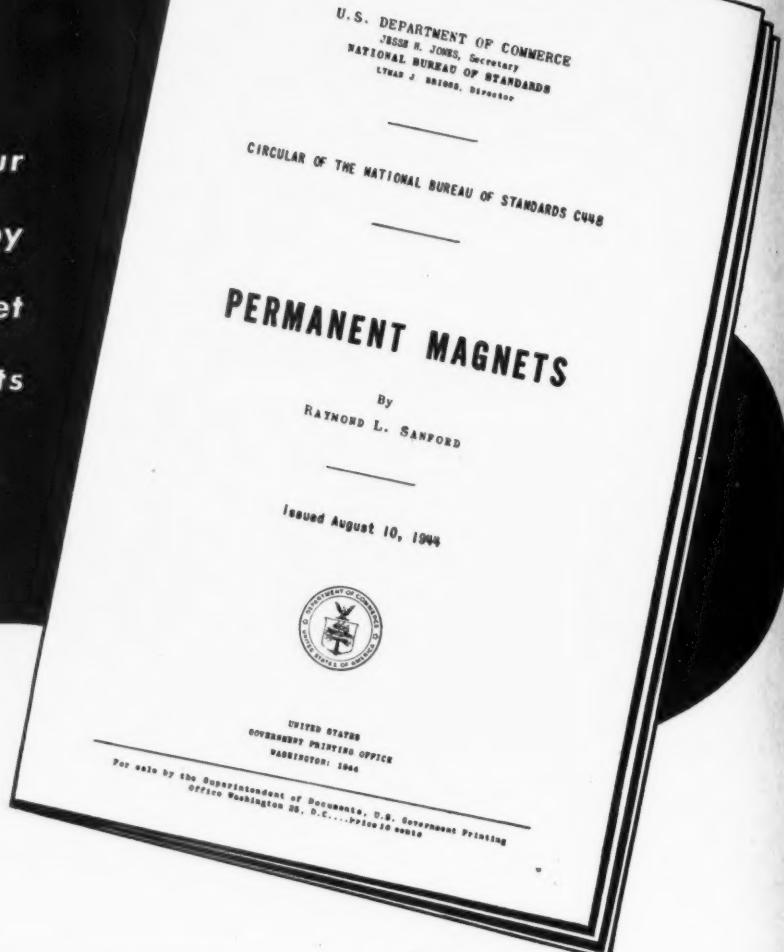
*Devoted to Research and the Manufacture of Tubes for the New Era of Electronics*

# YOURS!

Just write us, on your  
letterhead, for your copy  
of this valuable booklet  
on permanent magnets

● As a service to industry,  
The Arnold Engineering Com-  
pany is "lending a hand" in  
the distribution of what Arnold  
engineers believe to be a very  
informative study on the subject of permanent magnets.

This 39-page book of permanent magnet theory, de-  
sign data and references was published by the govern-  
ment. Arnold is pleased to make it available to you free  
of charge and without obligation. Write for it today!



## THE ARNOLD ENGINEERING COMPANY

147 EAST ONTARIO STREET, CHICAGO II, ILLINOIS

Specialists in the Manufacture of ALNICO PERMANENT MAGNETS

An Original **GUARDIAN** Development

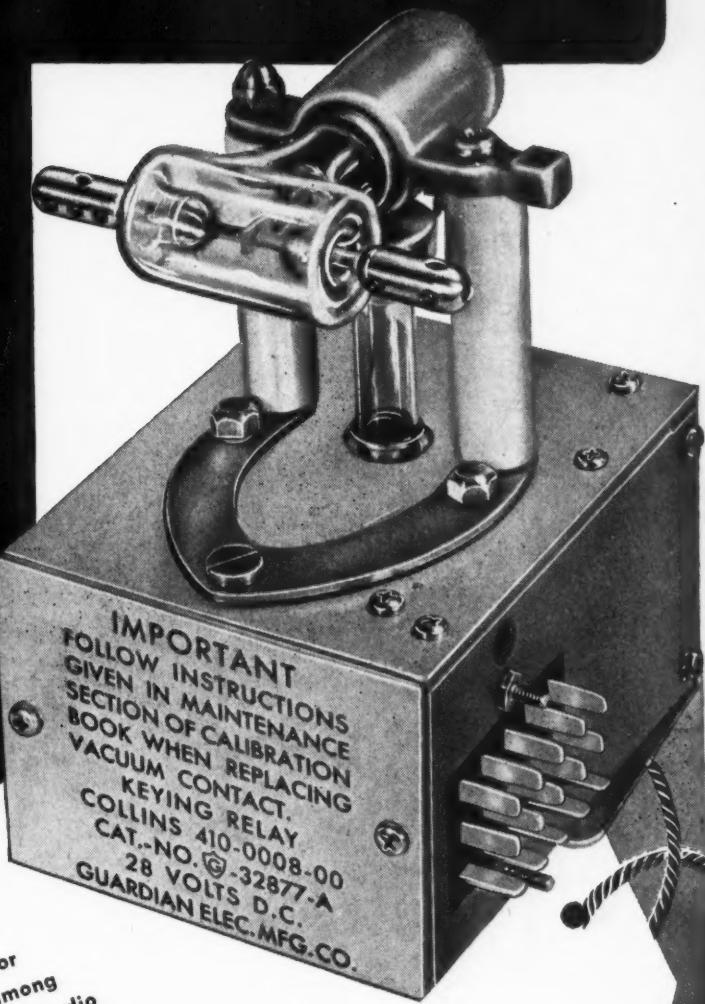


The New Vacuum Switch

# KEYING RELAY

for High Frequency—High Voltage—  
High Altitude Applications

The confidential development of this vacuum switch keying relay involved design ingenuity and ability to produce immediate results. It called for cooperation and a meeting of minds among Guardian engineers and those of Collins Radio Co., the U. S. Navy, Sperti, and General Electric. Then quantity production and the responsibility of being the sole source of supply for many months followed successful development of the relay. The same confidential treatment, the same engineering ability on electrical control, the same production capacity is yours for the asking. Write.



**GUARDIAN** ELECTRIC  
CHICAGO 12, ILLINOIS  
1605-H W. WALNUT STREET  
A COMPLETE LINE OF RELAYS SERVING AMERICAN INDUSTRY





**"JUST TELL HIM ALBION CAN SHIP ALL THE  
COILS HE NEEDS...THAT'LL QUIET HIM."**

---

**SUPER-QUALITY COILS AT REASONABLE PRICES**

More and more every day, the industry is turning to Albion for fast, quality and quantity production of coils, chokes, and transformers. That's because here you benefit from the unbeatable combination of management "know how," skilled workmanship, streamlined facilities, and central location. Your requirements will be given prompt and thoughtful attention.

**ALBION**  
**COIL COMPANY**  
ALBION, ILLINOIS

R. F. AND TRANSMITTING COILS AND CHOKES;  
I. F. TRANSFORMERS

**T**he Ballentine Record Changer Motor  
is engineered for just one purpose  
... to provide highest efficiency and  
lowest "rumble" for your changer.

This quiet, trouble-free motor  
is the result of expert technical  
design, the most modern manufacturing  
methods and equipment, and  
skilled craftsmanship . . . You can  
depend on the Ballentine Changer Motor.

**RUSSELL ELECTRIC COMPANY**  
370 W. HURON STREET • CHICAGO 10, ILLINOIS

*Manufacturers of*

**BALLENTINE CHANGER MOTORS**



**"HYTRON Tubes Are Good—SO WHAT!"**

Sure, Hytron tubes are good — so what! All tubes made for Uncle Sam are good. They have to be, or he wouldn't accept them.

But Hytron goes further. Not satisfied just to meet Uncle Sam's JAN-1A specifications, it always sets factory testing specifications to tighter tolerances than the Services require. In this way, Hytron assures top quality

despite slight meter inaccuracies and the human element. When more uniform adherence to specifications can be attained, tests simulating actual equipment performance are added.

This same insistence on the best will continue after the war. Then, too, we shall say, "Hytron tubes are good — so what! They have to be good to be good enough for you."

OLDEST EXCLUSIVE MANUFACTURER OF RADIO RECEIVING TUBES

HYTRON

MAIN OFFICE: SALEM, MASSACHUSETTS  
PLANTS: SALEM, NEWBURYPORT, BEVERLY & LAWRENCE




**BUY ANOTHER WAR BOND**

# TECHNICANA

## SPECTRUM ANALYSIS

\* The radio spectroscope as a device for viewing on a single screen the composition of radio energy being received by an antenna is discussed in the May 1945 issue of *Wireless World*. The article is entitled "Radio Spectroscopy" and was written by Thomas Roddam.

Mr. Roddam presents the principles of radio spectrum analysis and does not discuss any specific circuit diagrams.

The simplest form of radio spectroscope consists of a radio receiver with a motor-driven tuning capacitor. A variable resistor ganged to the common shaft delivers the horizontal sweep voltage to a cathode ray oscilloscope. The vertical deflection is obtained from the detector stage output of the receiver.

The spectrogram appears in Fig. 1.

An improved arrangement employs a motor-driven variable capacitor with

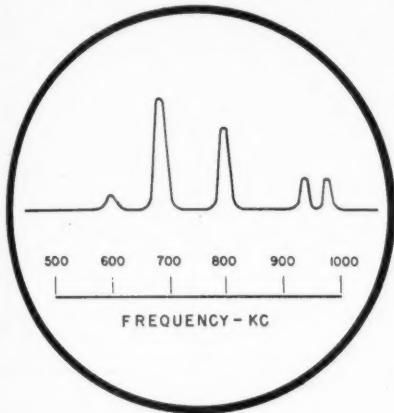


Figure 1

contacts on the shaft to provide synchronization with the cathode-ray sweep. The author describes the use of a magnetic strip rotating with the shaft, which passes near the gap of a magnetic pick-up and develops a triggering impulse for locking the sweep into the motor speed.

If the motor is truly synchronous the time base can be locked to the power line.

The author points out that the variable capacitor must be dynamically balanced and designed for 360° rotational coverage of the frequency band to be monitored.

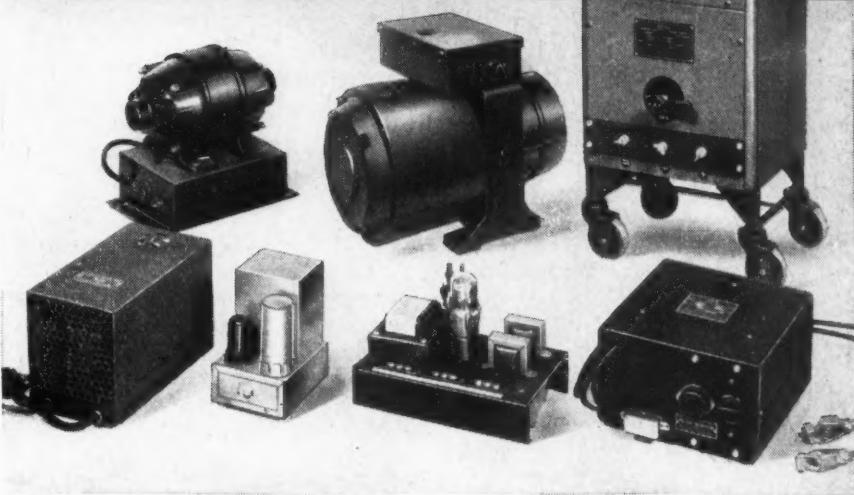
For a truly electronic spectroscope a visual alignment test oscillator is employed in place of the rotating capacitor. The test oscillator has saw-tooth frequency modulation over a suitable range at a low audio rate.

The horizontal sweep of the cathode ray oscilloscope is synchronized at this

QUICK DELIVERY ON LEADING MAKES OF

*Electronic and Electrical*

# POWER SUPPLIES



MANY types and makes of power supplies are centralized at ALLIED. This enables government and industry to obtain needed units in the shortest time possible. Quite a few types are on hand for rush delivery.

G.E.  
MALLORY  
ATR  
ELECTRONIC LAB.

JANETTE  
EICOR  
PIONEER  
KATO  
G.T.C.  
STANCOR  
KNIGHT  
ELECTRO PRODUCTS  
WINDCHARGER

Helpful  
BUYING  
GUIDE  
Available  
on Request  
Write for it!

Here you find Low Voltage High Current Supplies for aircraft, battery charging, plating, etc.; Vibrator and Rotary-Type Converters and Inverters for frequency changing and for converting A.C. to D.C. and D.C. to A.C.; Gas-Engine, Wind-Driven, and Motor-Driven Generators; Vibrapacks for mobile operation; Dry Batteries; and general utility Power Supplies. Also Dry Disc, Electronic and Vibrator Rectifiers.

Save time and work... call ALLIED First!  
Use our complete stock and procurement service.  
WRITE, WIRE, OR PHONE HAYMARKET 6800

# ALLIED RADIO

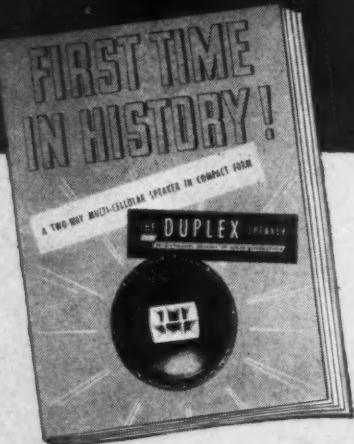
C O R P O R A T I O N

833 W. Jackson Blvd. • Dept. 14-G-5 • Chicago 7, Illinois

SUPPLIERS OF ELECTRONIC PARTS AND EQUIPMENT TO INDUSTRIAL AMERICA  
Electronic Tubes, Rectifiers, Power Supplies, Intercommunicating Systems, Sound Systems, Photo-Cell Equipment, Batteries, Chargers, Converters, Generators, Supplies for Resistance Welders, Fuses, Test Instruments, Meters, Broadcast Station Equipment, Relays, Condensers, Capacitors, Resistors, Rheostats, Transformers, Switches, Coaxial Cable, Wire, Soldering Irons, Microphones, Speakers, Technical Books, etc.

# Complete

## D U P L E X D E T A I L S



### NOW AVAILABLE!

Fresh off the presses, a 12-page bulletin on the new, amazing Duplex Speaker is now available . . . jam-packed with engineering and technical data, performance curves, distribution characteristics. Details of the Dividing Network, A323 Amplifier and attractive cabinets also included.

**SEND FOR YOUR COPY TODAY**

# ALTEC

LANSING CORPORATION

1210 TAFT BLDG., HOLLYWOOD 28, CALIF.  
250 WEST 57 STREET, NEW YORK 19, N.Y.  
IN CANADA: NORTHERN ELECTRIC CO.

## TECHNICANA

[Continued from page 25]

same rate. The output of the detector stage of the receiver when the frequency-modulated test oscillations are applied to the mixer, forms the vertical deflection.

A block diagram is shown in Fig. 2. The wide band amplifier delivers the r-f signal being monitored to the signal

of the i-f amplifier and  $N$  is the band width under investigation. For  $N = 500$  kc and  $M = 10$  kc, this a sweep rate of 67 cycles per second. The above formula is based on experience with television amplifiers which indicates that a signal lasting  $t$  seconds requires a band width of  $3/t$  cycles for a reasonable amount of distortion.

### INK RECORDER AMPLIFIER

★ A new circuit for a power amplifier designed to operate an ink recorder

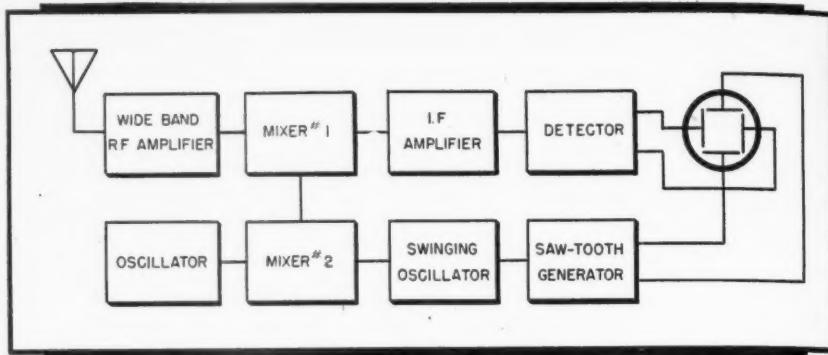


Figure 2

grid of the mixer tube #1. The lower chain of Fig. 4 delivers the f-m voltage to the oscillator grid of the mixer tube #1. The swinging oscillator is driven over the range of say  $10 \pm 0.25$  mc by the saw-tooth generator. The second oscillator, and mixer #2, are provided so that the range of the spectrum analyzer can be extended. Then a frequency ( $f_2 \pm 10$ )  $\pm 0.25$  mc will be supplied to mixer #1.

The saw-tooth sweep rate is of importance and this rate should not exceed  $M^2/3N$ , where  $M$  is the band width

consumes only  $22\frac{1}{2}$  watts of power with a 320 volt power supply. The static power consumption is  $6\frac{1}{2}$  watts and the equipment permits the use of a 3000 ohm per coil requiring only 0.3 watt. The amplifier frequency is 18%.

This amplifier is described by Mr. Donald Robinson, of Telephone Rentals, Ltd. The article, entitled "The Design of Power Amplifiers for Operating Ink Recorders" appears in the May 1945 issue of *Electronic Engineering*.

The pen recorder is suitable for medical work involving measurement of

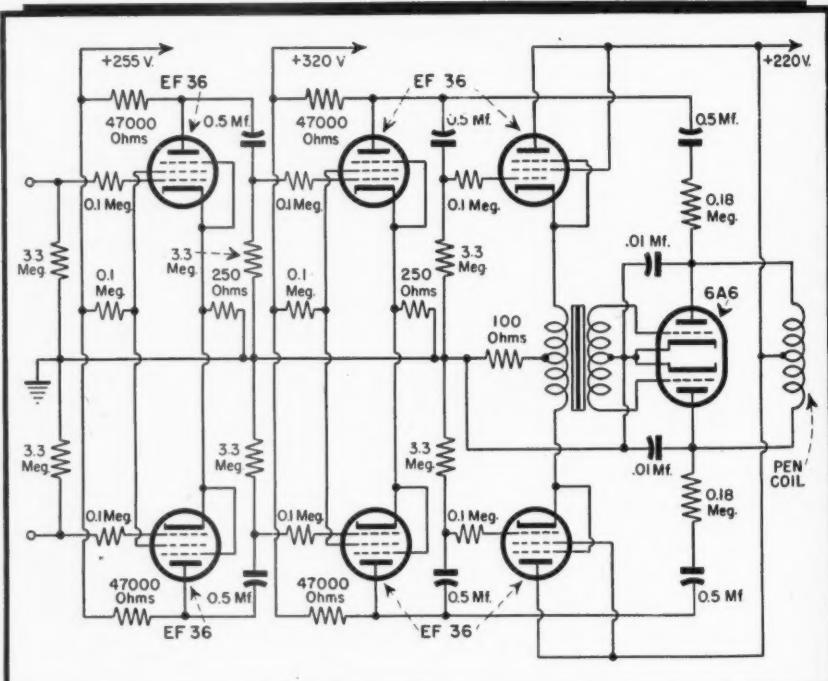
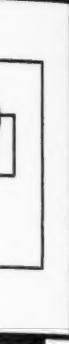


Figure 3

the band  
or  $N =$   
sweep rate  
the above  
ence with  
cates that  
quires a  
a reason-

ER  
amplifier  
recorder



ower with  
he static  
s and the  
f a 3000  
0.3 watt.  
3%.

by Mr.  
e Rentals,  
e Design  
ating Ink  
ay 1945  
ng.  
for medi-  
ement of

+220V.

PEN'  
COIL

## DUPLICATING A GERMAN VACUUM TUBE IN 3 DAYS

Just behind the battlefield, a telephone system lay dead. The retreating enemy, hoping to return, had not blown it up, but had taken with them its vacuum tubes. To put it back to work, the General ordered 1000 new tubes — spot delivery.

A sample tube was flown back to the United States and brought to Bell Telephone Laboratories. It was of German design, different from any American tube in both dimensions and characteristics. Could it be duplicated soon? The job looked feasible. Within three days, try-out models were on their way to Europe. Three weeks later, Western Electric Company had made and delivered every tube. They were plugged in; vital communications sprang to life.

Vacuum tubes are an old story for Bell Laboratories scientists. Back in 1912 they made the first effective high vacuum tube. Three years later, they demonstrated the practical possibilities of tubes by making the first radio talk across the Atlantic, pointing the way to radio broadcasting. Since then, they have developed and utilized the vacuum tube wherever it promises better telephone communication — there are more than a million in your Bell Telephone System.

Today, Bell Telephone Laboratories is solving many of the toughest tube problems faced by the Armed Forces. When the war is over, it goes back to its regular job—keeping American telephone service the best in the world.



• This electrical replica of a heater-type pentode was made for use in German telephone repeaters.



BELL TELEPHONE LABORATORIES

Exploring and inventing, devising and perfecting for our Armed Forces at war, and for continued improvements and economies in telephone service.

# FOSTER TRANSFORMERS

## AVAILABLE NOW!

Facilities for peacetime manufacture of transformers are already available at A. P. Foster, and, as war commitments are filled, will be increasingly at your service.

During the war years A. P. Foster has supplied thousands of custom-designed and custom-built transformers to all branches of our armed services, for use in all parts of the world under great extremes of climatic condition.

High production schedules have been maintained by advanced Foster manufacturing techniques. High standards of performance were demanded, achieved and will be maintained—to the benefit of America's peacetime economy.

As your own reconversion plans advance from the conference stage to the blueprint stage, it may well be worth your while to bear in mind that Foster engineers and designers are ready now to consult with you on every transformer problem and to furnish estimated costs and delivery schedules on experimental or quantity production of standard transformers or special jobs custom-built to your own specifications.

- BOB REID, 810 West 57th Street, Indianapolis 5, Ind., Telephone Broadway 2725
- BAUMAN AND BLUZAT, 2753 West North Avenue, Chicago 47, Ill., Telephone Humboldt 6809-10-11-12
- THE A. P. FOSTER COMPANY, BARRETT BORDER, 11 W. 42nd St., New York 18, N. Y., Telephone PEnnsylvania 6-9133

SPECIALISTS IN BUILDING TRANSFORMERS SINCE 1938

## A. P. FOSTER COMPANY

TRANSFORMER ENGINEERS & MANUFACTURERS

719 WYOMING AVENUE, LOCKLAND 15, OHIO (SUBURB OF CINCINNATI)

# HIGH VACUUM NOW CONTROLLED TO ONE-BILLIONTH OF AN ATMOSPHERE

HIGH on the list of important recent electron tube developments in the National Union Research Laboratories is this ultra sensitive N. U. Ionization Gauge.

Used as a control device in the evacuation of other electron tubes, this gauge reads pressures of .00001 of a micron! High vacuum is assured with resulting uniform high performance characteristics of all N. U. Tubes it helps to manufacture.

Having no grid element, this gauge is completely free from Barkhausen oscillations. Construction is simple, rugged, dependable—and, of course, economical to manufacture.

Here again is an example of the many contributions National Union engineers are making to the advance of electronics. For progress through research—count on National Union. *National Union Radio Corporation, Newark 2, New Jersey.*

## N. U. IONIZATION GAUGE

### Typical Operation

- Filament voltage—3.0 volts      • Filament current—1.8 A.
- Electron collector voltage—13 volts      • Electron current—20 Ma.
- Ion collector voltage—200 volts
- Sensitivity—Ten times the ion current in amperes equals the pressure in mms. of mercury.

*It is possible to expose the hot filament of this gauge to air at atmospheric pressure and later have it function efficiently under vacuum conditions.*



*Transmitting, Cathode Ray, Receiving, Special Purpose Tubes • Condensers • Volume Controls • Photo Electric Cells • Panel Lamps • Flashlight Bulbs*

**TURNER Microphones**

*A precision unit for every job*

WHATEVER your need for accurate reproduction of voice, music or sound, there is a Turner Microphone especially adapted to your requirements. The complete Turner line includes dependable crystal and dynamic microphones for every communications purpose. A few are illustrated here.

Illustrated Turner catalog gives full details on all Turner Microphones for P.A., recording, sound system, commercial broadcast and amateur work. Get the full story of Turner performance and let Turner engineers help you select the units which meet your requirements. Write for catalog today.

The **TURNER CO.**  
PIONEERS IN THE COMMUNICATIONS FIELD  
908 17th St. N.E., Cedar Rapids, Iowa

Crystals licensed under patents of the Brush Development Co.,

heart and nervous system activity and can also be used with some systems of submarine telegraphy. It is suitable for use in a portable system.

The amplifier is claimed to have linear frequency response from  $\frac{1}{2}$  cycle to 6 kc and the response is only 3 db down at 10 kc.

The author first describes two types of amplifiers in current use, both of which consume a greater amount of power at less efficiency and higher voltages.

Class B operation, using a 6A6 dual triode for the output stage, permits low standing anode current. Inverse feedback of voltage is employed to reduce the source impedance and improve the damping factor of the pen, and reduce harmonic distortion to less than 5%.

The complete circuit is shown in Fig. 3.

The inverse feedback consists of feeding part of the output voltage back to the grids of the EF36 driver tubes through the 180,000 ohm resistors and the 0.5  $\mu$ f capacitors. The percentage of feedback is determined by the relative values of the feedback resistors and the 47,000 ohm pre-drivers tube load resistors. The ratio is approximately 4:1, so that there is about 20% voltage feedback. There is no phase shift in the drivers stage so that feedback voltages are in the correct phase.

The introduction of feedback, however, increases the input voltage required by the driver stage from 83 volts to 122 volts (grid-to-grid, r.m.s.).

The driver stage is a transformer-coupled cathode follower which provides an output of 53 volts, r.m.s. at 0.2 watt and with good regulation.

A low resistance path from the 6A6 grids to ground is required to keep the grid near zero bias.

To meet above requirements a special pre-driver stage output transformer was developed.

The author also presents his design of the stabilized power supply.

#### CAPACITORS FOR SERIES HEATERS

\* There are some advantages in the use of capacitors instead of resistors in circuits consisting of several vacuum tube heaters in series. The capacitor offers longer life, low power consumption, and self compensation when the number of tubes is varied.

Mr. G. S. Light has reviewed these advantages versus the disadvantages in an article appearing in the April 1945

## TECHNICANA

[Continued from page 30]

issue of *Electronic Engineering*. The article is entitled "Condensers in Series-Heater Circuits".

The disadvantages in the use of capacitors are that only one frequency can be used with a given circuit arrangement, the capacitor has a slightly greater cost, and a special switching arrangement is necessary when using series pilot lamps. Furthermore, the warming-up period is increased.

The value of the capacitance required can be calculated as in the following example. For three 6.3 volt, 0.3 ampere tubes and two 25 volt, 0.3 ampere tubes, the voltage drop across the heaters is 68.9 volts. The voltage across the capacitor, with a 230 volt, 60 cycle, supply voltage is  $V_c = \sqrt{230^2 - 68.9^2} = 219.5$  volts. The capacitance in  $\mu F$  =  $10^6 \times 0.3 = 3.63 \mu F$ .

$$2\pi \times 60 \times 219.5$$

The self-regulating action is good when the total heater voltage is less than approximately one-third of the supply voltage. This is apparent from

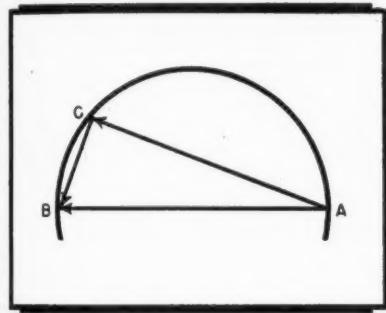
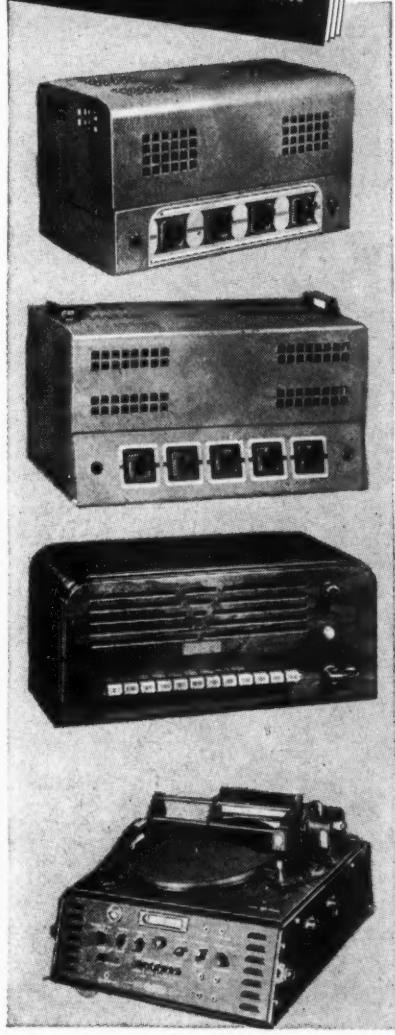
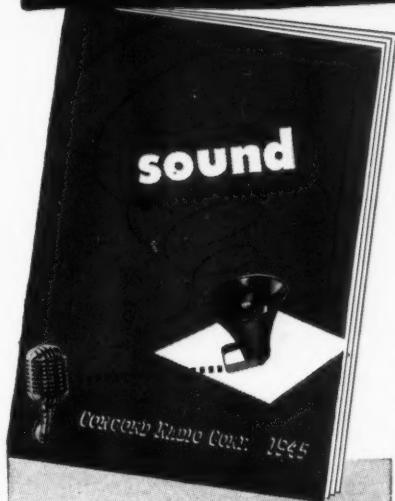


Figure 4

Fig. 4, in which  $AB$  = supply voltage,  $AC$  = capacitor voltage, and  $BC$  = total heater voltage. When  $BC$  is small compared to  $AB$ , then variations in  $BC$  do not produce substantial variations in  $AC$ , so that the current through the capacitor remains about the same. The current regulation with a resistor is not as good as this.

With indirectly heated tubes the warm-up period of the filaments is greater than the period of the transient current which occurs when the switch is first turned on. The warm-up period of a pilot lamp is shorter, and short life can be expected unless the pilot lamp is shorted out during the transient period. This can be accomplished with a delayed action switch, or by using a single switch to short out the heaters for "off". This latter method would mean that the capacitor would remain permanently in the line, but since there is no power consumption by the capacitor, this is permissible.

# AMPLIFIERS INTERCOMS RECORDERS



## Write for This Important New CONCORD Presentation

"Sound Equipment"—ready now—a new up-to-the-minute Concord folder illustrating and describing our complete line of Amplifiers, Intercoms and Recorders AVAILABLE FOR IMMEDIATE SHIPMENT.

**Amplifiers**—ranging in output ratings of 17 watts to 75 watts A.C.—also 6-volt units with and without built-in phonograph. Complete listing of speakers, microphones and essential equipment also included.

**Intercommunication Systems**—master and sub-station combinations for every purpose from 2 to 100 stations. Push button control, universal operation, "busy signal" and "call waiting light" features.

**Recording Equipment**—professional type for microphone recording, radio recording, transcriptions, public address.

**Engineering Service**—Our engineering service is at your command, without charge, to answer any and all "Sound Equipment" questions.

Mail the coupon below for your copy of "Sound Equipment" now.

## CONCORD RADIO CORPORATION

Lafayette Radio Corporation

CHICAGO 7, ILL. ATLANTA 3, GA.  
901 W. Jackson Blvd. 265 Peachtree Street

CONCORD RADIO CORP.

901 W. Jackson Blvd., Dept. F-75  
Chicago 7, Illinois

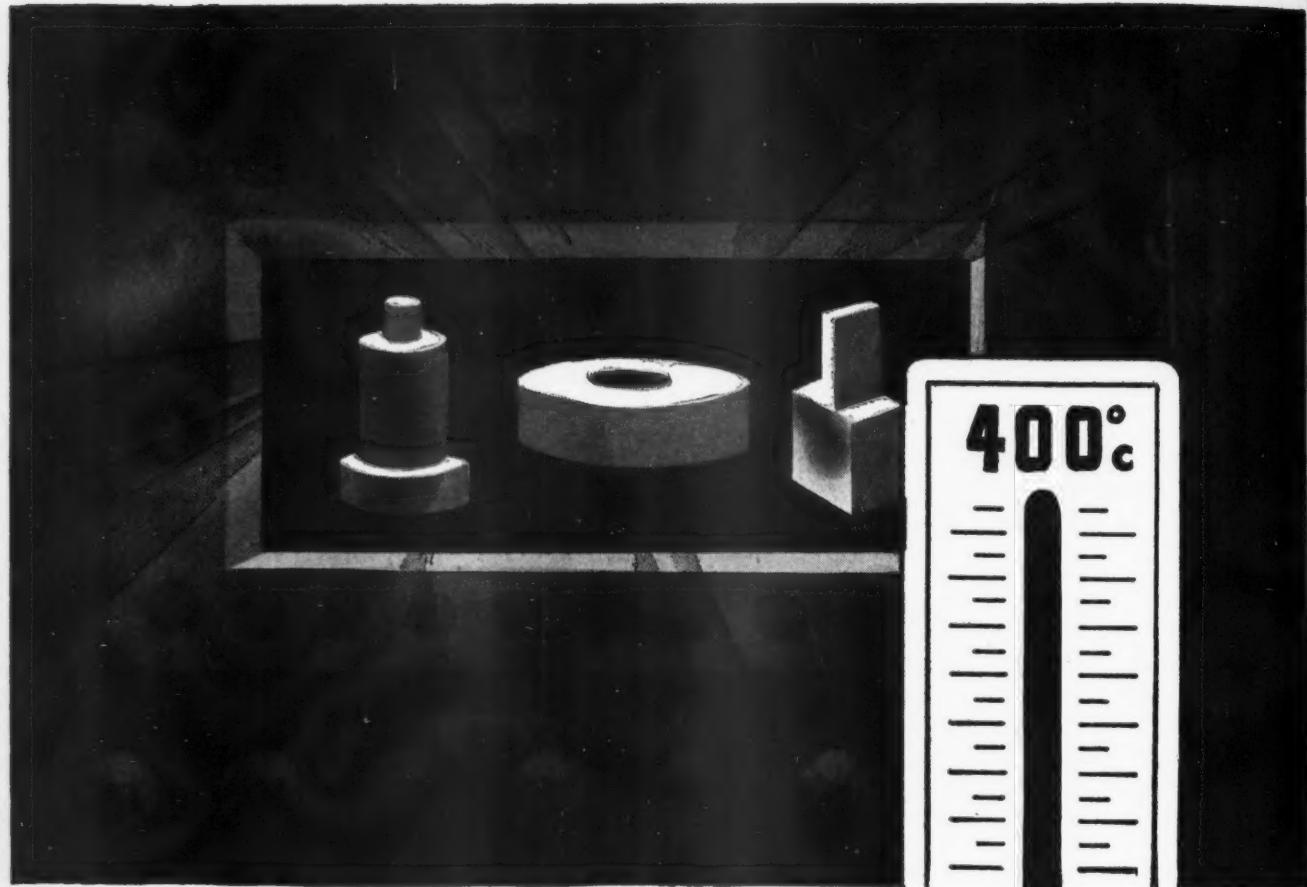
Please send me at once copy of your new  
"Sound Equipment" folder.



Name.....

Address.....

City..... State.....



# MYCALEX 400

## WITHSTANDS HIGH TEMPERATURES

An outstanding characteristic of MYCALEX 400 is that it can withstand temperatures above 400° C. without softening or any permanent change in dimensions or properties.

Thus MYCALEX 400 has proved of great value as a low loss insulator in communications and other high frequency apparatus intended for use at elevated operating temperatures.

MYCALEX 400 is inorganic, free of carbonization...impervious to oil and water...not subject to cold flow. It meets all Army and Navy specifications as Grade L-4 material (JAN-I-10). It combines low loss factor with machinability to close tolerances. In sheets and rods. Fabricated to specifications.



### OTHER MYCALEX CORPORATION PRODUCTS

#### ● MYCALEX K

A series of ceramic capacitor dielectrics, with dielectric constant selectable from 8 to 19. Low power factor, high dielectric strength. Meets Army and Navy requirements as Class H material (JAN-I-12). To specifications.

#### MOLDED MYCALEX

Low loss, high temperature injection molded insulation. Molded in union with metals in irregular shapes. High production rates result in economical prices.

MYCALEX K and MOLDED MYCALEX will also withstand 400° C.

## MYCALEX CORPORATION OF AMERICA

"Owners of 'MYCALEX' Patents"

Plant and General Offices, CLIFTON, N. J.

Executive Offices, 30 ROCKEFELLER PLAZA, NEW YORK 20, N.Y.

# Audio-Carrier-Frequency R-C Oscillator

ROBERT C. PAYNE

This oscillator covers a range of 20 to 20,000 cycles, using a direct-reading dial with but two logarithmic scales, and has other unusual features

THE resistance-capacity tuned type of audio oscillator has been widely accepted and valued for its stability, simplicity, and good wave form. The author has modified such an RC oscillator which has been previously described in RADIO<sup>1</sup> to obtain certain additional desirable features as shown in Fig. 1.

In this circuit a range of 20 cycles to 200 kilocycles is obtained, using a direct-reading dial calibrated in two scales, 20-70 and 60-210. By using an 8-position band switch and properly proportioning the resistors of the tuning circuit, these two scales are arranged to serve for the whole range and spread out the scale so that frequencies can be read very accurately for tests on filters or other equipment at audio and carrier

frequencies. High and low output impedances are under control of an output switch. These impedances remain at an approximately constant value because the output control is placed in the grid of the output tube. A built-in diode rectifier permits checking the output with any convenient d-c voltmeter or milliammeter. A "Clipped Wave" switch modifies the feedback circuit to clip the sine wave peaks and so to produce a partial square wave useful for synchronization or other special purposes.

## Oscillator Circuit

The operation of the oscillator circuit shown in Fig. 1 depends on positive feedback from the plate of tube  $V_2$  to the grid of tube  $V_1$  through the fre-

quency-determining network formed by the resistors  $R_{1-8}$ ,  $R_{11-18}$ , and condensers  $C_{1,2,3}$  and  $C_{11,12,13}$ . Negative feedback to the cathode of  $V_1$  through  $R_{30}$  controls the output and maintains good wave form. The two 6-watt lamps in the cathode circuit control the amount of negative feedback. As the circuit tends to oscillate more vigorously the increased alternating current causes the resistance of these lamps to rise rapidly, increasing the negative feedback voltage to the cathode and tending to keep the output voltage at a constant level. The tube  $V_3$  isolates the load from the oscillating circuit to prevent any frequency reaction.

The oscillating circuit consisting of the tubes  $V_1$  and  $V_2$  and the tuning

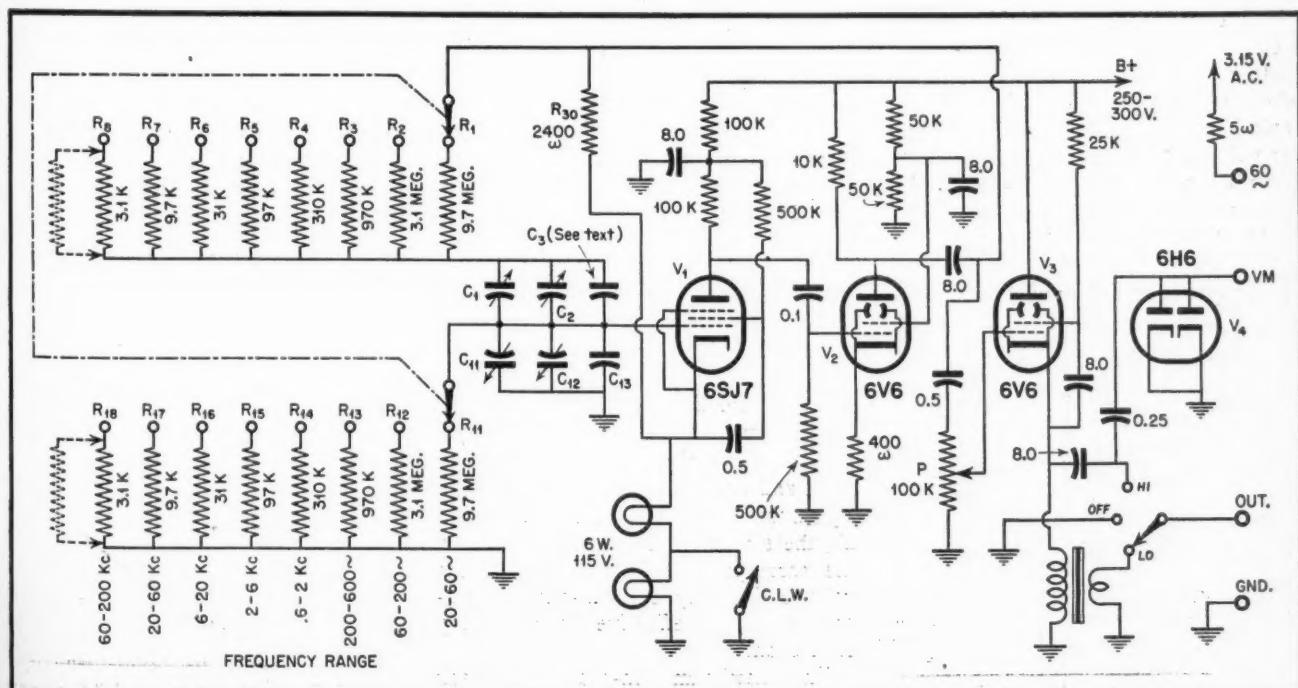


Fig. 1. Schematic of the oscillator tuned by R-C network with variable capacitors

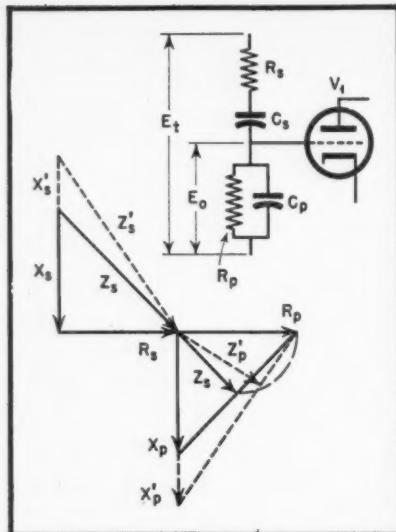


Fig. 2. Impedance vectors of R-C network,  $R_s = R_p$  and  $C_s = C_p$ . Solid lines at oscillating frequency, dotted lines at lower frequency

network are well shielded from the power pack and the rest of the circuit to avoid hum pickup and undesirable feedback from the output stage. The power supply has not been shown as this can be of conventional design, operated from the power line. The 8  $\mu$ F condensers are of the electrolytic type,  $C_s$  and  $C_{12}$  are mica, and all others are of the paper type. The output control potentiometer is placed in the grid of the output tube  $V_1$  so that an approximately constant output impedance may be presented to the load. Using an output transformer of about 10-to-1 ratio, the author obtains an output impedance of about 4 ohms on the "Lo" point and about 400 ohms on the "Hi" point. An "Off" position between the "Hi" and "Lo" points is convenient for cutting off output during tests.

The diode rectifier tube  $V_1$  furnishes a convenient means of checking and adjusting the output to constant value when this is required. For output indications a d-c voltmeter, of 1000 ohms per volt, on the 50 or 100 volt scale, or a milliammeter in series with 50-100 thousand ohms, can be connected between the "Vm" binding post and ground, for such use the meter need not

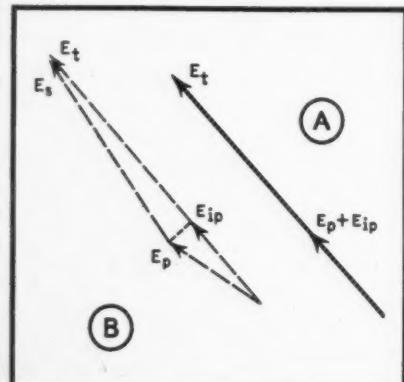


Fig. 3. Voltage vectors for Fig. 2: (a) at oscillating frequency, (b) at lower than oscillating frequency

be calibrated. The "CL. W." switch shorts out one of the 6-watt lamps to reduce the negative feedback. Since the amount of negative feedback is the principal factor in the production of a good wave form, this reduction of feedback results in the clipping of the peaks of the waves somewhat so they approach a square wave. Such a wave is useful for synchronization and for various testing purposes. Operation of the "CL. W." switch changes the frequency somewhat, for which corrections should be made when required.

### Theory of Tuning Network

The tuning network consists of a series combination  $R_{1-s}$  and  $C_{12,23}$ , and a parallel combination  $R_{11-18}$  and  $C_{11,12,18}$ . The impedance,  $Z_s$ , of the series combination is found graphically by the vector addition of the resistance,  $R_s$ , of resistors  $R_{1-s}$ , and the reactance,  $X_s$ , at a given frequency, of the capacity  $C_s$  formed by the condensers  $C_{12,23}$ . The

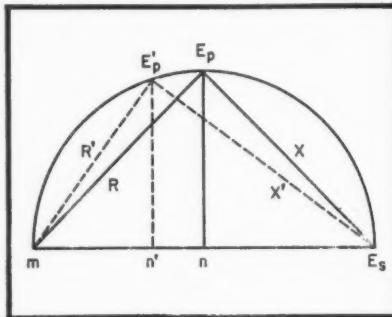


Fig. 4. Circle diagram of R-C network showing relative absolute voltages where  $R_s = R_p$  and  $C_s = C_p$

impedance,  $Z_p$ , of the parallel combination of the resistance,  $R_p$ , of the resistors  $R_{11-18}$ , and the reactance  $X_p$ , at the same frequency, of the capacity  $C_p$  formed by the condensers  $C_{11,12,18}$  is also found in a vector diagram, perhaps less familiar, which has been previously described by the author<sup>8</sup>.

These diagrams have been combined in Fig. 2 in which values have been chosen so that  $R_s = R_p$  and  $C_s = C_p$ . The dotted lines show impedances at a lower frequency where  $X_s = R_s$  and  $X_p = R_p$ , and the phase angles of  $Z_s$  and  $Z_p$  are both 45° and equal. The dotted lines show impedances at a lower frequency where  $X_s$  and  $X_p$  are greater. It is seen that  $Z_p/Z_s$  is greater than  $Z'_p/Z'_s$ . Fig. 3(a) and (b) show the corresponding voltage diagrams where  $E_s$  is the feedback voltage from the plate of  $V_1$  and equal to the sum of the voltage  $E_p$  across  $Z_p$  and the voltage  $E_s$  across  $Z_s$ , these voltages being proportional to the corresponding impedances. Of the voltage  $E_s$ , only the "in-phase" component  $E_{ip}$  is effective in producing oscillation.

The maximum "in-phase" feedback voltage occurs at the frequency which makes the phase angle of the series

combination equal to that of the parallel combination. If the values are so proportioned that  $R_s/C_s = R_p/C_p$ , the phase angles become equal (45°) and the circuit oscillates at a frequency such that  $R_s = X_s$  and  $R_p = X_p$ . If  $R_s = R_p$  and  $C_s = C_p$ , the relative values can be shown in a combined diagram, Fig. 4. Here the solid lines show the relative absolute values of the voltages  $nE_p$  and  $nE_s$  across the impedances  $Z_p$  and  $Z_s$ , respectively at the frequency of oscillation where  $R_s = X_s$  and  $R_p = X_p$ . The dotted lines show values at another frequency at which  $R_s \neq X_s$  and  $R_p \neq X_p$ . Although the scale of values for the dotted lines has been changed to accommodate the same semicircle, the relative values remain unchanged and it is seen that the ratio of voltage  $nE_p$  to  $nE_s$  is greatest at the oscillating frequency. Due to the fact that these voltages are no longer in phase at any frequency other than that shown by the solid lines, it can be shown also that the ratio of the in-phase component of  $nE_p$  ( $E_{ip}$  of Fig. 3) to the in-phase component of  $nE_s$  is relatively even less.

If the capacities are not in the same ratio as the resistors, or  $R_s/C_s$  is unequal to  $R_p/C_p$ , the maximum "in-phase" feedback voltage to the grid of  $V_1$  still occurs at the frequency which makes the phase angles of  $Z_s$  and  $Z_p$  equal. Then it is not possible for  $R_s$  to equal  $X_s$  and  $R_p$  to equal  $X_p$  at the same frequency, so the phase angles become equal at a frequency which causes these angles to differ from 45°. This is shown in Fig. 5 where, for example,  $R_s/R_p = 2/3$  and  $C_s/C_p = 3/4$  and the tangent of their phase angles is 1.4. However, in any practical design, it is desirable that the ratio  $C_s/C_p$  remain substantially constant over the tuning range to avoid variation in the feedback ratio and constant variation in output.

The oscillating frequency due to any particular combination can be calculated from the fact that the phase angles of  $Z_s$  and  $Z_p$  must be equal. The tangents of these angles must then be equal or

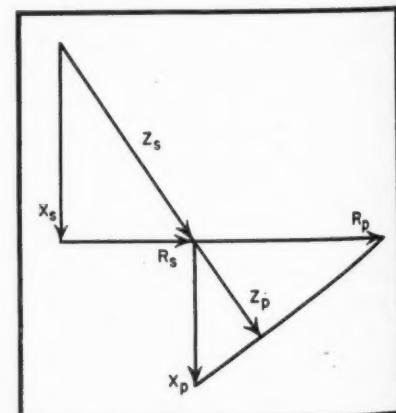


Fig. 5. Impedance vectors of R-C network tuning at oscillating frequency where  $R_s/C_s$  is not equal to  $R_p/C_p$

parallel so  $C_s = R_p/X_p$ , then  $1/R_s(1/2\pi f C_s) = R_p(2\pi f C_p)$ . From this equation it is found that the frequency of oscillation,  $f = 1/2\pi\sqrt{R_s R_p C_s C_p}$ , or expressed in cycles, megohms, and micromicrofarads,  $f = 15900/\sqrt{R_s R_p C_s C_p}$ .

The circuit shown in Fig. 1 as built by the author uses a four gang broadcast condenser for  $C_{1,2}$  and  $C_{11,12}$  with resistances  $R_s$ , ( $R_{1-8}$ ), and  $R_p$ , ( $R_{11-18}$ ), of equal value. The capacity per section is 380  $\mu\text{f}$  and the capacity shunt to ground, across  $C_{11,12,13}$ , of the condenser frame and common rotors, (which of course must be well insulated) is 30  $\mu\text{f}$ . The condenser  $C_s$  has a capacity of 180  $\mu\text{f}$  and  $C_{13}$ , 150  $\mu\text{f}$ , these values make  $C_s$  and  $C_p$  equal and also pads the condensers to reduce the frequency range as will be discussed later. The tuning condenser is driven by a vernier control dial which makes possible a very close setting of frequency.

It is possible to use a 3-gang con-

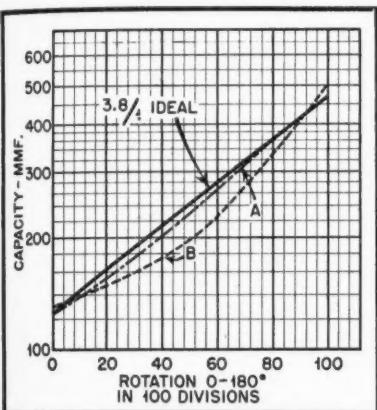


Fig. 6. Condenser capacity curves, the ideal logarithmic for a 3.8/1 range R-C oscillator, "A" a padded broadcast condenser suitable for this range, and "B" a condenser less suitable for this range. The same  $C_s$  is used in both cases. The angle of  $V_1$  still remains in phase with  $V_2$  which makes  $Z_p$  equal. This is due to equal sections of the same frequency. Some equal angles are shown in Fig. 5 between  $2/3$  and  $1/2$  of their respective tangents, in any case the angle is usually constant to avoid any errors. Due to any calculated angles of the tangents equal or not.

#### Frequency Scales

The ideal scale on the frequency dial is logarithmic, that is, the scale divisions are proportional to the logarithm of the corresponding frequency. This makes possible a constant percentage of accuracy in taking readings. Many test instruments have this type of scale and tests such as audio fidelity are usually plotted on logarithmic paper. Since it is usually necessary to use tuning con-

densers having capacity curves of conventional broadcast design, it is desirable to examine the possibilities of obtaining a logarithmic calibration with condensers which may be available.

The capacity curve for an ideal condenser can be readily calculated and this can be compared with curves of available condensers. With the capacities  $C_s$  and  $C_p$  equal and the resistances  $R_s$  and  $R_p$  equal, frequency is inverse proportional to capacity or  $f = k/C$  and, for a logarithmic calibration, the capacity must vary logarithmically from minimum to maximum. To cover a given range the condenser must be padded by a fixed condenser shunt. For example, consider a 3.8/1 frequency range using a variable condenser of 380–30  $\mu\text{f}$ . To cover this range the padded maximum and minimum capacities must have the ratio 3.8/1 =  $(380+X)/(30+X)$ , or  $X$ , the shunt capacity, = 95  $\mu\text{f}$ . The maximum and minimum padded capacities are then 475  $\mu\text{f}$  and 125  $\mu\text{f}$ , these values are plotted on semi-logarithmic paper and a straight line drawn through them. This line defines the ideal capacity variation vs. degrees rotation for this frequency range.

These values have been plotted in Fig. 6 where the vertical scale represents capacity values of the padded condenser and the horizontal scale divisions of rotation, 100 divisions being equal to 180°. The solid line represents the capacity of the ideal condenser. The dashed line represents the padded capacity of condenser A used to obtain an approximately logarithmic scale over a range of 3.8/1. The dotted line represents the capacity curve of condenser B, properly padded for this range. Condenser B is less suited for a logarithmic scale in this range; its use would result in a crowding together of frequencies at the low frequency, or high capacity, end of the dial and a spreading out at the high frequency end, tending to approach a linear scale.

In Fig. 7 is shown the ideal curve for a 10/1 frequency range. For this range condenser A requires only 9  $\mu\text{f}$  of padding capacity, it can be seen by the dashed curve that it is less suited for this range. Condenser B, also properly padded, is more suited for this range

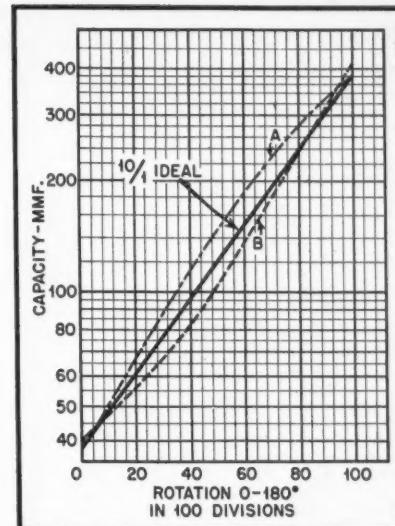


Fig. 7. Condenser capacity curves, the ideal logarithmic for a 10/1 range R-C oscillator. "A" and "B" curves of condensers shown in Fig. 6 but padded for a 10/1 range. Neither conforms closely to the ideal for this range

than it is for the 3.8/1 range, as seen by the dotted curve.

To divide a 10/1 range into two parts logarithmically, the square root of 10 or 3.16 is taken and the 10/1 range then becomes 2 ranges of 3.16/1 each. The required resistors then vary in steps of 3.16. It is convenient to select low values of  $9.7 \times 10^6$  ohms from resistors rated  $10 \times 10^6$  and high values of  $3.1 \times 10^6$  ohms from resistors rated  $3 \times 10^6$ . The tuning condenser has been padded by the author to give a range of about 3.5/1 instead of the exact value 3.16/1 in order to obtain a suitable overlap between ranges.

#### Calibration

The tuning condenser can be calibrated by the usual methods with an oscilloscope, using Lissajou figures with 60 cycles from the power line as a standard for the lower frequencies. Higher frequencies could use the 440 and 4000 cycles of the standard broadcasts from WWV or the harmonics of 60 cycles if a stable auxiliary audio oscillator is available on which to set up intermediate frequencies.

A convenient method of using WWV signals is to pick up the 5, 10, or 15 mc signal on a receiver and use the audio output to synchronize the CRO sweep.

[Continued on page 74]

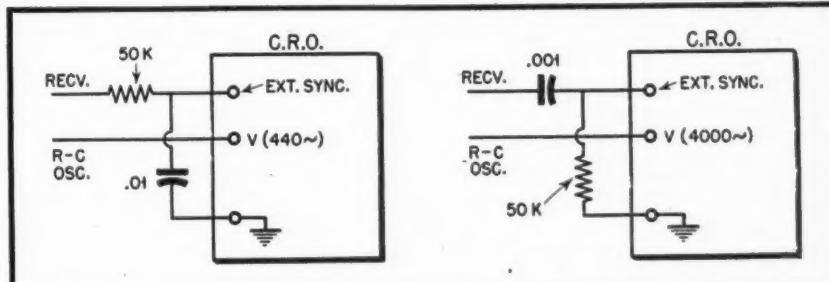


Fig. 8. Simple filter arrangements for using 440 and 4000 cycle signals of station WWV for calibrating the R-C oscillator

$R_p$   
C network  
where  
 $/C_p$

# Application of METALS in RADIO

**I**T IS SURPRISING to find in the radio engineering profession so many well qualified designers who have little knowledge of metals and their use in radio design. While it is true most radio engineers find such knowledge is not necessary, it is nevertheless an asset to be able to appreciate the metal problems encountered by the mechanical designer. Such understanding leads to better cooperation between groups and may often improve the quality of the overall design.

The object of this article is to explain for the radio engineer the various properties of those metals commonly employed in radio receiver design. Methods of fabrication and requirements for mechanical strength and prevention of corrosion will also be discussed. In an article of this length it is obviously impossible to cover the field in great detail; only the points with which the electrical design engineer should be ac-

quainted will be considered. If the need arises, more comprehensive information is readily available in texts on the subject. For convenient reference, Table 1 has been prepared to show at a glance characteristics of metals commonly used in the majority of present-day designs. To simplify the picture, many of the infrequently used metals and alloys have been purposely omitted.

For convenience we will divide the metals and their alloys into two groups: ferrous and non-ferrous. But before we specifically consider these materials, let us define some of the terms commonly used in order to establish a common ground for further discussion.

### Mechanical Properties

The *tensile strength* of a metal is determined by the force in pounds per square inch (psi) which will rupture the metal. This property is of little interest in the design of most radio equipment since the metals are seldom subjected to stresses of such large magnitude. Before the point is reached where rupture occurs the metal stretches or elongates. The degree of elongation is a measure of the stiffness or rigidity and is commonly known as the *modulus of elasticity*. The greater the modulus, the heavier the load a metal will withstand before bending occurs. As the force applied to a test specimen is increased, a point will be reached where the metal will permanently deform (not return to its original shape when the load is removed). When the permanent elongation reaches 0.5 per cent, the force applied in psi is a measure of the yield strength. This property together with the modulus of elasticity is important in choosing the material for levers,

**A. C. MATTHEWS**

TABLE 1

MATERIAL	MECHANICAL PROPERTIES				PHYSICAL PROPERTIES			
	FORM	YIELD STRENGTH 1000 PSI	HARDNESS BRINELL	TENSILE STRENGTH 1000 PSI	SPECIFIC GRAVITY	COEFF. LIN. EXPANSION $10^6''/\text{°F}$	ELECTRICAL RESISTIVITY OHMS/CIR. MIL FOOT	MODULUS ELASTICITY $10^{-6}$ PSI
ALCOA 25	COLD ROLLED <sup>1</sup>	21	44	24	2.72	13.8	17.6	10.3
ALCLAD 24S	ANNEALED <sup>3</sup>	41		62	2.77	13		10.3
COPPER	ANNEALED COLD ROLLED	10 48	30 120	31.8 60	8.92	9.8	10.4	16
BRASS (HIGH)	COLD ROLLED <sup>1</sup>	75	180	86	8.47	11.2	40	14
PHOSPHOR BRONZE	COLD ROLLED <sup>1</sup>	75	210	100	8.86	9.9	57	15
ZINC	COLD ROLLED <sup>2</sup>	21	40	36	7.15	16.5	36	12.4
CARBON STEEL SAE 1020	ANNEALED COLD ROLLED	40 75	130 146	58 81	7.86	6.7	60	29
STAINLESS STEEL 309	ANNEALED COLD ROLLED	50 110	165 275	100 150	7.90	8.3	470	29
INVAR	ANNEALED	42	130	70	8.09	0.6	480	21
SILVER	COLD ROLLED <sup>1</sup>	40	90	51	10.5	10.6	9.6	10.3
MAGNESIUM	CAST	12	48	28	1.83	15.5	69	6.25
DOWMETAL H	ROLLED		33	25				
1-HARD TEMPER		2-LONGITUDINAL TEST				3-HEAT TREATED AND AGED		

# 0 RECEIVER DESIGN

## Practical data on the use of metals in radio design

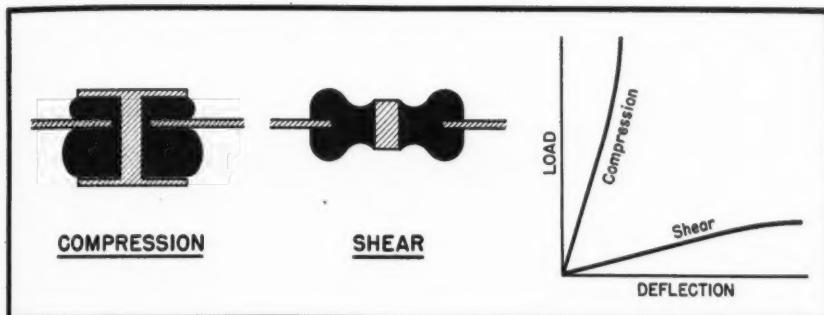


Fig. 1. Rubber shock mountings in compression and shear

om sub-  
magni-  
1 where  
ches or  
ation is  
dity and  
ulus of  
lus, the  
ithstand  
orce ap-  
eased, a  
the metal  
return to  
d is re-  
elonga-  
orce ap-  
he yield  
ner with  
important  
levers,

springs, etc. The higher the modulus the stronger the part, or if size is a factor the smaller the part for a given strength or stiffness.

Another property that is important in some design applications is *ductility*, because this is a measure of the ability of the metal to absorb sudden overloads or shocks; lack of ductility is brittleness. Two materials may have equal strength and hardness but different ductility and therefore one may be more suitable for bending, drawing or other cold working because it has the ability to "take it" without fracture. Obviously such a characteristic is important in the choice of the method of fabrication.

*Hardness*, although it is difficult to measure or define, is one of the three properties of a metal (ductility and toughness being the other two) to be considered where long life and wear are important requirements. Several methods of testing hardness are commonly employed depending upon the part to be measured. Since the Brinell and Rockwell methods are the most popular in most radio applications, only these two will be described.

The Brinell method consists of measuring the penetration of a standard hardened steel ball of 10 mm. diameter into a flat surface of the test specimen with a standard load for a prescribed

length of time. (3000 kg for 15 to 30 seconds for hard metals, 500 kg from 30 to 60 seconds for soft metals). The diameter of the indentation is converted to a Brinell Hardness Number by referring to a special table supplied for the instrument.

The Rockwell hardness is determined from a measure of the depth of penetration into the material due to a steel ball or diamond cone under a fixed load. A preliminary load of 10 kg is first applied to obtain an initial zero setting. The major load is then applied (major load depends on the nature of the material to be tested) until penetration into the test specimen ceases. The latter penetration is a measure of the Rockwell Hardness and is indicated by a pointer on the instrument as a hardness number.

*Fatigue* is another term that has become increasingly important in the design of metal parts subjected to a dynamic load, shock or vibration. When a metal part is subjected to repeated loads, though none exceeds the elastic limit of the material, it may eventually fail due to fatigue. Whenever possible, accelerated life tests should be made on the part or parts in question. Such tests indicate the suitability of a particular design and are of great importance in determining safe operating conditions for such parts.

## Physical Properties

Specific gravity, resistance, density, and the melting point are properties too well known to describe further. But the temperature characteristics are important because radio equipment designed for airborne use frequently must function at sub-zero temperatures. Not only are sub-zero temperatures encountered in such applications but usually they are accompanied by severe vibration and strains. If the metal becomes brittle and loses its toughness, failure is generally imminent.

Another effect of variations in temperature is the change in magnetic properties of a non-ferrous metal. Below a certain temperature, known as the Curie point, non-ferrous metals become magnetic. Such behavior often will result in undesirable effects and therefore this characteristic should be known before specifying a metal for a part whose operation is dependent upon definite non-magnetic properties.

Besides the above properties the *coefficient of expansion* is also of importance. This is particularly true where a change in physical dimensions will cause distortion of the part and either directly or indirectly cause the frequency of a tuned circuit to vary. The coefficient of expansion of a metal is determined by measuring the total expansion over a range of temperatures and dividing the expansion by the degrees change in temperature. It is expressed as parts per inch, per inch, per degree temperature. Frequently it is possible to choose metals having coefficients of expansion which, in a specific design, will compensate the effects of one another. This is especially true in the design of variable tuning condensers and coils.

## Non-Ferrous Metals

Since copper, aluminum, magnesium, zinc and their alloys are the most commonly used non-ferrous metals in radio equipment design, we will confine ourselves to brief descriptions of these metals only.

COPPER has a tensile strength of

DULUS	STICITY
6	PSI
10.3	
10.3	
16	
14	
15	
12.4	
29	
29	
21	
10.3	
6.25	
RADIO	

30,000 to 65,000 psi depending upon the treatment to which it has been subjected. It is fairly free from corrosive effects because in dry air a thin film of cuprous oxide is formed, and in moist air a green basic carbonate forms which is protective in nature. Copper is an excellent conductor of electricity and because it can be readily worked it finds many uses in radio, such as shields, wire and even castings if properly alloyed with other metals.

Copper alloys are divided into the brasses and bronzes. BRASS, an alloy of copper and zinc has excellent mechanical properties, is quite corrosion resistant and is readily machined. Its strength and toughness depend upon the percentage of zinc used and the mechanical and heat-treatment received.

BRONZE is an alloy of copper and tin and, like brass, its properties depend on the particular alloy and its treatment. It is chiefly used for castings, although it can be rolled satisfactorily. The addition of phosphorus to bronze greatly improves its characteristics especially in tensile strength, elasticity and

fatigue resistance. It can be readily forged, drawn, cold rolled and cast, and since it is comparatively corrosion resistant, it is often substituted for steel in the manufacture of corrosion-resistant parts.

Because ALUMINUM is one of the lightest of metals and relatively strong and tough, possesses high electrical conductivity and under ordinary atmospheric conditions forms a protective oxide coating, it is widely used in the manufacture of radio equipment. Where lightness and extreme strength are required, as in airborne equipment, some of its alloys are particularly suitable. For instance, Alclad 24S when properly treated has a tensile strength of 62,000 psi. This is comparable with mild steel in strength yet only about one-third the weight.

MAGNESIUM is the lightest of the metals (approximately 0.7 that of aluminum) used in radio applications. Although its tensile strength is comparable to that of aluminum it is somewhat harder. It may be alloyed with aluminum, zinc, manganese, cadmium and

copper; in fact, most metals with the possible exception of iron and chromium. These alloys are becoming increasingly important for use in airborne equipment since they can be rolled, extruded or cast.

ZINC is primarily used as a coating for other metals. It can, however, be rolled or cast satisfactorily and is therefore used for coil and tube shields, although it is not as satisfactory as aluminum or copper for this purpose. As an alloy with aluminum and copper, it is particularly suitable for die-castings. Its low cost and the fact that its dimensions can be held within plus or minus 0.002" per inch of casting makes it suitable for many applications. As a die-casting it is quite tough and less likely to breakage in handling or service compared with some of the other alloys. Wherever an intricate piece is required a zinc alloy die-casting should be considered.

#### Ferrous Metals

There is a wide variety of steels to choose from in the design of radio equip-

TABLE 2

COMMONLY USED FINISHES				
TYPE (ELECTROPLATED)	PROTECTION	THICKNESS IN INCHES (MIN)	SALT SPRAY (HOURS)	REMARKS
CADMIUM	MILD EXPOSURE	0.0002	50	ON STEEL
CADMIUM	SEVERE EXPOSURE	0.0005	100	MEETS AN SPECS
CADMIUM	VERY SEVERE	0.001	200+	REQD ONLY FOR UNUSUAL CONDITIONS
ZINC	MILD	0.0002	35	NOT TO BE PAINTED OR SOLDERED
* ZINC	SEVERE	0.0005	100	CAN BE PAINTED
ZINC (BRIGHT)	VERY SEVERE	0.0007 TO 0.0009	150	
ZN (OX BLACK)	MILD	0.0002	35	0.0002" DEPOSIT BEFORE OXIDIZING
SILVER		0.00012 TO 0.00018		LOW ELECTRICAL RESISTANCE
SILVER		0.0003		LOW ELECTRICAL RESISTANCE CAN BE SOLDERED
NICKEL	SEVERE	0.0014	48	ON STEEL
NICKEL	SEVERE	0.0003		ON BRASS
BLACK NI.	SEVERE	ZN OR CD BEFORE NI.	50	RUST RESISTANT BLACK
WHITE NI.		0.0012	50	ON BRASS
FLASH COPPER	NONE	0.00008		UNDERCOAT BEFORE NICKEL
COPPER	MILD	0.0002		
ANODIZED ON ALUMINUM	SEVERE			EXCELLENT FOR SALT SPRAY ELECTROLYTIC MEANS
BLACK ANODIZE	SEVERE			DURABLE BLACK FINISH
CHEMICAL FINISHES NOT ELECTROPLATED				
BONDERITE	TREATMENT FOR ZINC TO IMPROVE PAINT ADHESION			
LITHOFORM	USED ON HOT GALVANIZING TO IMPROVE PAINT ADHESION			
BONDERIZING	ON STEEL BEFORE PAINTING			
PARKERIZE	ON STEEL BEFORE PAINTING			
CRONAK	ON ZINC FOR ADDITIONAL PROTECTION			
SHERARDIZE	ZINC IRON ALLOY COATING BY CEMENTATION			

ment, but for most applications ordinary carbon steel is very satisfactory because it can be readily formed and finished and has excellent mechanical properties. The carbon content of a steel is extremely important and for this reason a method of classification or identification has been standardized by the Society of Automotive Engineers. Each carbon steel is assigned a series of four digits; the first digit for all carbon steel is 1, the second digit represents the type of carbon steel (0 for plain, 1 for free cutting, etc.) and the last two digits indicate the percentage carbon content in hundredths of one per cent. Thus SAE 1010 is plain carbon steel having approximately .010 per cent carbon content.

Steel alloys are used only where special characteristics are required, as for instance silicon electrical steel for transformer laminations, or some of the stainless steels where freedom from corrosion is desired. These special applications are outside the scope of this article and therefore will not be discussed.

A metal or alloy is made up of a great number of small crystals arranged at random. Their properties are dependent upon the treatment and working to which they are subjected. In the process of manufacture the rate of cooling determines to a large extent the size of the crystals formed. (Slow cooling will generally result in large crystals which produce a weak material. On the other hand, rapid cooling is likely to produce a less ductile material.)

The cold working of a metal will increase its hardness and strength at the expense of ductility. This can be seen by bending a piece of soft metal with the hands and then trying to straighten it out again. While it bends easily it is very difficult to straighten. Apparently the bending distorts the crystalline structure in some manner and a structural change occurs which increases its rigidity or hardness. If a piece of cold rolled or drawn metal which has been distorted is examined under a microscope, the crystals or grain will appear to have fine parallel lines running through them. These lines are caused by a movement of the crystals and are known as slip planes. So long as the slipping occurs the metal will not fracture, but as soon as the limit of slipping is reached, the metal will break.

Once the metal has been hardened by cold working, the crystals remain in their distorted condition until the metal is heated to a high temperature, known as the annealing point. At this point the crystals are relaxed and regain their symmetry. (An annealed part must be allowed to cool slowly). Annealing makes the metal soft and more workable, at the expense of its hardness and strength.

Hot working is a combination of an-

nealing and cold working, wherein the grain size is decreased but the crystals retain their symmetry and no strain is apparent. This results in some hardening and strengthening without loss of ductility.

### Design Notes

Chasses and other metal parts for radio equipment are generally fabricated from steel, although aluminum is widely used for airborne equipment where weight is an important factor. As mentioned previously there are many grades of steel available and accordingly it might seem difficult to choose the correct type. The requirements, however, are fairly well defined; that is, a metal is required that has a good surface for finishing, is capable of being easily formed, and low in cost. Many companies specify half-hard cold rolled automobile body steel. This has an excellent finish and is not too hard for working. In general, cold rolled steel is specified rather than hot rolled because the former takes a smoother finish or plating. Very few companies specify the actual composition of the metal they purchase, but they do specify what it will be used for and leave the details as to composition etc., to the supplier.

Aluminum, magnesium, brass, bronze and copper are specified in the B & S gage while steel is specified in the

U.S.S. gage. The gage or thickness varies of course with the size of the part to be fabricated. In general, small chasses or parts use 0.037" material, medium sized 0.050" and the larger chasses 0.062". This of course varies with the actual design of the part. For example, if the chassis has large cutouts, which obviously would weaken the unit, then it would appear that a heavier gage material should be used than if the cutouts were small. Unfortunately this is not always the case; it may be much more economical to fold and weld the corners or add strengthening ribs at the weak spots rather than use a heavier material. While it is true such designs necessitate extra operations which add to the piece price, nevertheless the dies for blanking and forming the lighter material are not quite as expensive and will produce more parts before wearing out.

No hard and fast rules are available with which to make this decision as each design must be considered individually. An experienced cost estimator, in collaboration with a qualified tool designer and a representative of the purchasing department, usually make such decisions. Where the design is quite similar to a previously produced part the mechanical design engineer can of course rely on his past experience for the answer.

The cost of a unit can often be reduced by eliminating extra brackets. Separate mounting brackets which must be riveted or welded on the chassis can, in many cases, be eliminated by piercing and folding a suitable piece of metal from the chassis. Of course, the opening in the chassis must be such that it does not materially weaken the unit and it should be so placed that Underwriters requirements are not violated, where these restrictions apply. Furthermore, in designing a substitute bracket of this type the folding or forming should require no additional operations as these would practically offset any savings.

Where it is necessary to use separate brackets or super-structures on a chassis a saving in the mounting time can often be made, particularly when the bracket is not subject to handling, by omitting one of the mounting holes and substituting a locating dowel in its place. The dowel only positions the bracket and contributes nothing to holding the part so this can only be used where the strength requirements are low.

Another important consideration when designing brackets, particularly where two are required and one must be right-handed and the other left handed, is to make the design such that only one part will be needed. This eliminates extra die cost, the cost of handling an extra part and the avoidance of confusion in production since

TABLE 3

CORRODED END (ANODIC, OR LEAST NOBLE)
MAGNESIUM
MAGNESIUM ALLOYS
ZINC
ALUMINUM 2S
CADMUM
ALUMINUM 17ST
STEEL OR IRON
CAST IRON
CHROMIUM IRON (ACTIVE)
NI-RESIST
18-8 STAINLESS (ACTIVE)
18-8-3 STAINLESS (ACTIVE)
LEAD TIN SOLDERS
LEAD
TIN
NICKEL (ACTIVE)
INCONEL (ACTIVE)
BRASSES
COPPER
BRONZES
COPPER-NICKEL ALLOYS
MONEL
SILVER SOLDER
NICKEL (PASSIVE)
INCONEL (PASSIVE)
CHROMIUM IRON (PASSIVE)
18-8 STAINLESS (PASSIVE)
18-8-3 STAINLESS (PASSIVE)
SILVER
GRAPHITE
GOLD
PLATINUM
PROTECTED END (CATHODIC, OR MOST NOBLE)

the parts are usually quite similar in appearance.

Separate spacers to hold parts in position can often be eliminated by a so-called "embossing" operation on the main chassis. These are relatively easy to include in the die and give very satisfactory results. They cannot, however, be placed too close to a hole in the chassis as the embossing operation tends to pull the metal in such a manner that nearby holes become distorted and very likely would run out of tolerance. The embossing is usually done during the piercing operation.

Another design feature which reduces costs is the use of extrusions or punch-formed holes. These have a variety of applications. For example, where it is necessary to provide a hole in the chassis for lead wires, cables or power cords it is customary to insert a metal or fiber grommet to eliminate the raw metal edge which might otherwise abrade the insulation. An extruded or punch-formed hole can be specified to provide a smooth surface for the wires and thereby eliminates the chances of failure from this cause.

Another use for punch-formed holes is where the mounting of a part would ordinarily require a machine screw, lockwasher and nut. By providing a punch-formed hole, a hardened drive screw can be employed with a saving in both time and material costs. If the part to be mounted requires frequent removal during the life of the apparatus, a self-tapping drive screw can be used, or the punch-formed hole can be tapped and a regular machine screw employed. Punch-formed holes provide extra material for tapping purposes; the engagement of the thread should never be less than its major diameter, even in non-ferrous materials.

Sharp corners on brackets, etc., are to be avoided because of the danger of injury to production personnel. Some designers cut the corners at a  $45^{\circ}$  angle, which is a compromise between safety and cost. A small radius usually increases the die cost while cutting the corners at a  $45^{\circ}$  angle is relatively inexpensive.

Chasses are usually fabricated from sheet metal by stamping, piercing and folding. Sometimes mounting feet and

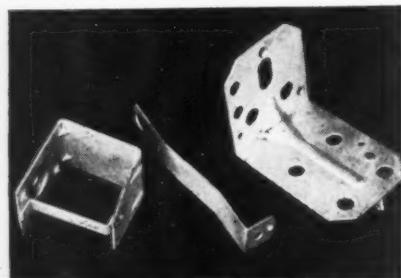


Fig. 3. Examples of strengthening ribs, dowels, spot welds, etc.



(Courtesy Osg Mfg. Co.)

Fig. 2. Silver plating on wave switch contact. Cross-sectional view shows silver deposit of .0001", indicated as a white line at top of photo. Magnification 750.

brackets are formed during the same operations but these cases are limited because of the complexity of the dies. It is therefore usually necessary to rivet several metal parts together to make a complete assembly. For this reason, complicated designs may lend themselves to die-casting. Shields, coil mountings, brackets, and mounting feet can then be made as one integral part without additional assembly operations. Zinc die-casting alloy is ideal for such purposes as it is tough and will withstand rough handling in service, and dimensions can be held extremely close so that very little machining is required.

The material cost of zinc die-castings is slightly higher than steel, but in some designs a cost saving may be apparent because of the fewer operations required to obtain a finished products.

As mentioned previously, riveting is the most common method of assembling a unit, although spotwelding is often employed where the material of the parts to be joined are approximately equal in thickness. Spotwelding or two parts that differ appreciably in thickness is not recommended.

When specifying spotwelding it is important that adequate space be available for performing the operation. Inaccessible spotwelds often require special jigs or fixtures and require additional time which defeats its main purpose, that is, speed in production and decreased cost. Dowels, stamped in the part at the same time the original stamping operation is performed, often can be used in place of holding fixtures thereby saving both time and equipment.

There is no set rule for determining the minimum number of spotwelds required. This is usually left to the judgment of the designer, but it should be clearly specified because of the cost involved. Flanges to be spotwelded should be at least one-half inch wide to avoid coming too close to the edge of the material.

The matter of tolerances is probably one of the most misused details in mechanical design (particularly by radio engineers). Because it is practically impossible to fabricate a part in production quantities to exact dimensions, it is necessary to specify allowable limits or tolerances. This can often be in the form of a general statement as, for instance, "All fractional dimensions are  $\pm 1/64"$ , all decimal dimensions  $\pm 0.005"$ , all angles  $\pm 1^{\circ}$  unless otherwise specified". The assignment of general limits depends upon the function of the part and the interchangeability required.

Tolerances should be as liberal as possible. They should be determined by taking the tightest permissible fit and the greatest allowable clearance, keeping in mind necessary clearances between parts, particularly where such parts are shock-mounted or subject to movement during normal operation, where it is necessary to insert or remove plugs etc. or adjustment may be necessary after assembly. In other words, tolerances are applied to obtain the greatest permissible variation between parts which will allow proper functioning of the assembled unit.

Tolerances should permit ready interchangeability of production parts with a minimum loss in time due to fitting, again keeping in mind that narrow limit are usually costly. After limits are decided question whether, considering the cost of the piece, if a part 0.003" or 0.005" outside of tolerance should be scrapped. Remember close tolerances are expensive and should only be specified when absolutely necessary. If possible the tolerances should be specified in the direction which permits reworking of the part should it be outside specified limits.

### Shock Mountings

In radio equipment design it is often necessary to provide some isolating medium between certain parts to prevent them from periodically changing value so as to cause undesirable microphonism. Sometimes it is necessary only to isolate a single stage or a single part, as for example the variable tuning condenser. In general, however, the entire unit is isolated from its cabinet or case. Considering the problem from a structural standpoint, where heavy parts such as power transformers, speakers and chokes are mounted in the center of a chassis, some means of isolation between chassis and cabinet may be necessary to prevent excessive vibration from causing structural failures.

Adequate mountings spaced well apart will go a long way in reducing vibration effects. Ribs, flanges, embossings and welded sections as

[Continued on page 66]

# THE FCC REPORT

**So much controversy has arisen regarding the action of the Federal Communications Commission in changing the FM frequency allocations that we believe this statement by the Commission deserves careful consideration**

**O**N MAY 25, 1945, the Commission made public its final report of allocations above 25,000 kilocycles, except for the region of the spectrum from 44 to 108 megacycles. With respect to this region, the Commission proposed three alternative allocations for FM, television, facsimile non-government fixed and mobile services, and the amateur service. In its report, the Commission stated that the final decision among the three alternatives could be made with a great deal more assurance if more factual data were available. The Commission also pointed out that a program of experimentation during the summer months designed to collect further data was possible, since the War Production Board had assured the Commission that the radio industry would not resume production of AM, FM, and television transmitters and receivers in 1945 or even in the first part of 1946 unless Japan capitulated, and that the War Production Board would give the Commission 90 days' advance notice in the event of any change in its production estimates.

However, in view of the fact that the War Production Board subsequently advised the Commission that the manufacture of AM, FM, and television transmitters and receivers might commence at an earlier date than was originally indicated to the Commission, and that it would probably not be possible for the War Production Board to give 90 days' advance notice to the Commission before production was resumed, the Commission on June 5, 1945, ordered a further argument and hearing in order that a final decision might be reached at the earliest possible date. Such a hearing was held on June 22 and 23, 1945, marking the culmination of an extended series of hearings and oral arguments which began in September, 1944.

As the Commission noted in its report of May 25, 1945, its primary concern in making allocations between 44 to 108 megacycles is that FM shall be assigned the frequencies best adapted to its needs. All of the other services for which provision is made in this portion of the spectrum, have allocations in other portions of the

spectrum, so that they are not wholly dependent upon their assignments here. FM, on the other hand, is receiving assignment only in this portion of the spectrum, and accordingly it is essential that it receive an allocation which will give a permanent locus, as free as possible from interference and other shortcomings.

The three alternatives proposed for FM are:

- (1) 50-68 megacycles
- (2) 68-86 megacycles
- (3) 84-102 megacycles

There was unanimity that alternative No. 2 (68-86 mc) is completely unfeasible. Accordingly, the choice lies between alternatives Nos. 1 and 3.

The primary objection to alternative No. 1 is the amount of skywave interference which will result among FM stations if FM is placed in the 50-68 megacycle region. The nature and extent of this anticipated interference was set forth in great detail in Section 8 of the Commission's report of May 25, 1945 (pp. 49-72). The tables showing such interference are reproduced at the end of this report. For example, interference among 50 kilowatt FM stations at 58 mc from sporadic E transmissions alone, assuming a 10/1 ratio of desired to undesired signal and full oc-

**TABLE I**  
**APPROXIMATE HOURS PER YEAR OF INTERFERENCE AT THE 50  $\mu$ V/M CONTOUR FROM SPORADIC E LAYER TRANSMISSIONS\***

A. 50 kw stations with an antenna power gain of 6 (300 kw effective radiated power)				
mc.	2:1 ratio, one co-channel station (hours)	2:1 ratio, full channel occupancy (hours)	10:1 ratio, one co-channel station (hours)	10:1 ratio, full channel occupancy (hours)
43	132-298	660-1490	166-482	830-2410
58	22-56	110-280	28-96	140-480
48	75-166	375-830	95-280	475-1400
66	8.9-23	44.5-115	11-38	55-190
84	1.1-3.1	5.5-15.5	1.3-5.1	6.5-25.5
104	0.1-0.32	0.5-1.6	0.13-0.52	0.65-2.6

B. 1 kw stations with no antenna gain				
mc.	2:1 ratio, one co-channel station (hours)	2:1 ratio, full channel occupancy (hours)	10:1 ratio, one co-channel station (hours)	10:1 ratio, full channel occupancy (hours)
43	0.58-0.87	2.9-4.35	57-86	285-430
58	0.1-0.16	0.5-0.8	9.7-15	48.5-75
48	0.33-0.51	1.65-2.55	33-49	165-245
66	0.03-0.07	0.15-0.35	3.8-6.1	19-30.5
84	less than 1 min.	less than 1 min.	0.5-0.87	2.5-4.35
104	less than 1 min.	less than 1 min.	0.05-0.087	0.25-.43

\*Based upon measurements and methods previously described.

**TAB**  
**APPROXIMATE HOURS PER YEAR  
 $\mu$ V/M CONTOUR FROM SPORADIC E LAYER TRANSMISSIONS\***

A. 50 kw stations with an antenna power gain of 6 (300 kw effective radiated power)		
mc.	2:1 ratio, one co-channel station (hours)	2:1 ratio, full channel occupancy (hours)
43	95-173	475-865
58	16-32	80-160
48	54-100	270-500
66	6.4-13	32-65
84	0.75-1.7	3.75-8.5
104	0.07-0.18	0.35-0.9

B. 1 kw stations with no antenna gain		
mc.	2:1 ratio, one co-channel station (hours)	2:1 ratio, full channel occupancy (hours)
43	Negligible	Negligible
58	Negligible	Negligible
48	Negligible	Negligible
66	Negligible	Negligible
84	Negligible	Negligible
104	Negligible	Negligible

\*Based upon measurements and methods previously described.

# ON FM

cupancy of the channel, might be expected for 140 to 480 hours per year at the 50 microvolt contour from stations 900 and 1000 miles distant, respectively. At 84 mc, in contrast, interference under these conditions would be anticipated for only 6.5 to 25.5 hours per year. It should be noted that the 140-148 hours per year of anticipated interference would not be spread out evenly throughout the entire year but that the great bulk of it would be concentrated in two or three summer months.

The existence and extent of such sporadic E interference is not merely a matter of abstract calculation. In addition to the measurements of such interference made by the Commission, there is the experience of the amateurs, who have heretofore utilized both the 56-60 mc and the 112-116 mc bands. Mr. Grammer of the American Radio Relay League stated that there have been thousands of communications via sporadic E in the 56-60 mc amateur radio band but that there have been no recorded instances of such transmission in the 112-116 mc band (CI, Tr. 144).

The amount of sporadic E interference will vary with the particular frequency involved, the power of the transmitters, the distance between transmitters, the number of transmitters on a channel, and other

Height of Transmitting Antenna (ft.)	Height of Receiving Antenna (ft.)	Power in Kilowatts	Frequency in Megacycles	Separation in Miles For Ratio of Desired to Un- desired Signal Shown	
				2/1	10/1
500	30	300	58	257	290
500	30	300	66	259	295
500	30	300	104	276	306
1000	30	300	58	271	312
1000	30	300	66	272	313
1000	30	300	104	281	319
500	30	1	58	98	170
500	30	1	66	100	176
500	30	1	104	104	193
1000	30	1	58	121	183
1000	30	1	66	123	187
1000	30	1	104	132	213

factors; but regardless of these factors, the region of the spectrum above 84 mc is markedly superior to the region below 68 mc with respect to sporadic E.

In addition to this interference from sporadic E transmissions, interference from F2 transmission at 53 mc may be anticipated for as many as 470 hours per sunspot cycle—concentrated in a period of three years—in the case of a sunspot cycle the same as the last one, or interference may exist for as much as 2,650 hours per sunspot cycle if the next sunspot cycle is as severe as the highest on record. These figures for F2 transmission, it should be noted, assume only two stations on a channel; more than two stations on a channel would double or treble the number of hours during which F2 interference

would be expected at 53 mc. In contrast, no F2 interference whatever is to be anticipated above 84 mc.

For listeners buying FM receivers in reliance on a belief that FM is an interference-free service, these figures are extremely serious. They mean, for example, that a listener tuned to a station which is carrying the program of his choice may suddenly find, either that the program to which he has been listening is being interfered with by a station hundreds or even thousands of miles away, or else that control of his receiver has been seized altogether by a distant station completely obliterating the desired program of the local station. These distant transmissions, moreover, are sporadic in nature, with the

[Continued on page 58]

## TABLE II OF INTERFERENCE AT THE 100 MICROVOLT LAYER TRANSMISSIONS\*

antenna power gain of 6 (radiated power)		
occupancy	10:1 ratio, one co-channel station (hours)	10:1 ratio, full channel occupancy (hours)
157-429	785-2145	
27-81	135-405	
90-247	450-1235	
10-33	50-165	
1.2-4.5	6.0-22.5	
0.12-0.46	0.6-2.3	

no antenna gain	
18-22	90-110
3.1-4.1	15.5-20.5
10-13	50-65
1.2-1.7	6-8.5
0.15-0.23	0.75-1.15
0.013-0.024	0.065-0.120

previously described.

## TABLE III APPROXIMATE HOURS PER YEAR OF INTERFERENCE AT THE 200 MICROVOLTS/MILE CONTOUR FROM SPORADIC E LAYER TRANSMISSIONS\*

A. 50 kw stations with an antenna power gain of 6 (300 kw effective radiated power)				
mc.	2:1 ratio, one co-channel station (hours)	2:1 ratio, full channel occupancy (hours)	10:1 ratio, one co-channel station (hours)	10:1 ratio, full channel occupancy (hours)
43	47-70	235-350	139-333	695-1665
58	8-13	40-65	24-63	120-315
48	27-40	135-200	80-192	400-960
66	3.2-5.3	16-26.5	9.4-25	47-125
84	0.38-0.7	1.9-3.5	1.1-3.5	5.5-17.5
104	0.03-0.07	0.15-0.35	0.1-0.36	0.5-1.8

B. 1 kw stations with no antenna gain				
mc.	Negligible	Negligible	1.8-2.5	9-12.5
43	Negligible	Negligible	0.3-0.46	1.5-2.3
58	Negligible	Negligible	1-1.4	5-7
48	Negligible	Negligible	0.12-0.19	0.6-0.95
66	Negligible	Negligible	0.015-0.02	0.075-0.1
84	Negligible	Negligible	0.0013-0.002	0.0065-0.01
104	Negligible	Negligible		

\*Based upon measurements and methods previously described.

s For  
o Un-  
own

0/1

290  
295  
306

312  
313  
319

170  
176  
193

183  
187  
213

contrast,  
to be an-

eivers in  
interfer-  
are ex-  
example,  
which is  
oice may  
ogram to  
being in-  
dreds or  
or else  
een seized  
completely  
on of the  
missions,  
with the  
page 581

E 200  
NS\*

o, full  
cupancy  
)

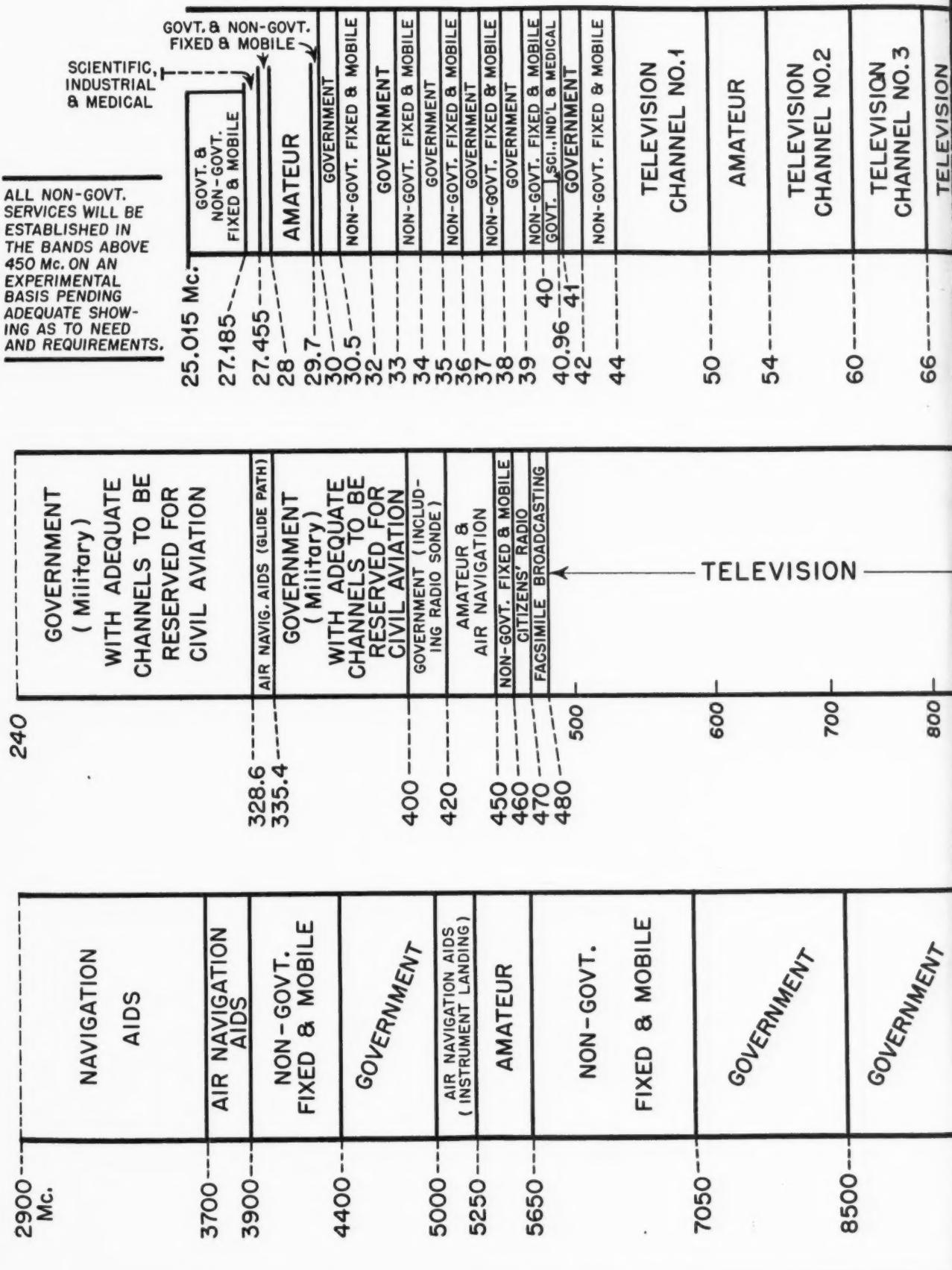
01

RADIO



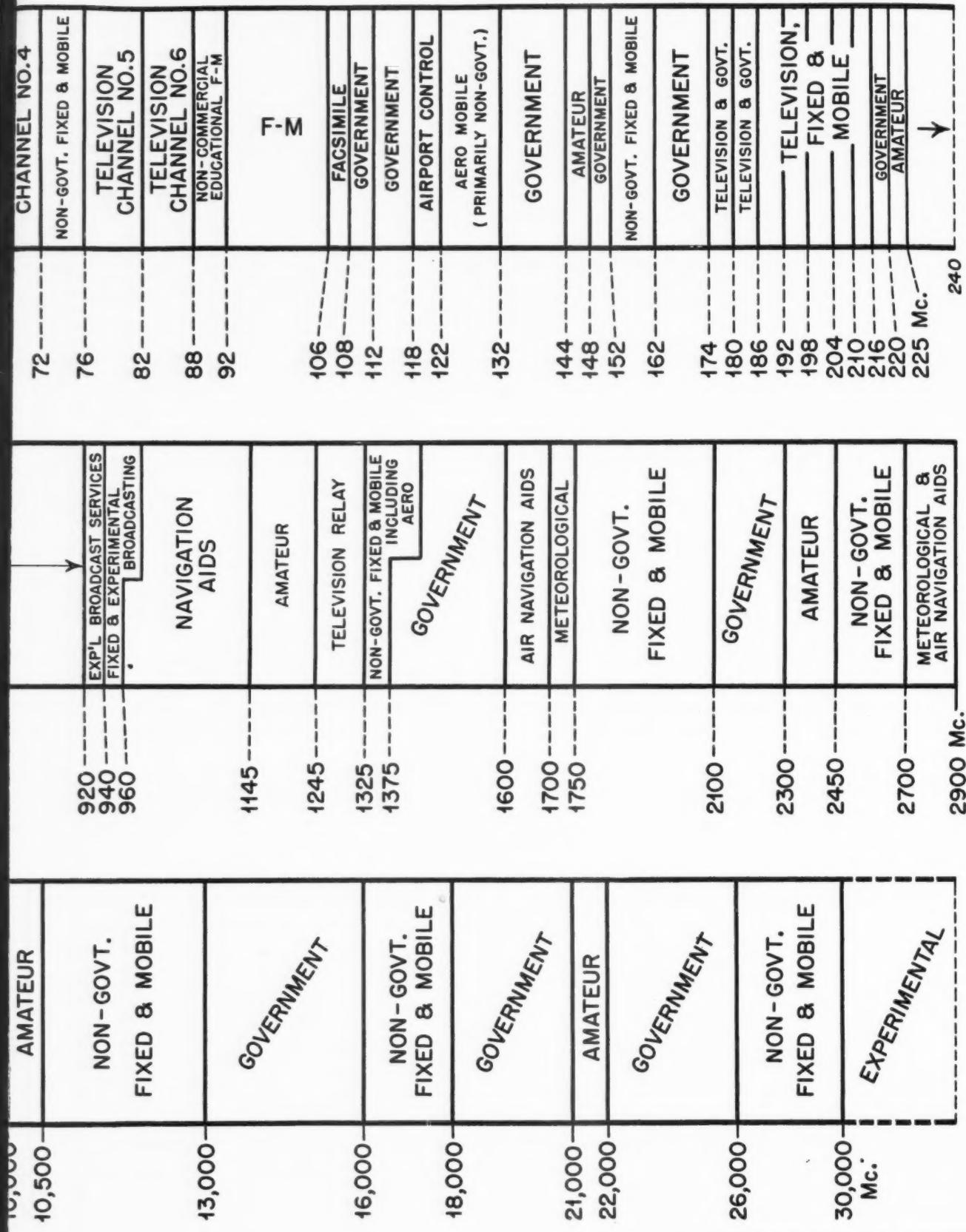
# FREQUENCY ALLOCATIONS

25 Megacycles TO



# LOCATION CHART

## 30,000 Megacycles



Copyright 1945 by RADIO MAGAZINES INC., New York, N.Y.

# A Circuit For PHASE MODULATION

BERNARD GROB

This article describes a new phase modulation circuit which has proved successful in a commercial transmitter

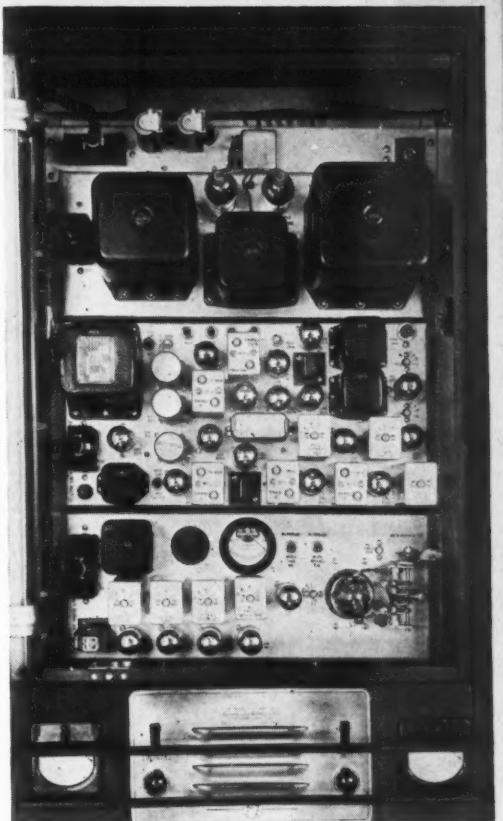


Fig. 1. Link Type 1498 FM Relay Station, 50-watt transmitter-receiver using crystal frequency control

AS THE USE of frequency modulation has increased, new and interesting methods for accomplishing frequency modulation have been developed. One of these is the phase modulator circuit employed in the transmitter component of the Fred M. Link Model 1498 Relay Station. The equipment is shown in Fig. 1, the complete unit consisting of an f-m transmitter, f-m receiver, and transmitter power supply, all mounted on a relay rack in one cabinet. In Fig. 2 is shown the remote control unit that can be used to control the equipment from a remote position.

The schematic diagram of the phase modulator circuit is illustrated in Fig. 3. One section of the 7F7 twin triode is used for the modulator, the other triode section, (not shown), serving as a crystal controlled oscillator.  $T_1$  is the microphone transformer.  $L_1$  and  $C_2$  form

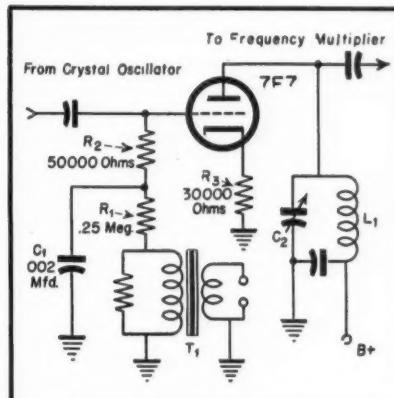


Fig. 3. Schematic of phase modulator circuit

the plate tank circuit, tuned to the oscillator frequency.  $R_2$  is the grid load resistor, and  $R_s$  is the unby-passed cathode resistor.  $C_1$  and  $R_1$  make up an audio corrector circuit whose function will be explained later. This compact circuit has the advantage of simplicity plus the frequency stability of crystal control, in addition to the many advantages inherent with frequency modulation.

In this circuit the radio-frequency signal from the crystal oscillator is shifted in phase by an amount proportional to the audio modulation voltage, resulting in a phase-modulated output. This phase modulation is accomplished by means of an output voltage across the plate tank circuit which is the re-

sultant of two voltages of different phase. One is due to the amplification of the tube, and the other is due to the inter-electrode capacitance between grid and plate. The phase of this latter voltage is shown in the simplified diagram of Fig. 4. Here, the grid voltage acts as a generator,  $E_g$ , the grid-plate capacity as  $C_{pg}$ , and the plate load is the resistance,  $R_L$ , since the tank circuit is tuned to resonance. In this a-c circuit the capacitive reactance due to  $C_{pg}$  will result in a capacitive current,  $I_c$ , that leads the generator voltage. Let this leading phase angle be 30 degrees. The voltage across  $R_L$  is in phase with the current  $I_c$ . Therefore the voltage across the plate load due to the grid-plate capacitance,  $E_c$ , leads the grid voltage by 30 degrees. Since the plate load is resistive, the voltage across  $R_L$  which is due to the amplification of the tube,  $E_a$ , will be 180 degrees out of phase with the grid voltage  $E_g$ .

## Plate Tank Voltage

The actual voltage across the plate tank,  $E_r$ , is the resultant of  $E_a$  and  $E_c$ , which are 150 degrees out of phase with each other. With the vector lengths for  $E_a$  and  $E_c$  shown in Fig. 5a, the resultant,  $E_r$ , leads  $E_a$  by 60 degrees. This is true so long as  $E_a$  is of constant amplitude. However, when an audio modu-

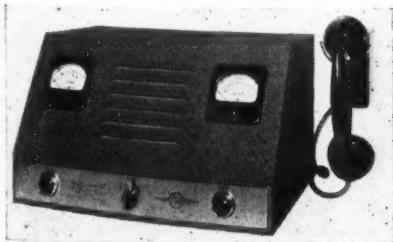


Fig. 2. Remote control desk unit

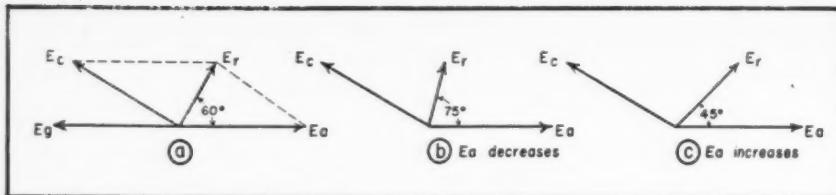


Fig. 5. Vector diagrams of plate tank voltage. See text

lating voltage is impressed on the modulator grid, varying the grid voltage, the amplitude of  $E_a$  is also varied at the audio rate. The resultant voltage,  $E_r$ , will then change in phase as the magnitude of  $E_a$  varies, as illustrated in Figs. 5b and c. In order to produce degeneration, and thereby reduce the magnitude of amplitude variations of  $E_a$ , the cathode resistor is not by-passed. This minimizes the amount of amplitude modulation in the output.

The output radio-frequency signal, then, is phase modulated because its phase with respect to the fixed reference,  $E_a$ , changes in direct proportion to the audio modulating voltage. As shown in Fig. 6, at the positive peak of the audio voltage there is the maximum amount of phase change in one direction. At zero audio voltage there is no change in phase. At the negative audio peak there is the maximum change of phase in the opposite direction. The fixed phase angle "at rest", where  $\phi$  equals 60 degrees,

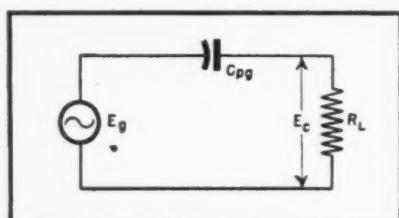


Fig. 4. Phase shift due to tube capacitance

contributes nothing to the modulation, but is merely the starting point for the phase modulation.

#### Mathematical Analysis

This voltage of varying phase can be described by the equation

$$e_r = E_r \sin (\Omega t + \alpha) \quad (1)$$

where  $e_r$  = the instantaneous value of the r-f signal voltage.

$\Omega$  = the angular velocity of the r-f signal voltage.

$\alpha$  = a varying phase angle whose value depends on the audio modulating voltage.

As shown in Fig. 6, this varying phase angle is equal to the fixed angle  $\phi$  plus or minus any change in angle due to modulation. The amount of the change in angle "follows" the audio voltage, and the maximum change in angle is  $\Delta\phi$ . Therefore  $\alpha$  may be written

$$\alpha = \phi + \Delta\phi \sin \omega t \quad (2)$$

where  $\phi$  = the fixed phase angle "at rest"

$\Delta\phi$  = the maximum change in phase angle, which occurs for maximum audio voltage

$\omega$  = the angular velocity of the audio signal

Substituting equation 2 in equation 1

$$e_r = E_r \sin [\Omega t + (\phi + \Delta\phi \sin \omega t)] \quad (3)$$

Equation 3 completely describes this phase modulated radio frequency voltage, with angular velocity  $\Omega$ , maximum amplitude  $E_r$ , initial phase  $\phi$  and a varying phase corresponding to the audio modulating voltage.

This continuous change in phase is equivalent to a change in frequency because there can be no change in one without a change in the other. Further examination of equation 3 will show the connection between phase modulation and the equivalent f.m. Since the general equation for a sine wave is  $e = E \sin \theta$ , the quantity  $[\Omega t + (\phi + \Delta\phi \sin \omega t)]$  must equal  $\theta$  where  $\theta$  is the instantaneous angle through which the vector  $E_r$  has turned, including any change in phase angle. Also, since in general,  $d\theta = \Omega dt = 2\pi F$ ,  $dt$ ,

$$\text{then } F = \frac{1}{2\pi} \frac{d\theta}{dt}. \text{ Therefore, in order to}$$

find the instantaneous frequency due to the changing angle  $\theta$ , it is only necessary to differentiate  $\theta$  with respect to  $t$ .

$$F_i = \frac{1}{2\pi} \frac{d\theta}{dt} = \frac{1}{2\pi} \frac{d}{dt} [\Omega t + (\phi + \Delta\phi \sin \omega t)]$$

$$= \frac{1}{2\pi} [\Omega + \omega \Delta\phi \cos \omega t]$$

$$F_i = \frac{\Omega}{2\pi} + \frac{\omega}{2\pi} \Delta\phi \cos \omega t$$

center frequency      change in instantaneous frequency due to modulation

Note that the change in frequency is proportional to  $f$ , the audio modulating frequency. Therefore, for audio signals of the same amplitude, higher frequencies will give more frequency deviation. In order to correct for excessive fre-

quency deviation at high audio frequencies, and to allow use of the usual f-m detector, an RC circuit is used as an audio corrector circuit to provide an audio modulating voltage that is inversely proportional to the modulating frequency. This RC circuit cancels the  $f$  factor in  $f \Delta\phi \cos \omega t$ , making the frequency deviation dependent only on the amount of phase change, which is pro-

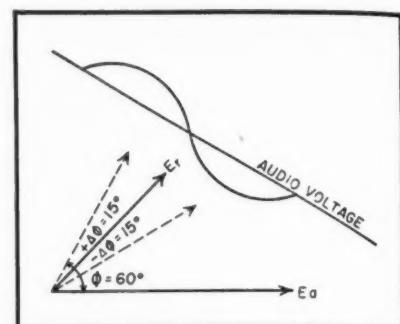


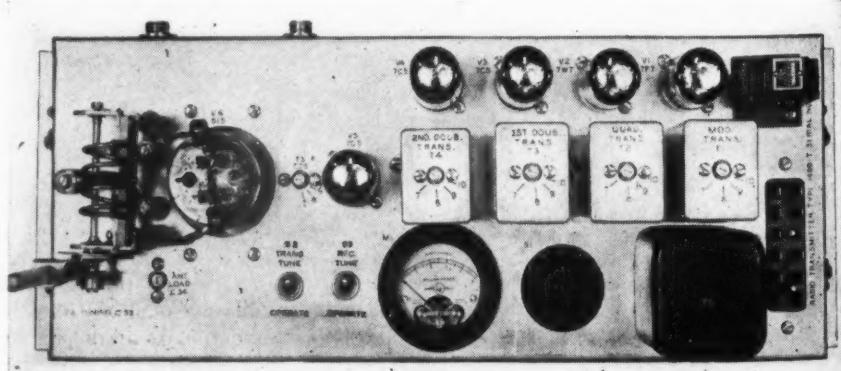
Fig. 6. Phase change is a maximum for positive and negative peaks of audio voltage

portional to the amplitude of the audio voltage.

#### Audio Corrector Circuit

$R_1$  and  $C_1$  form the RC audio corrector circuit. They are connected as a voltage divider across the secondary of  $T_1$ , with  $C_1$  in series with the modulator grid resistor  $R_2$  to ground. Since the small reactance of  $C_1$  at radio frequencies grounds  $R_2$  for radio frequencies, but not for audio, the audio voltage across  $C_1$  is the modulation voltage applied to the grid in series with the radio frequency voltage across  $R_2$  from the crystal oscillator. This audio voltage is inversely proportional to the audio frequency  $f$ , thus correcting the frequency deviation of the radio frequency signal.

In conclusion, then, this phase modulation circuit provides an f.m. signal, with crystal control. In actual operation in the field it has given trouble-free service, with all the advantages of f.m. The equipment has been used in a radio-telephone network with excellent results—stable in operation and free from interference.



Top view of Link power amplifier chassis, type 1498-T

# A Direct Reading

## C-R-L Impedance Bridge

ATHAN COSMAS, Engineer, Station WQXR

Design and constructional data on a useful laboratory instrument

BECAUSE OF THE difficulty of obtaining commercial bridges, such as the General Radio Type 650-A, the author undertook last year the design and construction of a simplified instrument for measuring capacity, resistance, and inductance. This bridge was designed around components which were low in cost and not subject to priorities. Considering these limitations, the results secured were very satisfactory. This instrument was described elsewhere.\*

The instrument to be described utilized the same basic bridge circuits but has greatly improved accuracy and convenience of operation, adapting it to the exacting needs of laboratories. It includes an internal d-c supply, 1000-cycle signal source, and null indicator. Provision is made for using an external null indicator, d-c power, or signal source, by means of switches.

The following bridge circuits are provided:

1. Capacity Bridge (low power factor)
2. Capacity Bridge (high power factor)

\*"An Inexpensive Impedance Bridge", Athan Cosmas, *QST*, July, 1944

Photos for this article by Robert E. Cobaugh.

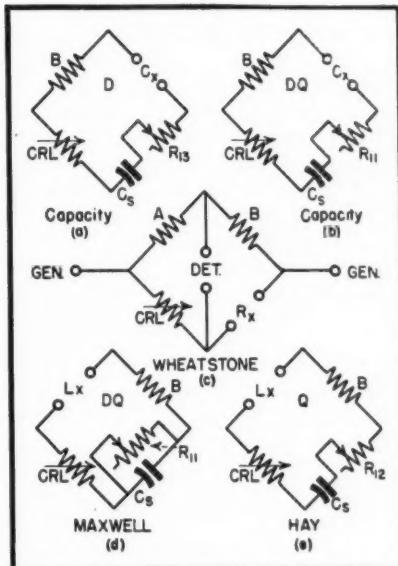


Fig. 1. Fundamental circuits used in impedance bridge

3. Wheatstone Bridge
4. Maxwell Inductance Bridge (low Q)
5. Hay Inductance Bridge (high Q)

These fundamental bridge circuits are illustrated in Fig. 1. By means of a selector switch, any one of these five circuits may be rapidly chosen.

The complete schematic of the bridge is shown in Fig. 2. The switch S<sub>2</sub> is used to select the desired bridge circuit. With this switch in the CD or CDQ position, the circuit is that of a standard capacity bridge. In the R position, it becomes a conventional Wheatstone bridge. The LDQ position provides a Maxwell bridge arrangement for measuring apparent inductance for Qs up to 10. The final position, LQ connects the necessary bridge components to form a Hay bridge, to measure apparent inductance of components with Qs up to 1000.

The range of the CRL Bridge is as follows:

Selector switch	Minimum	Maximum
CD (low p.f.)	1 $\mu\text{f}$	100 $\mu\text{f}$
CDQ (high p.f.)	1 $\mu\text{f}$	100 $\mu\text{f}$
R	1 millionohm	1 megohm
LDQ (low Q)	1 $\mu\text{f}$	100 h
LQ (high Q)	1 $\mu\text{f}$	100 h

### Resistance Measurement

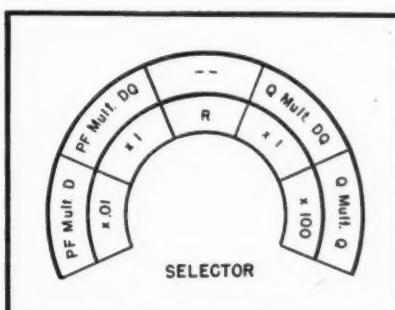
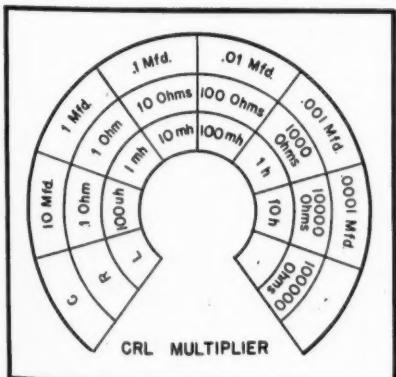
Referring to Fig. 1 (c), the basic circuit for the Wheatstone bridge consists of four resistance arms, the unknown resistance being connected in the R<sub>x</sub> arm. Fixed resistors are employed in two arms, A and B, the values of which are selected by the dual tap switch S<sub>1</sub> (Fig. 2). The third arm is the calibrated variable resistor CRL. A galvanometer (G, in Fig. 2) is used as a null indicator. At balance,

$$A/B = "CRL"/R_x$$

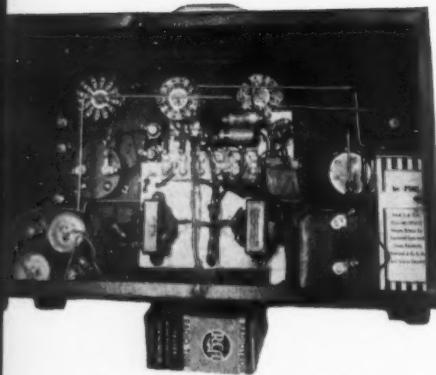
whence

$$R_x = B "CRL"/A$$

In operation, the unknown resistor is connected to the lower left-hand binding posts, S<sub>3</sub> is set at Galv. Shunt, and the generator switch S<sub>4</sub> at DC. The CRL multiplier tap is then adjusted to the proper range, if known. Then press the



Layout for CRL multiplier (left) and (above) selector dials



Bottom view of CRL bridge

push-button ( $S_6$ ), competing the galvanometer circuit. Adjust the CRL dial for zero reading. Then set  $S_3$  to "Galv."

and re-adjust the CRL dial for precise balance. The value of the unknown resistance is read directly from the CRL dial (times the CRL multiplier factor, see Table 1).

#### Capacity Measurement

Referring to Figs. 1 (a) and (b), the reactance of an unknown capacitor  $C_x$  is determined from the expression for bridge balance

$$\frac{B}{1/C_x} = \frac{"CRL"}{1/C_s}$$

whence

$$C_x = \frac{B}{"CRL"} C_s$$

The standard capacitor is  $C_s$  ( $C_2$  in Fig. 2). Table 1 shows the multiplying

factor, as determined by the setting of the CRL Multiplier for direct reading of capacity on the CRL dial.

#### Power Factor

A close approximation of the power factor of a capacitor is given by the ratio  $R/X$ , which is known as the dissipation factor.  $R$  is the equivalent series resistance of the unknown capacitor and  $X$  is its reactance. Assuming the standard to have negligible losses, resistance introduced into the  $C_s$  arm sufficient to afford a sharp balance serves as a means of determining the dissipation factor. When the resistance in the  $C_s$  arm equals that of the  $C_x$  arm, the losses in each arm are equal and the amount of resistance introduced into the  $C_s$  arm is

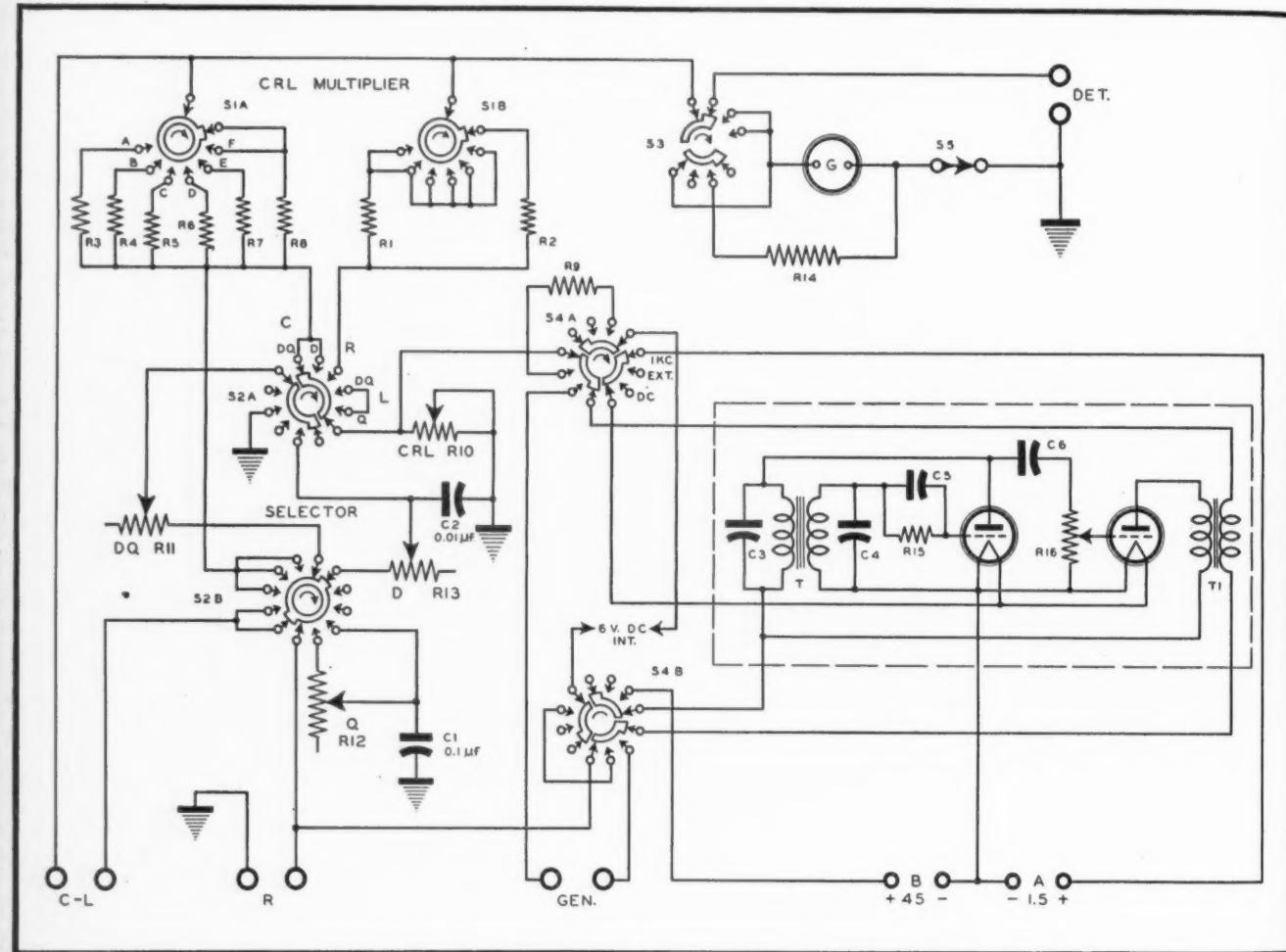


Fig. 2. Complete schematic of the CRL Impedance bridge

#### PARTS LIST

$R_1$	10,000 ohms (#8119)	Ohmite Riteohm Type 81 Precision (1%) Wirewound (Noninductive) See text
$R_2$	1,000 ohms (#8111)	
$R_3$	1 ohms (#8102)	
$R_4$	10 ohms (#8103)	
$R_5$	100 ohms (#8106)	
$R_6$	1,000 ohms (#8111)	
$R_7$	10,000 ohms (#8119)	
$R_8$	100,000 ohms (#8131)	
$R_9$	60 ohms	
$R_{10}$	10,000 ohms, General Radio Type 371-T (See text)	
$R_{11}$	20,000 ohms (Linear taper—wirewound)	Centralab, Clarostat or equivalent
$R_{12}$	200 ohms (Logarithmic taper—wirewound)	
$R_{13}$	2,000 ohms (Linear taper—wirewound)	
$R_{14}$	Galv. Shunt (Will depend upon type of Galv. used.)	
$R_{15}$	1 megohm $\frac{1}{2}$ watt.	
$R_{16}$	.25 megohm pot.	

$C_1$	.1 $\mu$ f	"Bridge selected" (Stacked micas)
$C_2$	.01 $\mu$ f	"Bridge selected" Mica
$C_3$	.25 $\mu$ f	
$C_4$	.015 $\mu$ f mica	
$C_5$	250 $\mu$ uf mica	
$C_6$	.1 $\mu$ f (paper)	
$T$	Stancor "Victory Model" (Core removed)	
$T_1$	UTC S-14 (With 500 ohm output)	
$S_1$	2 Gang, 2 pole, 7 position rotary (Centralab #1413)	
$S_2$	2 Bang, 4 pole, 5 position rotary (Centralab #2515)	
$S_3$	1 Gang, 2 pole, 3 position rotary (Centralab #1405)	
$S_4$	2 Gang, 6 pole 3 position rotary (Centralab #1417)	
$S_5$	Push button, Utah-Carter Type 1s-13	
Cabinet:	7 x 9 x 15 Bud # CU-882	
Galv.:	(Presently using an "off-set" Gruen Microammeter, 150 microamps full scale deflection) See text	

TABLE ONE			
CRL MULTIPLIER		L	
	C ( $\mu$ F)	R (ohms)	L
A	10	.1	100 $\mu$ H
B	1	1	1 $\mu$ H
C	.1	10	10 $\mu$ H
D	.01	100	100 $\mu$ H
E	.001	1000	1 H
F	.0001	10000	10 H
G		100000	—
PF	CD	MULTIPLY BY .01 D	
	CDQ	MULTIPLY BY .1 DQ	
	LDQ	MULTIPLY BY 1 DQ	
	Q	MULTIPLY BY 100 Q	

equivalent to the series resistance of the unknown capacitor in the  $C_s$  arm. This is done by means of the variable resistors  $CD$  ( $R_{12}$ )—2,000 ohms and  $CDQ$  ( $R_{11}$ )—20,000 ohms. The dissipation factor is then determined by substitution in the following formula

$$\text{Dissipation factor} = (2\pi f C) R_s$$

where

$f$  = frequency in cycles of applied voltage

$C$  = capacity of capacitor in farads

$R_s$  = series resistance in ohms

### Inductance Measurements

The Maxwell and Hay bridges differ principally in the range of  $Q$  which may be measured.

Because the impedance of a coil is proportional to its inductance while the

should be remembered that all values of  $CR$  and  $L$  are direct reading on the CRL dial by applying the unit multiplying factors indicated in Table 1.

### Construction

Obviously one of the most important parts of the bridge is the CRL calibrated resistor. The General Radio potentiometer Type 371-T is recommended since it has the required taper by which the low end of the CRL calibration can be opened up. If this is unobtainable a 15,000 ohm Clarostat (Type W) wire-wound potentiometer, shunted by a 41,000 ohm resistor will provide a taper in which the low end can be opened up. This will be adequate but not as desirable as the 371-T. A Clarostat 15,000 ohm Type V might be used without the shunting resistor. Then, too, it is possible to substitute a four section resistance decade for the CRL pot.

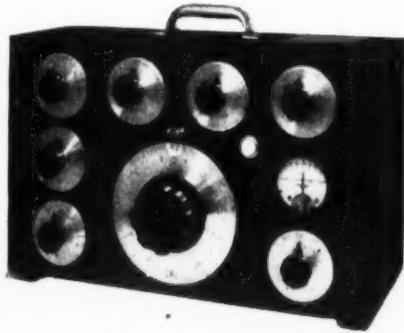
The absolute accuracy of measurements made with the bridge will naturally depend upon the accuracy of the fixed resistors and capacitors used as standards, as well as the accuracy of calibration.

In this instance, "bridge selected" condensers and Ohmite Riteohm Type 81 1% resistors were used. The resistors were checked on a bridge and fortunately averaged much closer than one per cent.

If precision resistors are unobtainable, they can be made with a little effort. Study of the wire tables will show that ordinary copper wire magnet wire may be used in constructing the low ohm standards, while meter multipliers might be used for the higher values.

For example, the wire table shows that #28 wire has a resistance of 66.2 ohms per 1000 feet, or 0.0662 ohms per foot. Therefore a length of 16 feet will have a resistance of 1.0392 ohms.

The resistances  $R_1$  through  $R_8$  must be of the non-inductive type. Fig. 3 shows how the low ohm (1, 10 and 100) resistors can be made. The two ends of the wire are first soldered to the terminals at the end of the strip. The two



Panel of Impedance Bridge

reactance of a capacitor is inversely proportional to its capacity, the condition for balance for either bridge circuit is

$$\frac{L_s}{B} = \frac{\text{"CRL"}}$$

$$\frac{B}{C_s} = \frac{1}{\text{"CRL"}}$$

Therefore

$$L_s = B(\text{"CRL"})C_s$$

Thus the product of  $B \times \text{"CRL"}$  is the factor by which the numerical value of  $C_s$  must be multiplied to determine the value of the unknown inductance.

As in the case of capacity measurements, it will be found necessary to balance resistive as well as reactive components in the non-resistive arms. The amount of resistance which must be added in the capacitive arm to obtain a sharp balance serves as a means of measuring  $Q$  (or  $X/R$ ) of the coil under test.

$$Q = 1/2\pi fCR$$

The range of  $Q$  which may be measured with the Maxwell bridge is up to 10 and for the Hay bridge, to 1000. It

TABLE THREE					
THIS TABLE SHOWS HOW THE DQ, D AND Q		DIALS SHOULD BE MARKED TO BE DIRECT READ-		ING FOR EACH RESISTANCE SETTING OF $R_{12}$ ,	
$R_{12}$		$R_{11}$		$R_{12}$	
DQ ( $R_{12}$ )	D ( $R_{11}$ )	D ( $R_{11}$ )	Q ( $R_{12}$ )	DIAL	OHMS
0	0	0	0	0.10	165
0.1	160	0.1	16	0.12	138
0.5	800	0.2	32	0.14	113
1.0	1600	0.4	64	0.16	103
1.5	2400	0.6	96	0.18	92.5
2.0	3200	0.8	128	0.2	83.0
3.0	4800	1.0	160	0.25	66.3
4.0	6400	2.0	320	0.3	54.3
5.0	8000	3.0	480	0.35	46.6
6.0	9600	4.0	640	0.40	40.3
7.0	11200	5.0	800	0.45	35.6
8.0	12800	6.0	960	0.5	32.0
9.0	14400	7.0	1120	0.6	26.8
10.0	16000	8.0	1280	0.7	23.0
—	—	9.0	1440	0.8	20.1
—	—	9.5	1520	0.9	17.7
—	—	10.0	1600	1.0	16.1
—	—	—	—	1.5	10.8
—	—	—	—	2.0	8.1
—	—	—	—	3.0	5.95
—	—	—	—	4.0	4.1
—	—	—	—	5.0	3.27
—	—	—	—	10.0	1.7

half-lengths of wire are then close wound in opposite directions. The looped end is pulled through the holes at the left of the bakelite strip. The one ohm "standard" is then connected to the  $R_s$  terminals of a Wheatstone Bridge — pre-set to the correct value. Insulation is removed from the loop end and the wire is twisted (reducing the total value of resistance) until a balance is indicated. When this point is reached, the junction is soldered and the excess wire cut away.

The 1000 and 10,000 ohm standards can be made by turning down some  $\frac{1}{2}$ " bakelite rods in pies. In the first model of this bridge some 80-ohm-per-foot wire, with about 250 ohms per pie for the 1000 ohm resistors, were used. Direction of winding reverses in each pie. The 10,000 ohm standards require 2500 ohms per pie. Slightly more than the required amount is placed in the last pie. This permits trimming to precise value by means of a bridge. Two 50,000 ohm 1% meter multipliers were used for the 100,000 ohm standard.

### Calibration

It is suggested that the  $R$  portion of the bridge be wired up first. The wiring

[Continued on page 62]

TABLE TWO					
THIS TABLE SHOWS HOW THE CRL DIAL CONTROLLING $R_{12}$ SHOULD BE CALIBRATED					
CRL	OHMS	CRL	OHMS	CRL	OHMS
0	0	1.0	2.0	2.0	2000
0.05	50	1.05	2.1	2.1	2100
0.1	100	1.1	2.2	2.2	2200
0.15	150	1.15	2.3	2.3	2300
0.2	200	1.2	2.4	2.4	2400
0.25	250	1.25	2.5	2.5	2500
0.3	300	1.3	2.6	2.6	2600
0.35	350	1.35	2.7	2.7	2700
0.4	400	1.4	2.8	2.8	2800
0.45	450	1.45	2.9	2.9	2900
0.5	500	1.5	3.0	3.0	3000
0.55	550	1.55	3.1	3.1	3100
0.6	600	1.6	3.2	3.2	3200
0.65	650	1.65	3.3	3.3	3300
0.7	700	1.7	3.4	3.4	3400
0.75	750	1.75	3.5	3.5	3500
0.8	800	1.8	3.6	3.6	3600
0.85	850	1.85	3.7	3.7	3700
0.9	900	1.9	3.8	3.8	3800
0.95	950	1.95	3.9	3.9	3900

# RADIO DESIGN WORKSHEET

## NO. 38—IMAGE SUPPRESSION; CONSIDERATIONS INVOLVED IN CHOICE OF INTERMEDIATE FREQUENCY

### IMAGE SUPPRESSION

One of the early difficulties of double detection receivers was that due to undesired responses. One of the most troublesome of the undesired responses was the so-called "image frequency." Fig. 1 illustrates a first detector fed by an antenna. Let the incoming desired signal be 40 mc. The frequency of the oscillator might be 42 mc. This would produce beat notes of 40 plus 42, or 82 mc, which would be eliminated by the fixed tune i-f filters, and 42 minus 40, or 2 mc, which would be accepted by the i-f filters. However, an interfering signal of 44 mc applied to the antenna would be attenuated by the antenna tuned circuit but that part of the interference which did reach the grid of the first detector would likewise produce a beat note of 2 mc. Thus 44 plus 42 = 86 mc would not be accepted by the i-f filter but 44 minus 42 would be accepted. This is the so-called image frequency, which differs from the desired signal by twice the intermediate frequency.

One method of reducing this type of interference is to use two or more tuned circuits between the antenna and the first detector, as in Fig. 2. This method attenuates the undesired interfering frequency reaching the first detector grid by something more than the square root of that reaching it in Fig. 1. This might also have been accomplished by using an amplifier between the tuned circuits as in Fig. 3. In the case of Fig. 2, the desired signal reaching the first detector grid is reduced 6 db or more over that of Fig. 1. The circuit of Fig. 2 remedies this situation and correspondingly improves

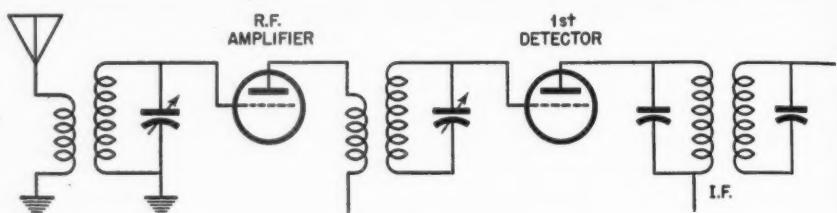


Figure 1

the signal-to-receiver-noise ratio. The circuit of Fig. 3 represents one of the best methods of reducing undesired response from an interfering r-f signal. Cheaper methods were sought, however, and a number of well-known image suppression circuits came into being.

One of these is illustrated in Fig. 4. In this circuit the first detector grid is

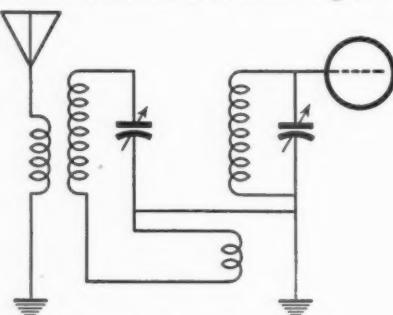


Figure 2

connected to a suitable tap on the tuned circuit secondary winding. This causes a corresponding reduction in desired signal voltage and first circuit noise as well that reaches the grid of the first detector. The tap is properly chosen in this case so that  $L_2C$  is resonant (or nearly so) at the image frequency. This forms a shunting series resonant circuit at the image frequency which greatly

attenuates it. The shunt resonant circuit  $(L_1 + L_2)C$  is, however, tuned to the desired frequency, which is lower than the interfering image frequency. Thus, in the case cited above,  $(L_1 + L_2)C$  would be resonant at 40 mc, while  $L_2C$  would be series-resonant at 44 mc.

Fig. 5 illustrates another image suppression circuit which has been quite popular. In general, this circuit is not as effective as the circuit of Fig. 4. In this arrangement the signal frequency, the oscillator frequency, and the image frequency appear in the feedback cathode circuit coil, and are fed back into the antenna circuit. The voltage transferred to the antenna primary will be greater for the higher frequencies than for the lower signal frequency. Consequently more of the image frequency will be fed back than signal frequency. All the voltages thus fed back are phased so that they will subtract from the voltage induced in the antenna. As a result, there is some reduction of signal voltage which will reduce the signal to first circuit noise ratio. This did not occur in the arrangement of Fig. 4, where signal and thermal noise are reduced in like amount and their ratio is unaffected. Probably the greatest disadvantage of the circuit of Fig. 5 lies in the practical difficulty of adjusting the circuit constants to function properly over the whole tuning band. This results partly from the fact that the selectivity of the antenna tuned circuit decreases as the frequency increases and partly from the fact that the phase angle of the tuned circuit varies more rapidly than the attenuation. This is illustrated by Fig. 6.

This figure may be computed as follows:

$$\text{At resonance } I_o = E/R$$

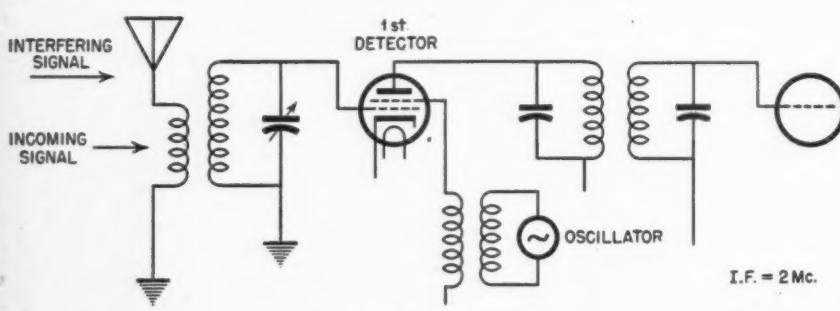


Figure 3

At any other frequency

$$I = \frac{E}{\sqrt{R^2 + X^2}}$$

Let

$$K = \frac{I}{I_0} = \frac{R}{\sqrt{R^2 + X^2}} = \frac{1}{\sqrt{1 - \tan^2 \theta}} = \frac{\sqrt{1 - K^2}}{\sqrt{1 - K^2}}$$

$$\text{phase angle } \phi = \pm \tan^{-1} \frac{X}{R}$$

where

$$X = \omega L - \frac{1}{\omega C}$$

From Fig. 6 it will be noted that

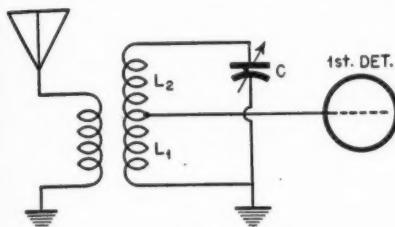


Figure 4

when the phase angle is  $45^\circ$  the signal amplitude is still seven-tenths that at resonance. This illustrates the practical difficulties of keeping the circuits of Fig. 5 properly phased over a wide frequency band without manual adjustment.

The best circuit arrangement from the standpoint of performance is probably a single tuned circuit coupling the antenna to the r-f amplifier, followed by a double tuned coupled circuit cou-

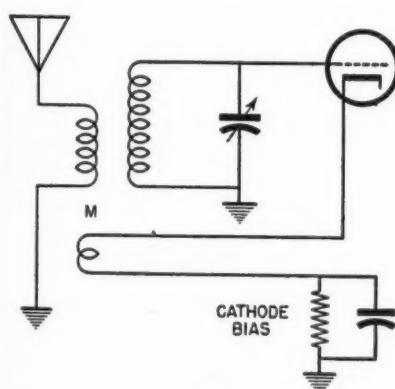


Figure 5

pling the amplifier to the first detector. Such a circuit is shown in Fig. 7.

This arrangement obviously yields optimum antenna step-up, optimum signal-to-thermal-noise ratio and has an image response which is the cube root of that for Fig. 1.

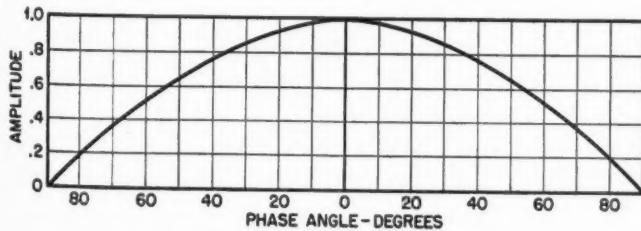


Figure 6

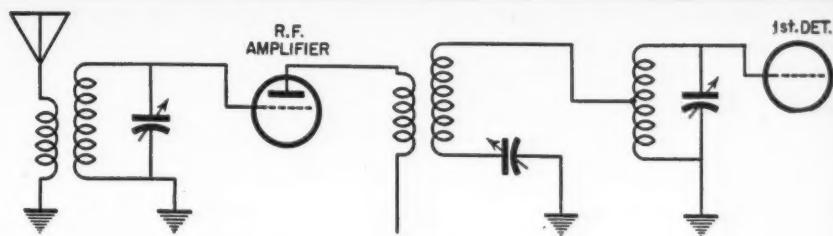


Figure 7

#### CONSIDERATIONS INVOLVED IN CHOICE OF INTERMEDIATE FREQUENCY

The choice of the proper intermediate frequency for superheterodyne broadcast receivers has at various times in the past come up for much discussion. It is now pretty well settled at 465 kc and the F.C.C. has cleared this part of the spectrum to prevent interference. However, the first intermediate frequency to be widely used was 30 kc. Later 50 kc became popular, then 175 kc was used for many years. It would appear instructive to inquire into some of the important considerations involved in the choice of the optimum intermediate frequency.

Some of the boundary conditions are:

1. The intermediate frequency must be at a sufficiently high frequency that two incoming signals differing in frequency by an amount equal to the intermediate frequency cannot feed through the radio-frequency circuits and cause audible interference (see Fig. 8). This is obviously influenced by the r-f attenuation embodied in the receiver.

2. The intermediate frequency must be sufficiently high to permit the radio frequency circuits to offer about 60 db attenuation to the image frequency.

3. The intermediate frequency must not be so high that good sensitivity and selectivity at moderate cost cannot be attained.

4. The intermediate frequency must not be so high that its second or third harmonic falls in the band to be received. Such harmonics may be generated by the intermediate frequency tubes or by the second detector and fed back to the first detector through coupling in the wiring.

5. The intermediate frequency should not fall on or too near the frequency of any nearby transmitters which might be strong enough that some of the signal from such transmitters would feed through the radio-frequency circuits or be picked up by exposed wiring in cir-

cuit elements and thus be amplified to cause interference.

6. The intermediate frequency should be chosen to reduce all modulator products that fall in the intermediate-frequency or radio-frequency band to a minimum. While there are an unlimited number of possible combinations, some of the most important are:

Oscillator frequency beating with second harmonic of signal

Second harmonic oscillator beating with signal

Oscillator frequency beating with third harmonic of signal

Third harmonic of oscillator beating with second harmonic of signal

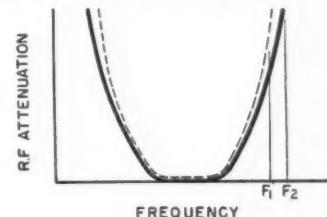


Figure 8

Second harmonic of oscillator beating with third harmonic of signal

Third harmonic of oscillator beating with signal

Such a list could be extended to perhaps 30 undesired responses for the broadcast band alone. When the spectrum of the broadcast and international short wave bands is considered, the number of important responses may number several thousand.

It is of utmost importance that sufficient radio-frequency circuits be used. However such circuits are much more expensive than the fixed tuned intermediate frequency circuits, so that economy dictates that no more of them than required be used. Let the Q of the radio frequency circuits vary from 50 which represents a poor circuit to 200 which is extremely good. The table below illustrates the attenuation in decibels at 1%, 5% and 10% of turns for one tuned circuit.

ADJACENT CHANNEL ATTENUATION FOR SINGLE TUNED CIRCUIT, VARYING Q

Q	1%	5%	10%
50	3 db	13.5 db	20 db
100	7 db	20 db	26 db
150	10 db	23 db	28 db
200	12 db	26 db	32 db

# RADIO BIBLIOGRAPHY

F. X. RETTENMEYER

RCA Victor Division, Radio Corporation of America

## 18—VELOCITY MODULATION, PART 2

Velocity—Modulated Beams—R. Kompfner: Tombs, *Wireless Engineer*, vol. 17, No. 17, No. 198, pp. 110-111, March 1940.

Induced Currents in Split Cylindrical Electrodes by Moving Charges—A. Okazaki—*Electrot. Journ.*, (Tokyo), vol. 4, No. 2, pp. 46-47, Feb. 1940.

Velocity—Modulated Electron Beams in Crossed Deflecting Fields—B. Kockel & L. Mayer—*Jahrb. der AEG-Forschung*, No. 2, vol. 6, pp. 72-77, 1939.

Velocity Modulated Beams—Letter to the Editor—R. Kompfner—Correspondence Section—*The Wireless Engineer*, March 1940, pg. 110.

The Cyclotron—(Book)—W. B. Mann, Published by Methuen & Co., London.

Velocity Modulated Beams—Letter to the Editor—R. Kompfner—Correspondence Section—*The Wireless Engineer*, May, 1940, p. 202.

Velocity-Modulated Beams—Letter to the Editor—C. Strachey, Correspondence Section—*The Wireless Engineer*, May, 1940, pp. 202-203.

Volicity-Modulated Beams—Letter to the Editor—M. Martineau Tombs—Correspondence Section—*The Wireless Engineer*, May, 1940, pp. 203-205.

The Electron Lens with Transit-Time Phenomena, and On the Achromatism of Electron Lenses—A. Recknagel: A. Nesslinger—*Jahrb. der AEG-Forschung*, No. 2, vol. 6, pp. 78-82: pp. 83-85, 1939.

Velocity Changes of the Electrons in the Deflecting Condenser at Ultra-High Frequencies—H. Doring—*Jahrb. der AEG-Forschung*, No. 2, vol. 6, pp. 91-94, 1939.

New Transit-Time Devices—H. E. Hollmann—*Funktech. Monatshefte*, No. 1, pp. 1-7, Jan. 1940.

Ballistic Models of Velocity-Modulated Transit-Time Devices—H. E. Hollmann, *Hochf:tech. u. Elek:akus.*, vol. 55, No. 3, pp. 73-86, March 1940.

Klystrons at Stanford University (Photographs only)—*Electronics*, Vol. 13, No. 1, p. 25, Jan. 1940.

Velocity-Modulated Beams—Kompfner, Strachey, Clavier—*Wireless Engineer*, Vol. 17, No. 201, pp. 262-263, June 1940.

Current-Flow Characteristic in Velocity-Modulated Valves—M. Geiger—*Physik. Berichte*, No. 7, Vol. 21, pp. 710-711, 1940.

Natural Oscillations of Electrical Cavity Resonators—W. L. Barrow & W. W. Mieher—*Proc. IRE*, Vol. 8, No. 4, pp. 84-191, April 1940.

A Method of Loading Micro-Wave Generators—K. Morita—*Nippon Elec. Commn. Eng.*, No. 19, pp. 182-187, Jan. 1940.

The Electronic Valve with Velocity Modulation—Bethenod—*Comptes Rendus*, Vol. 210, No. 11, p. 423, 11th March 1940.

On the Resonant Frequency of a Type of Klystron Resonator—E. H. Smith, *Phys. Review*, Vol. 57, No. 11, p. 1080, 1st June 1940.

On the Theory of Transit-Time Oscillations—F. Ludi—*Helvetica Phys. Acta*, Fasc. 2, Vol. 13, pp. 77-121, 1940.

The Ultra-Short-Wave Generator with Phase-Focusing—F. Ludi—*Helvetica Phys. Acta*, Fasc. 2, Vol. 13, pp. 122-143, 1940.

Causes of Frequency Variations in Klystron Oscillators—Ginzton and others, *Proc. I.R.E.*, Vol. 28, No. 6, p. 282, June 1940.

Simple Calculations of Klystron Efficiency—E. U. Condon—*Phys. Review*, Ser. 2, Vol. 58, No. 2, p. 204, 15th July 1940.

Some Typical Phenomena Relating to Ultra-Short-Wave Pentode Amplifier Circuits—K. Posthumus & C. A. Gehrels—*Philips Transmitting News*, Vol. 6, No. 3/4, pp. 49-55, Dec. 1939.

Ultra-High-Frequency Power—D. H. Sloan & L. C. Marshall—*Phys. Review*, 15th July 1940, Ser. 2, Vol. 58, No. 2, p. 193.

Influence of, and Influence on, the Composition of Charges Periodically Moving in an Electronic Tube, Especially with a View to Shock Excitation of Short-Wave Oscillations—G. Jobst—*Telefunken-Hausmitteilungen*, p. 84, 1939.

Currents Induced by Electron Motion in Electrodes—Simon Ramo—*Proc. IRE*, p. 854, 1939.

A Wide-Band Inductive-Output Amplifier—A. V. Haeff and L. S. Neergaard—*Proc. IRE*, p. 127, March, 1940.

On Velocity-Modulated Electronic Tubes—J. Bethenod—*Comptes Rendus*, p. 103, 1940.

Phase Focusing in Velocity-Modulated Beams—W. E. Benham—*The Wireless Engineer*—Vol. 17, p. 514, December, 1940.

Velocity-Modulated Beams—Letter to the Editor—R. Kompfner—Correspondence Section—*The Wireless Engineer*—p. 262, June, 1940.

The Generation and Amplification of Decimetric and Centimetric Waves—H. E. Hollmann—*T.F.T.*, Vol. 32, No. 3, pp. 65-69, March 1943.

Arrangement for the Setting-Up of Ultra-High-Frequency Oscillations in a Cavity Resonator by Means of a Gaseous-Discharge, F. Borgnis—*Hochf:tech. u. Elek:akus.*, Oct. 1942. Vol. 60, No. 4, p. 112.

Tubes Employing Velocity Modulation—R. I. Sarbacher & W. A. Edson—*Proc. IRE*, Vol. 31, No. 8, pp. 439-542, Aug. 1943.

Impulse Formation and Oscillatory Output for an Electron Flow in the Longitudinal-Field Chamber—M. Geiger—*Telefunken-Rohre*, No. 19/20, p. 119, March 1941; No. 24/25, p. 38, Oct. 1942.

Contribution to the Theory of Velocity-Modulated Tubes and Other Transit-Time Valves—R. Warnecke & J. Bernier—*Rev. Gen. de l'Elec.*, Vol. 51, Nos. 1 & 2, pp. 43 & 117 onwards, Jan. & Feb. 1942.

## RADIO BIBLIOGRAPHY

On the Theory of the Split-Anode Magnetron—F. Ludi—*Sci. Abstracts*, Sec. B, Aug. 1943, Vol. 46, No. 548, p. 155: from *Helv. Phys. Acta*, No. 1 Vol. 16, 1943.

New Receiving Tubes for Very High Frequencies—Sylvania Electric Products—*QST*, Vol. 27, No. 8, p. 59, Aug. 1943.

Current and Power in Velocity-Modulation Tubes—L. J. Black & P. L. Morton—*Proc. IRE*, Vol. 32, No. 8, pp. 477-482, Aug. 1944.

Klystron Technical Manual—Sperry Gyroscope—*Proc. IRE*, Vol. 32, No. 8, p. 501, Aug. 1944.

Deflected Electron Beams—D. Gabor—*Wireless Engineer*, Oct. 1944, Vol. 21, No. 253, p. 480.

Paths of Electrons and Ions in Non-Uniform Magnetic Fields—N. D. Coggeshall & M. Muskat—*Phys. Review*, 1st/15th June 1944, Vol. 65, No. 11/12, pp. 352-353.

Electromagnetic Hollow-Space Resonators in Short-Wave Technique—F. Borgnis—*ETZ*, Vol. 61, 1940, p. 461.

The Ultra-Short-Wave Generator with Phase-Focusing—Ludi—*Hochf:tech. u. Elek:akus.*, Aug. 1940, Vol. 56, No. 2, pp. 60-62.

Low-Loss Hollow-Space Circuits for Oscillation Generation in the Decimetric-Wave Region by Velocity-Modulation—R. H. Varian—*ETZ*—1st Aug. 1940, Vol. 61, No. 31, p. 722.

Production of Ultra-High-Frequency Radio Waves by Electronic Oscillations—S. S. Banerjee & A. S. Ramo—*Indian Journ. of Phys.*, April 1940, Vol. 14, Part 2, pp. 93-100.

Velocity-Modulated Transit-Time Valves—H. Doring & L. Mayer—*ETZ*, 25th July & 1st Aug. 1940, Vol. 61, Nos. 30 & 31, pp. 685-690 & 713-715.

Characteristics of Electron Oscillations of "Hammer-Type" Thermionic Vacuum Tube with Lecher Wires and Determination of its Input Resistance—R. Nakamura—*Electrotech. Journ., Tokyo*, Aug. 1940, Vol. 4, No. 8, pp. 180-183.

On the Magnetron with a Bowl-Type Resonator—K. Owaki—*Electrotech. Journ., Tokyo*, Aug. 1940, Vol. 4, No. 8, p. 188.

On the Static Theory of the Magnetron—S. V. Bellyustin—*Journ. of Exp. & Theoret. Phys.*, No. 2, Vol. 10, 1940, pp. 190-198.

Velocity Modulation: Results of Further

Considerations—R. Kompfner—*Wireless Engineer*, Nov. 1940, Vol. 17, No. 206, pp. 478-488.

Phase Focusing in Velocity-Modulated Beams—W. E. Benham—*Wireless Engineer*, Dec. 1940, Vol. 17, No. 207, pp. 514-516.

Forced Oscillations in Cavity Resonators—E. U. Condon—*Journ. of Applied Phys.*, Feb. 1941, Vol. 12, No. 2, pp. 129-132.

A New Method for the Calculation of Cavity Resonators—W. C. Hahn—*Journ. of Applied Phys.*, Jan. 1941, Vol. 12, No. 1, pp. 62-68.

Retarding-Field Valves with a Magnetic Field: Static Characteristics and Short-Wave Generation—F. Hoffmann—*Hochf:tech. u. Elek:akus.*, Nov. 1940, Vol. 56, No. 5, pp. 137-148.

On the Theory of an Electron-Beam Oscillator with Phase Focusing—V. I. Kalinin—*Elektrosvyaz*, No. 9, 1940, pp. 46-54.

The Phase Focusing of Electron Beams Travelling in a Straight Line—F. Borgnis & E. Ledinegg—*Zeitschr. f. tech. Phys.*, No. 11, Vol. 21, 1940, pp. 256-261.

Current-Flow Characteristics in Velocity-Modulated Valves—M. Geiger—*Telefunken-Röhre*, No. 16, 1939, p. 177 onwards.

Elementary Theory of the Spherical Cavity Resonator—T. G. Owe Berg—*Hochf:tech. u. Elek:akus.*, Feb. 1941, Vol. 57, No. 2, pp. 56-60.

A Recently Developed Circuit for the Generation of Power at Ultra-High Frequencies—A. L. Nelson—*Proc. IRE*, Nov. 1940, Vol. 28, No. 11, p. 532.

Addition to the Paper "The Phase Focusing of Electron Beams Traveling in a Straight Line"—F. Borgnis & E. Ledinegg—*Zeitschr. f. tech. Phys.*, No. 1, Vol. 22, 1941, pp. 22-23.

Klystrons—*Electronics*, January, 1940, Vol. 13, No. 1, p. 25.

The Mode of Action of the Four-Slit Magnetron—I. Runge—*ETZ*, 10th April, 1941, Vol. 62, No. 15, p. 381; summary only, from *Telefunken-Röhre*, No. 18, 1940, pp. 1-17.

On the Electron Mechanism in the Retarding Field Valve—F. W. Gundlach & W. Kleinsteuber—*Zeitschr. f. tech. Phys.*, No. 3, Vol. 22, 1941, pp. 57-65.

Traveling Waves in Electron Beams—S. Ramo, Hahn—*Communications*, Nov. 1940, Vol. 13, No. 11, pp. 5-8 and 24, 25.

Inside the Klystron—*Electronics*, Nov. 1940, Vol. 13, No. 11: front cover.

Electron Amplifier Valves with Static Secondary-Emission Multiplication—W. Klechsig & M. Sandhagen—*ETZ*, 24th April 1941, Vol. 62, No. 17, pp. 413-414; summary only, from *Mitteil. Fernseh-A. G.*, Vol. 2, 1940, p. 16 onwards.

Discussion on "On Ultra-High-Frequency Oscillations Generated by Means of a Demountable Thermionic Tube Having Electrodes of Plane Form"—W. E. Benham: Leyshon—*Proc. Phys. Soc.*, 1st July 1941, Vol. 53, Part 4, pp. 490-491.

Ultra-Short-Wave Group Transmitter—J. Pintsch Co.—*Hochf:tech. u. Elek:akus.*, April 1941, Vol. 57, No. 4, p. 121.

Negative-Transconductance Oscillators of Retarding-Field Type as Frequency Converters—A. Pinciroli—*Alta Frequenza*, Oct. 1940, Vol. 9, No. 10, pp. 581-593.

Position of Ultra-Short-Wave Valve Technique—W. Kleen—*Zeitschr. f. tech. Phys.*, No. 12, Vol. 21, 1940, pp. 357-367.

Generation of Ultra-Short Waves—J. Pintsch Laboratories—*Hochf:tech. u. Elek:akus.*, May 1941, Vol. 57, No. 5, p. 139.

Deflection and Impedance of Electron Beams at High Frequencies in the Presence of a Magnetic Field—L. Malter—*RCA Review*, April 1941, Vol. 5, No. 4, pp. 439-454.

The Operation of Electron Tubes at High Frequencies—H. Rothe—*Proc. IRE*, Vol. 28, No. 7, July, 1940, p. 325.

The Transitron Oscillator—Cleto Brunetti—*Proc. IRE*, Vol. 27, No. 2, February, 1939, p. 88.

Electron-Beam Magnetrons and Type-B Magnetron Oscillations—Kinjiro Okabe—*Proc. IRE*, Vol. 27, No. 1, January, 1939, p. 24.

The Harmonic Mode of Oscillation in Barkhausen-Kurz Tubes—W. D. Hershberger—*Proc. IRE*, Vol. 25, No. 5, May, 1937, p. 564.

Excess-Energy Electrons and Electron Motion in High-Vacuum Tubes—Ernest G. Linder—*Proc. IRE*, Vol. 26, No. 3, March, 1938, p. 346.

Magnetron Oscillators for the Generation of Frequencies Between 300 and 600 Megacycles—G. R. Kilgore—*Proc. IRE*, Vol. 24, No. 8, August, 1936, p. 1140.

Note on Vacuum Tube Electronics at Ultra-High Frequencies—F. B. Llewellyn .. [Continued on page 731]

# This Month



Measuring fine wires for electronic tubes at the Dobbs Ferry, N. Y., plant of the North American Philips Company. A unit-length sample is weighed on an accurate torsion balance. From the density of the wire and its weight, the diameter can then be computed.

## 30 PER CENT PRICE INCREASE ON RADIOS FORECAST AFTER WAR

Due to increased labor and materials costs, postwar radio receivers will sell for about 30 per cent more than they did in 1941, according to Mort N. Lansing, of the Specialties Unit, Bureau of Foreign and Domestic Commerce.

Writing in the April issue of "Domestic Commerce" on "Television and its Post-war Outlook," Mr. Lansing forecast a rising volume in postwar sales of radio and television sets for the first four years after V-E Day, reaching a retail value of \$1,870,000,000 in the fourth year, compared with the 1941 volume of \$460,000,000.

Mr. Lansing's article predicted that FM broadcasting and television on a broad scale will open new markets. The development of the walkie-talkie in the war has paved the way for widespread civilian use

of this radio service, Mr. Lansing also said. "Many factors were considered in making these estimates," he wrote. "Weight is given to the fact that AM-FM receivers and television receivers will represent an increasingly larger proportion of total sales each year. This in turn will result in increased average receiver prices each year.

"However, it is believed that at least on a short-time basis, FM will be much more important than television on account of its more general utility and the fact that sound broadcasting techniques have already been developed. As television broadcast techniques are perfected, television sales will become increasingly larger."

Copies of the April issue of "Domestic Commerce" may be obtained at ten cents from the Government Printing Office, Washington, D. C.

## Direct-Viewing Cathode-Ray Tube Receiver

**T**HIS merits of direct-viewing television systems were set forth by Allen B. Du Mont, who heads his own company engaged in the development and manufacture of cathode-ray tubes and equipment, including television receivers and transmitters, before the June 15th meeting of The Institute of Radio Engineers, in New York. Stated Dr. Du Mont:

"In the past, and also at the present time, the direct-viewing cathode-ray tube has been used almost universally in all oscilloscope, television and radar applications with very satisfactory results. The tubes that have been used previously for television ranged in size from 5" in diameter to 14" in diameter. Because of the desire on the part of television viewers for a larger picture, a 20" tube has been developed with a reasonably flat face. This tube utilizes a pressed face in order to economize on manufacture and insure uniformity of product. It is possible with this tube to obtain a picture 13½" x 18", which our experience has shown is of a satisfactory size for any ordinary home living room.

"The principal advantages obtained with the direct-viewing cathode-ray tube are: high light brilliance, better contrast range, wide angle viewing, lower accelerating voltage, longer life, better resolution, less alignment difficulty, and simplicity of the focusing system. It would seem from this list of advantages of the direct-viewing cathode-ray tube as compared with projection systems, that there should be very little question as to which is the most satisfactory providing any picture larger than 13½" x 18" is not desired.

"The disadvantage of the direct-viewing cathode-ray system is a slight curvature of the screen and the need for a special mounting arrangement to reduce the depth of the television receiver in the larger bulb sizes. For instance, the length of the 20" tube is 31", but by using a mechanical arrangement so that the tube is only in a horizontal position when being used, the depth of the cabinet can be held to 24".

"Taking up the various characteristics of the direct-viewing cathode-ray tube television receiver in detail, we find that the highlight brightness of the 20" tube is in the order of 20 foot lamberts as compared with approximately 3.5 foot lamberts for the most efficient projection system now in use. In both cases the size of the picture is considered to be 13½" x 18".

"One of the big advantages of the higher light brilliance is the fact that the 20" tube receiver can be used satisfactorily in a quite brilliantly illuminated room and an ambient light level as high as 5 foot lamberts can be tolerated without seriously impairing the picture quality. On the other hand, with the projection system only about .5 foot lambert average ambient light can be tolerated. It is interesting to com-

pare the brilliance of the 20" picture with that of the normal commercial 35 mm screen, which averages between 6 and 10 foot lamberts.

"As regards the brightness ratio, or contrast range, the 20" tube has a contrast range of approximately 35 as compared with a contrast range of 17 for the projection system. This is an extremely important characteristic of the television picture and in many cases the lack of contrast range gives people the impression of poor resolution.

"As to directivity (maximum viewing angle from the normal-angle at which the apparent brightness decreases to 50% of its value in normal direction) we find that the 20" tube can be viewed from  $\pm 80^\circ$  whereas the projection system screen can only be viewed from  $\pm 15^\circ$ . It is of course possible to widen this angle somewhat in the projection system but in so doing the highlight brightness will decrease from its already low value.

"In making these comparisons we have assumed an accelerating voltage on the 20" tube of 15 kilovolts and 30 kilovolts on the 5" flat face tube of the projection system. It is obvious that the lower accelerating voltage of the direct-viewing tube effects certain economies in the manufacture of the receiver.

"The anticipated life of the 20" direct-viewing tube should run considerably above 1,000 hours, whereas the present tubes used in the projection system the anticipated life is from one-half to one-third that of the direct-viewing tube. This is because of the higher accelerating voltage as well as the much greater concentration of energy per unit of area in the projection tube.

"With the 20" direct-viewing tube, the spot size is sufficiently small to resolve any 525-line television pattern or even higher with a well-designed deflection yoke, whereas care must be taken with the 5" tube used in the projection system to obtain full 525-line resolution.

"Forgetting about the size of the spot for the moment, we have noticed that the resolution on the 5" projection tube is considerably reduced by light scattering on the fluorescent surface as well as on the translucent projection screen. With the direct-viewing tube, all the elements are aligned within the glass envelope, whereas with the projection system the tube and optical system have to be very carefully lined up and any slight inaccuracy of this line-up will seriously interfere with the resolution of the picture.

"In order to focus the picture on the direct-viewing tube, it is only necessary to make an electrical adjustment, whereas with the projection system both electrical and optical adjustment are necessary. Furthermore, the lenses and translucent screen of the optical system, and in some cases a mirror, are not encased in vacuum and the picture is subject to deterioration

with age unless the mirror, translucent screen, and lens surfaces are carefully kept clean.

"As regards the cost between the two systems, at the present time there seems to be very little to chose between. In the one case we have the cost of the 20" tube and its special mechanical arrangement for putting it in the horizontal position during use, and in the other case we have the cost of the 5" projection tube, its optical system, usually a mirror, and a translucent screen.

"As previously mentioned, the voltage on the direct-viewing tube is 15 kilovolts as against 30 kilovolts with the projection system, so that there is a saving here in the case of the direct-viewing tube.

"As regards the design of the cabinet, with the 20" tube it can be somewhat lower than with the projection system although the maximum depth is slightly greater as compared with the projection receiver.

New General Electric large-screen television receiver, to be manufactured as soon as war conditions permit. Screen measures 16 by 22 inches. This receiver was recently shown for the first time, in New York City



"This comparison has been made mainly taking into consideration the actual results obtained to date with the two systems. Undoubtedly improvements will be made in the projection system but it is also reasonable to assume that improvements will be made in the direct-viewing tube. If we desire to go to a larger picture than 13½" x 18", as previously pointed out, some type of projection system is imperative."

#### RAYTHEON RADIO-TELEPHONE STATIONS

The Raytheon Manufacturing Co. announced recently that it has filed applications with the Federal Communications Commission for construction permits to install five coastal harbor radio-telephone stations in New England at Eastport, Rockland, Portland, Maine; and Gloucester and New Bedford, Massachusetts.

Included with Raytheon's application were statements from eighty-nine import-

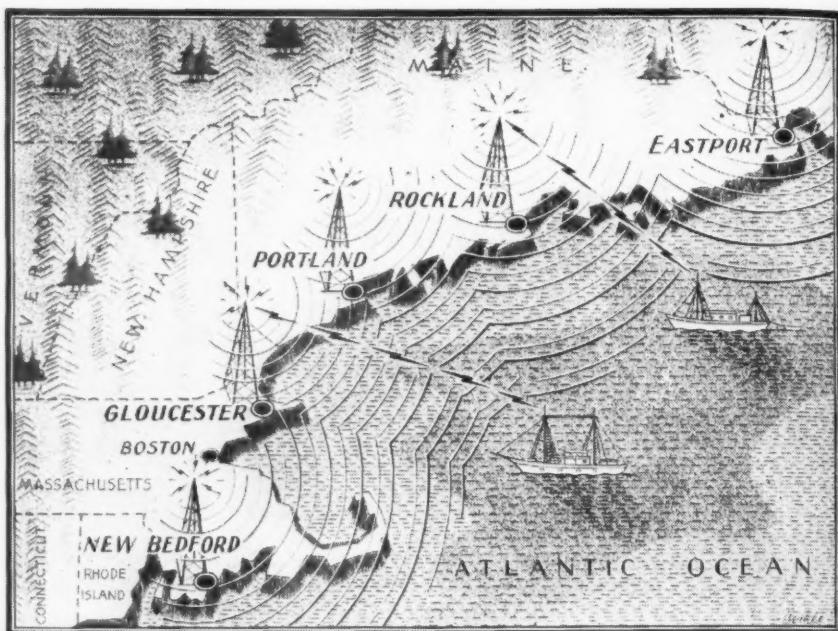
ant potential users testifying as to the vital need for the proposed service. At present only one coastal harbor radio-telephone station is in operation in this part of the country. This is the Boston station operated by the New England Telephone and Telegraph Company.

One of the most important users of the proposed service would be the fishing industry. New England represents 16.2% of the total yearly volume in pounds of the United States fishing industry, and 19.7% in dollar value. The New England proportion of the entire United States is 626 million pounds, or 20 million dollars.

It is proposed to introduce for the first time in the coastal harbor service frequencies in the newly allocated 152-162 mc band. The engineering report discloses that an average satisfactory service range of some 45 miles is estimated for the 160 mc operation at each of the five points.

In addition to the 160 mc frequencies Raytheon requests the assignment of 2, 4, 6 and 8 mc for servicing vessels in the area beyond the range of the 160 mc channels. The application pointed out that the most efficient operation would be obtained by the assignment of exclusive 2, 4, 6 and 8 mc frequencies for the five stations, but in the event the Commission found it impossible to make such assignments, the application requested shared use of 2550, 4282.5, 6470, and 8585 kc now allocated by the Commission to Great Lakes Coastal Harbor stations.

Raytheon discloses that its survey indicates that fishing vessels require communications service at distances as great as 800 miles from New England.



Proposed Raytheon coastal harbor radio telephone stations

The proposed coastal harbor radio-telephone rates employ a basis quite different from those offered by existing coastal harbor stations. A rate of \$1.00 for three minutes is offered when the 160 mc frequencies are employed, and a rate of \$1.50 for three minutes when the frequencies in the 2-8 mc band are employed with an additional per minute charge of 35c and 50c respectively.

In its application a power of 2,000 watts was specified on the 2-8 mc operation and 50 watts on the 160 mc operation. Three frequencies are requested in the newly allocated 152-162 mc band with one channel for calling purposes and the other two channels for traffic operations. Two traffic frequencies are requested in order to meet peak traffic loads and to avoid interference between stations when a vessel is located in a position within the over-lapping service area of two stations.

The rates proposed are for the radio link of the circuit only, to which would be added the regular Bell System land-line rates for communications with telephone subscribers ashore.

Raytheon proposes to transmit on a scheduled basis free of charge, United States Weather and Hydrographic reports. Repetitions of these reports will be furnished upon request at a rate of 50c when 2-8 mc frequencies are employed and 35c when 160 mc facilities are employed. A similar differential is used for message forwarding and position reporting services.

The application also stated that it would offer service to land mobile units, such as trucks and buses when within the 160 mc service area range, if such service was requested.

#### I. T. & T. APPOINTS KOHLHAAS

Herman T. Kohlhaas, editor of Electrical Communication, technical journal of the International Telephone and Telegraph Corporation and associated companies, has been appointed an assistant vice-president of the Corporation. He has had a long career in the I. T. & T. System.

Mr. Kohlhaas received a B.S. degree in

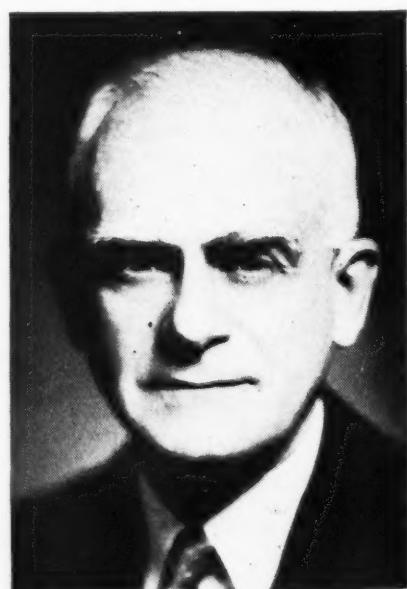
electrical engineering from Cooper Union in 1907. Later he was awarded E.E. degrees by both Cooper Union and Brooklyn Polytechnic Institute.

From 1905 to 1922, he served in the Bell Telephone Laboratories as an engineer, a section head, and finally as a division head in the Physical Laboratory. In 1922, he was appointed executive personnel assistant to the system's engineer of the Bell Labs. He was transferred to the Western Electric Company headquarters in 1924.

In 1925, Mr. Kohlhaas was transferred to the International Western Electric Company to make statistical studies and to start his responsibility as editor of Electrical Communication. Through the purchase of that Company, he became a member of the staff of the International Telephone and Telegraph Corporation. During 1937-39, he edited Electrical Communication from London, serving also as publicity representative of the I. T. & T. and International Standard Electric Corporation.



The Bradley tube, duplicate of German-made repeater, made by Western Electric for Belgian telephone systems



Herman T. Kohlhaas

# New Products



## NEW REPRODUCER

Specially designed for railroad use in intercommunication, the new Type NJ-300 Reproducer, announced recently by Jensen Radio Mfg. Co. of this city, is arousing widespread interest among railroad signal engineers and builders of intercommunication equipment.

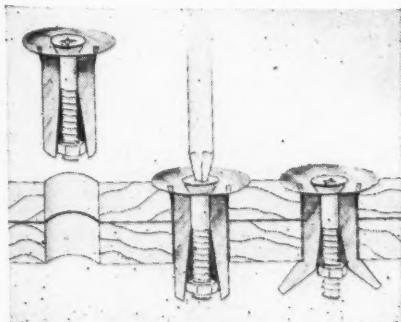
Type NJ-300 Reproducer was originally designed for Navy use as a loud speaker and microphone (talk-back) but has been developed for all types of railroad use in locomotives, cabooses, signal towers, and outdoors in railroad yards. In tests made on trains and in locomotive cabs, Jensen engineers found that this speaker, because of its frequency range, over-rode the surrounding high noise levels and delivered clear, crisp, intelligible speech.

Because of correct case design, wind noise pickup, when used as a microphone, shows a reduction up to 6 db as compared with the conventional type of loud speaker. Voice coil impedance is 12 ohms nominal value; power handling capacity for speech is 10 watts.

Type NJ-300 is in production and available on properly rated priority orders showing suitable end use.

## BLIND BOLT ASSEMBLY

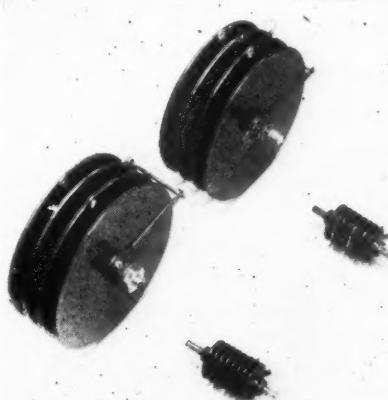
The "Des-Bolt", another of the plastic



fastening devices developed by Victory Manufacturing Company, has recently been announced. The complete unit is composed of a molded plastic expansion sleeve and any standard nut and bolt assembly of the correct size to match the sleeve. The sleeve is the important element of the design and makes possible the simplicity of the device. The sleeve is composed of three thin fingers with an inside taper extending approximately three-fourths of their length from the flanged head. The head is a flange with a cored hole to accommodate the bolt shank and countersunk to receive standard countersink type of bolts, with three sharp ribs attaching the flange and sleeve. These thin ribs wedge into the work and prevent the sleeve from turning.

Advantages of the "Des-Bolt" unit are many. When used in small assembled units, such as electronic and radio equipment, improved fastening is accomplished in locations highly inaccessible to hold the nut by normal methods.

For complete information, write to Engineering Dept. 2-E, Victory Manufacturing Company, 1105 So. Fair Oaks Ave., So. Pasadena, Calif.

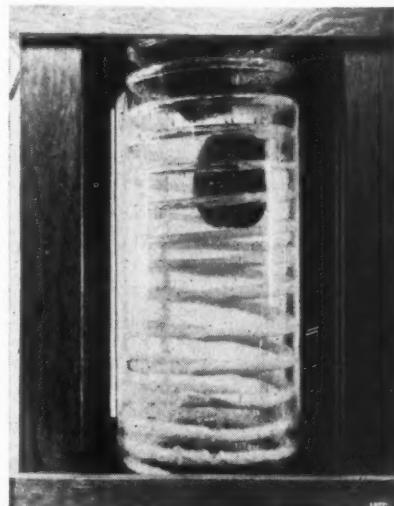


## NEW SELENIUM RECTIFIER

A newly developed selenium rectifier for applications on sea and at high humidity has been perfected by the Selenium Corporation of America, 1719 West Pico Blvd., Los Angeles 15, California, according to Mr. Carl Holmes, Project Engineer. The new unit featuring a radically different assembly method and coating technique does not show any effect of salt spray after 100 hours of operation at 50°C. Type designation of the new rectifier is "K".

Results of testing thus far, according to Mr. Holmes, prove conclusively that two-way protection of the selenium plates has been achieved. This new coating protects the selenium barrier layer from within and preserves its rectifying properties indefinitely. It also protects the selenium barrier layer from exterior attacks by salt spray, fungi, mercury vapor and other corrosive fumes.

The recently completed test of a 3-minute spraying of the selenium rectifiers



with 20% salt solution at 55°C., followed by a 3-minute air blast at 55°C., the cycle being repeated continuously throughout the entire 100-hour test.

A strong ultra-violet light was continuously played on the rectifiers during the length of the test.

After extended production runs, with many units already subjected to test, there have been no instances of corrosion nor have electrical characteristics varied in any way. As a result, concludes Holmes, the new coating not only provides the armed forces with proved dependable rectifying units, but also opens new fields for the industrial application of selenium rectifiers.

## NEW DECADE UNIT

To meet the demand for a line of flexible circuit components, Harvey-Wells Electronics, Inc., Southbridge, Massachusetts, has developed a decade unit which makes immediately available almost any desired value or combination of values covering capacitance, inductance, resist-

[Continued on page 62]



## FM REPORT

[Continued from page 42]

result that his enjoyment may be further destroyed by an alteration of first one program and then another as transmission vagaries decree. The effect may well be to render FM receivers useless to many listeners for substantial periods of time.

It has been argued that the bulk of the interference anticipated will be found in outlying rural areas which rely upon low-intensity signals for their radio reception and that if these areas be excluded, FM service will be more than 99 percent perfect. The tables make it clear that urban as well as rural service will be subject to substantial interference on the lower fre-

quencies. This Commission, moreover, is under a statutory duty to make available to all the people of the United States an efficient nationwide radio service. The Commission's duty is not fulfilled if its provision for FM service is such as to make it impossible for rural areas to enjoy satisfactory FM service.

The tables and data upon which the Commission's interference predictions are based were set forth in full in the May 25 report and were the particular topic for the oral argument on June 22 and 23. Practically without exception all persons appearing at the hearing stated either that they agreed with the Commission's predictions or that in determining the best allocation for FM they were willing to assume that the predictions as to interference contained

in the Commission's report were accurate. In those cases where exception was taken, no substantiating data were offered. Indeed, the testimony at the June 22-23 argument indicated that the Commission's predictions might underestimate in at least one respect the number of hours of interference to be anticipated at particular contours. The Commission's predictions were based upon the assumption that receivers will be generally available which are capable of rejecting an undesired signal one half as strong as the desired signal. Manufacturers generally appearing at the hearing were unwilling to state that their post-war receivers would meet this standard. With inferior receivers, an even greater number of hours of interference can be anticipated. The issue, accordingly, is whether the freedom from long-range interference which FM will enjoy at the higher frequencies is to be sacrificed by reason of other considerations.

Various objections to assigning the higher frequencies to FM have been raised in this record. For example, it has been alleged that tropospheric interference may be worse in the vicinity of 100 mc than in the 50 mc region. The Commission in its report of May 25, 1945, specifically pointed out that there would be some difference in tropospheric propagation; but this difference would be only slight and that tropospheric interference at the higher frequencies could be eliminated by slightly increasing the geographical separation between stations. This evidence was not controverted at the oral arguments on June 22 and 23, 1945, and Dr. Beverage, one of the propagation experts chiefly relied upon by persons favoring alternative No. 1, testified that tropospheric effects change slowly and that they would not be greatly different throughout the range of frequencies under consideration (Tr. 5583).

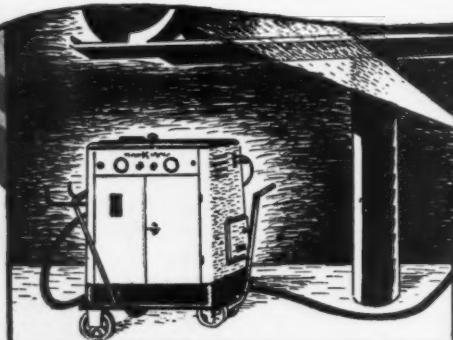
The point has also been made that equipment for use in the vicinity of 100 mc will cost more than equipment for use in the vicinity of 50 mc. This will no doubt be true at least temporarily, but it seems equally clear that competition will reduce the differential substantially, and that the benefit to the public resulting from an interference-free service will more than outweigh the slight increase in initial cost for service in the 100 mc region.

At the earlier hearings, some contended that FM might be delayed for two years or even longer if FM were assigned to the higher frequencies. At the time of the oral argument, June 22-23, 1945, the estimates of delay were reduced to four months. It may well be that competition will markedly reduce even this four-month estimate. Moreover, this report makes it possible for manufacturers to begin at once their planning and design for the higher frequencies. The War Production Board has not yet authorized construction of AM, FM, or television equipment for civilian use; and some months may still elapse before manpower or materials become available in sufficient quantities for such production to begin. If so, the planning and design of equipment for the higher frequencies can be completed before civilian production of any AM, FM, and television equipment is authorized.

Manufacturers, of course, are desirous of

## Ingenious New Technical Methods

Presented for Your Peacetime Use



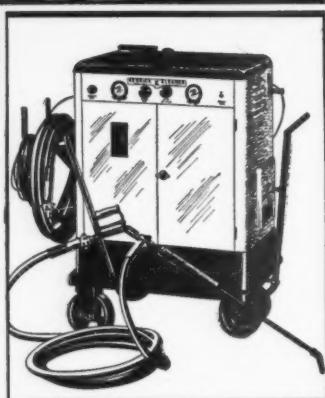
### Coming to Users of Gas-Powered Equipment 80% SAVINGS IN CLEANING TIME With Steam Rig Now the Army's Standby

An economical solution to the problem of cleaning and de-greasing trucks, passenger cars, tractors, locomotives, excavators, and the like will be available to garages, service stations, all users of oil-burning equipment, as soon as war demands permit. It is a more efficient steam cleaner now in use by the thousands in the Armed Forces.

Neat "housekeeping" has too often been neglected by industry due to the costliness of hand labor. But the best housekeepers in the World, the U. S. Army, Navy and Marine Corps, dare not neglect frequent and thorough cleaning of all equipment to safeguard against fire and malfunctioning, and to permit fast, certain inspection. This cleaner, developed to meet their high standards, removes grease, dirt and grit 5 times as fast as any other method. It cleans by a balanced combination of heat, detergent, water and friction. It is typically "army" in simplicity of design and operation; in 30 minutes, the entire machine can be dismantled and completely cleaned.

Wartime uses of Wrigley's Spearmint Gum also point the way that industry may benefit when this quality product again becomes available. It will again be a "help on the job" in many ways. Right now no Wrigley's Spearmint is being made, as present conditions do not permit the manufacture of Wrigley's Spearmint in quantity and quality sufficient for all. But remember the Wrigley's Spearmint wrapper—it is a certificate of highest quality and flavor—and will always remain just that.

You can get complete information from  
Clayton Manufacturing Company, Alhambra, Calif.



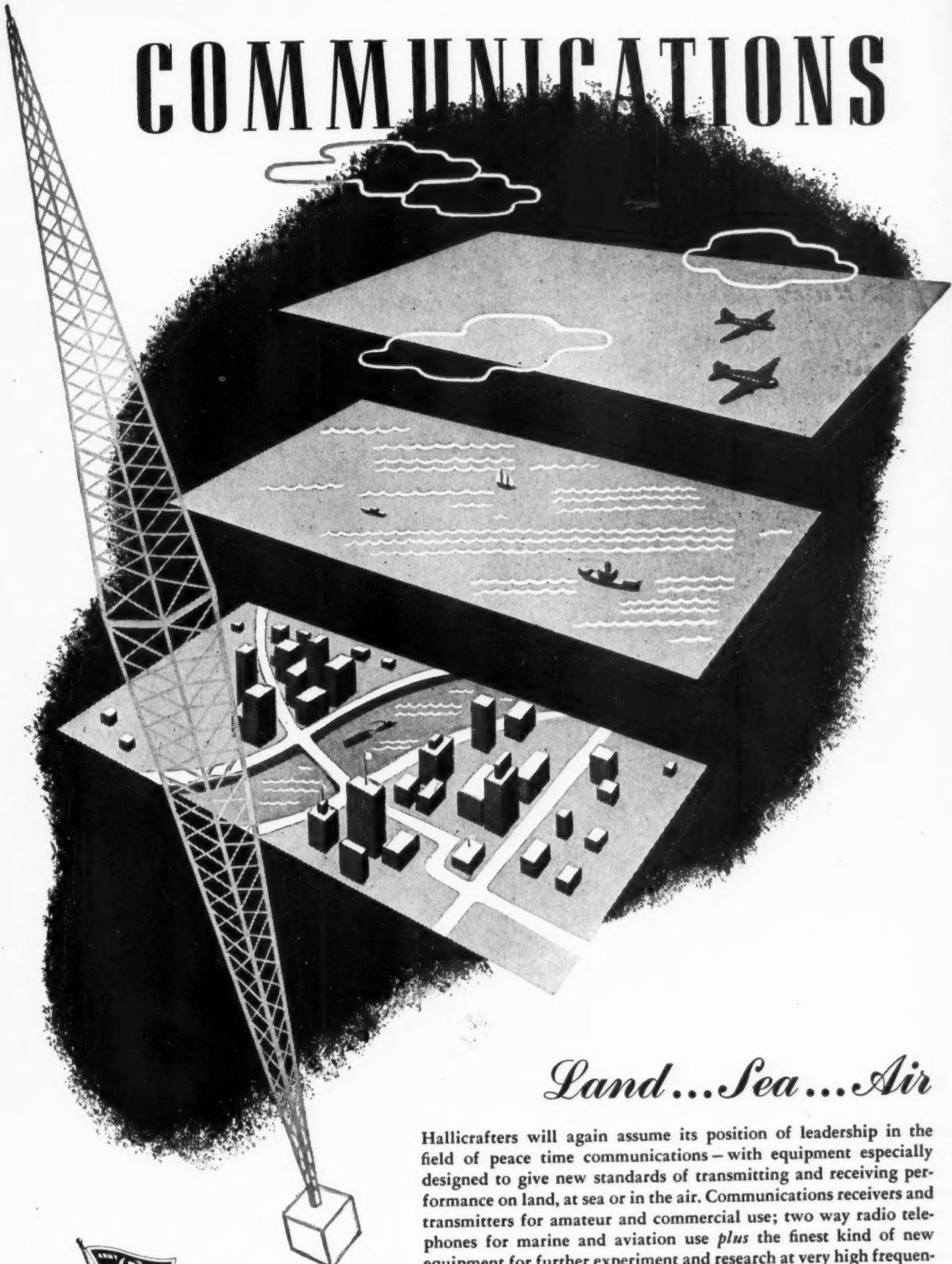
The Kerrick Cleaner



Remember this wrapper

Z-7

# COMMUNICATIONS



*Land...Sea...Air*

Hallicrafters will again assume its position of leadership in the field of peace time communications—with equipment especially designed to give new standards of transmitting and receiving performance on land, at sea or in the air. Communications receivers and transmitters for amateur and commercial use; two way radio telephones for marine and aviation use *plus* the finest kind of new equipment for further experiment and research at very high frequencies will all be included in Hallicrafters postwar production plans.



BUY A WAR  
BOND TODAY!

COPYRIGHT 1945  
THE HALLICRAFTERS CO.

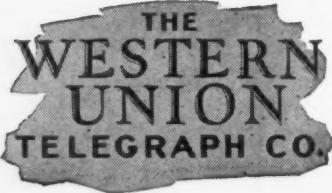
## hallicrafters RADIO



THE HALLCRAFTERS CO., WORLD'S LARGEST EXCLUSIVE MANUFACTURERS OF SHORT WAVE RADIO COMMUNICATIONS EQUIPMENT, CHICAGO 16, U. S. A.

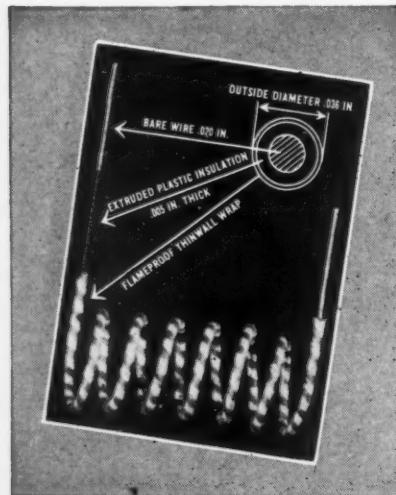
RADIO

★ JULY, 1945



## ... installs SURCO THINWALL WRAP after Rigid Testing

..... the first uniformly  
high quality fine wire, plastic  
insulated with flame proofed  
yarn serving.



This photo of typical construction is absolutely unretouched

**Voltage Breakdown — 7000 Volts**  
(For spiraled section shown in photograph  
after 5 minutes in water)  
**Insulation Resistance—30 Megs. Per 1000**  
**Ft. at 60°F. (After 72 hrs. in water)**

**Here are Thinwall's Characteristics:**  
High dielectric properties, Maximum saving in space and weight, Unlimited coding and identification, High temperature operation, Excellent abrasion resistance and toughness, Maximum protection against damage by soldering iron, Unusual flexibility at below freezing temperatures, Flameproof qualities, Good end and spot-stripping characteristics, Low cost.

Surco-American Thinwall Wrap is available in a wide variety of formulations finer sizes of wire and thinner insulations than shown above, for use where maximum performance under specific operating conditions is required.

**Surprenant**  
ELECTRICAL INSULATION CO.  
Dept. T 84 Purchase St., Boston 10, Mass.

marketing FM receivers at the earliest possible moment; and the Commission, too, is concerned that FM receivers shall be freely available to the public early enough to supply the immediate post-war demand. However, the Commission has a duty to consider the long range effects of its action as well as the effects during the months immediately ahead, and it does not propose to provide an inferior FM service during the decades to come merely because of the transitory advantages which may be urged for an inferior type of service.

Earlier in these proceedings, much emphasis was placed on the presumed hardship which would result to the approximately 400,000 persons who had purchased FM receivers before the war. Most of these receivers are combination AM-FM and the AM part of the receiver will continue to be used. There is now substantial agreement that the band (42-50 mc) for which these receivers were made is wholly inadequate and unsuited to FM reception. Accordingly, no one today argues that post-war FM should be degraded to the point necessary to accommodate these receivers. However, interim operation in the present band from 42 to 44 mc is being provided until such time as equipment for the higher frequencies is freely available to the public and until owners of existing receivers have had equal opportunity to convert them to the new band. In this connection, a converter was demonstrated to the Commission which would make existing FM receivers capable of tuning to the higher frequencies and which should retail for approximately \$10.00.

For the foregoing reasons and upon the basis of data set forth in Section 8 of the report of May 25, 1945, the Commission is adopting alternative No. 3 with certain modifications. The allocation between 42 and 108 mc is as follows:

Freq. Band (mc)	Proposed Allocation
42-44	Non-Government Fixed and Mobile
44-50	Television—Channel No. 1
50-54	Amateur
54-60	Television—Channel No. 2
60-66	Television—Channel No. 3
66-72	Television—Channel No. 4
72-76	Non-Government Fixed and Mobile
76-82	Television—Channel No. 5
82-88	Television—Channel No. 6
88-92	Non-commercial educational FM
92-106	FM
106-108	Facsimile

This allocation is essentially the allocation proposed as alternative No. 3 of the earlier report, except that the non-government fixed and mobile services have been moved from 104-108 mc to 72-76 mc, and FM and television have been adjusted accordingly. The advantage of this change is that it makes possible immediately the use of all 13 television channels below 300 mc. Under alternative No. 3 as originally proposed, the entire 6 mc television channel between 72 and 78 mc could not be used until the aviation markers centering on 75 mc were moved. The non-government fixed and mobile services are not under the same disability. They can use the entire band



### DOUBLE SENSITIVITY D.C. VOLT RANGES

0-1.25-5-25-125-500-2500 Volts, at 20,000 ohms per volt for greater accuracy on Television and other high resistance D.C. circuits.  
0-2.5-10-50-250-1000-5000 Volts, at 10,000 ohms per volt.

### A.C. VOLT RANGES

0-2.5-10-50-250-1000-5000 Volts, at 10,000 ohms per volt.

### OHM-MEGOHMS

0-400 ohms (60 ohms center scale)  
0-50,000 ohms (300 ohms center scale)

## Here's that New TRIPPLET 625-N

### Long Scale, Wide Range Volt-Ohm-Milliammeter

#### DIRECT READING OUTPUT LEVEL DECIBEL RANGES

-30 to +3, +15, +29, +43, +55, +69 DB

#### TEMPERATURE COMPENSATED CIRCUIT FOR ALL CURRENT RANGES D.C. MICROAMPERES 0-50 Microamperes, at 250 M.V.

#### D.C. MILLIAMPERES

0-1-10-100-1000 Milliamperes, at 250 M.V.

#### D.C. AMPERES

0-10 Amperes, at 250 M.V.

#### OUTPUT READINGS

Condenser in series with A.C. Volts for output readings.

#### ATTRACTIVE COMPACT CASE

Size: 2½" x 5½". A readily portable, completely insulated, black, molded case, with strap handle. A suitable black, leather carrying case (No. 629) also available, with strap handle.

#### LONG 5" SCALE ARC

For greater reading accuracy on the Triplet RED • DOT Lifetime Guaranteed meter.

#### SIMPLIFIED SWITCHING CIRCUIT

Greater ease in changing ranges.

Write for descriptive folder giving full technical details.

**Triplet** ELECTRICAL INSTRUMENT CO., Bluffton, Ohio



### Yes, Here's Why Bridgeport's the Answer to Postwar Coil Supply Problems

Bridgeport has the personnel and facilities. Right now, they're turning out highly important search coils and variometers for the armed forces. After their war job is done, the same skilled technicians will be able to give you the benefits of this experience in high production of quality radionic equipment.

And look at Bridgeport's central location! Because it is located near the population center of America, Bridgeport can give you fast, trunk line service to any part of the country. Place your order with Bridgeport NOW to insure early postwar delivery.



# BRIDGEPORT

MANUFACTURING COMPANY

Bridgeport, Illinois

R. F. Coils • R. F. Chokes • I. F. Transformers  
Transmitting Coils • Transmitting Chokes

# HARVEY

has test equipment  
for immediate delivery



**WESTON MODEL 697**  
*Volt-Ohm-Milliammeter*

A small, lightweight multi-range master test unit. Ideal for production tests on motors, electrical equipment, and parts, as well as laboratory work and general maintenance. Ranges have been carefully selected to meet many measuring requirements. .... \$24.00

**R. C. P. MODEL 804**  
*Tube, Battery and Set Tester*

A portable tester equipped for direct testing of all acorn tubes as well as old and new types of regular receiving tubes, rectifiers, etc. Also tests condensers, batteries, etc. Complete with sturdy wood case; ready for operation on 105-135 volts, 50-60 cycles. .... \$84.50

**R. C. A. MODEL 160 B**  
*Portable Oscilloscope*

May be used for engine-pressure measurements and similar applications, besides standard oscilloscope functions. Amplifiers have unusually wide frequency range. The 5" screen gives an easily read image. .... \$142.50

## Also

Precision Model 832 S—AC-DC Tester. .... \$18.65  
R. C. P. Model 442—  
Volt-Ohm-Milliammeter. .... 21.00  
Electronic Design Model 100—Voltohmist 48.00  
Jackson Model 652—Audio Oscillator. .... 88.50

\*On AA-5 Priority or better

HARVEY is prepared to provide information on all Standard Instruments . . .

R. C. A.  
WESTON  
HICKOK  
SIMPSON  
G. E.

TRIPPLETT  
SUPREME  
R. C. P.  
PRECISION  
JACKSON

. . . and others

Reasonably prompt deliveries

Telephone: LOnagre 3-1800



between 72 and 76 mc at once, with the exception of approximately one-half mc in the vicinity of 75 mc to protect the aviation markers. This shift of the non-government fixed and mobile services from 104-108 mc to 72-76 mc also results in a possible increase in the number of channels available to the non-government fixed and mobile services, since a 40 kc channel is adequate in the 72-76 mc portion of the spectrum, whereas a 50 kc channel was proposed in the 104-108 mc region.

## NEW PRODUCTS

[Continued from page 57]

ance, transformer ratios, etc., over a wide range.

So far as is known, this is the only decade unit available with circuit components that will dissipate heat and power and stand up indefinitely under actual operating conditions. The various components of this decade unit may be included in actual circuits necessary for testing equipment of all natures by research and experimental laboratories, classrooms, power companies, electrical repair and maintenance shops, and especially by industrial manufacturers for testing refrigerators, motors, insulated wire, appliances, etc.

The electrical circuits for the various components were engineered in the Harvey-Wells Research Laboratories. The unit is purely functional in design and occupies a minimum of space. Complete information and technical data is available from the manufacturer.

## IMPEDANCE BRIDGE

[Continued from page 49]

should be rigid and it is suggested that #10 or #12 tinned copper bus be used.

The CRL dial should be as large as possible. A six inch diameter dural or aluminum disc will provide enough space for the calibrated points as indicated in Table 2. This dial can be calibrated very simply by use of a G-R or equivalent 1 to 10,000 ohm resistance decade. For example, the decade ("unknown resistance") is set at 50 ohms and the CRL dial is adjusted for balance. This point is then marked on the dial. The "unknown" is then set to 100 ohms and the CRL dial again adjusted for balance, with this point marked on the dial. This step is followed in order for all the values of  $R$  indicated in Table 2.

The first markings can be made in pencil and later carefully cut in with a scribe. The cuts should then be filled in with india ink. Lettering and numbering can be engraved or stamped in.

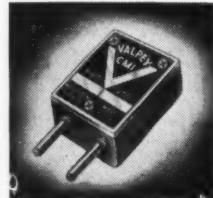
Once the CRL dial is calibrated it is a relatively simple matter to calibrate  $R_{11}$ ,  $R_{12}$  and  $R_{13}$  in accordance with the values indicated in Table 3, by simply connecting them to the "R" terminals of the bridge. After these pots are calibrated, the bridge wiring can be completed.

The "Detector" switch  $S_2$  (Fig. 1) provides means of picking up an ex-

*an Invitation  
to Peacetime  
Product Planners  
from the  
Valpey Crystal  
Corporation*

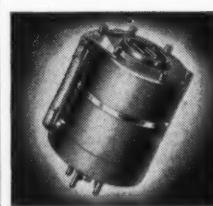
**Let Valpey Engineers  
help you plan the  
"heartbeat" of your  
postwar product**

Experienced in volume production of vital crystals for wartime communications needs, Valpey engineers and craftsmen are well equipped to solve any commercial crystal problem. Insure the success of your future products by planning to use Valpey Crystals in every "Vital Spot." Valpey's never vary.



**CM-1**

A design for normal frequency control applications.



**VP-3**

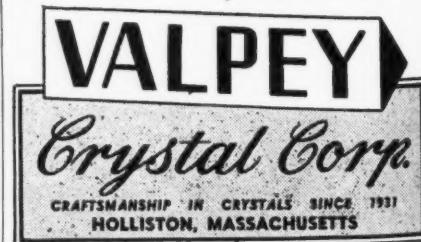
Developed for use in limited space . . . in mobile equipment.

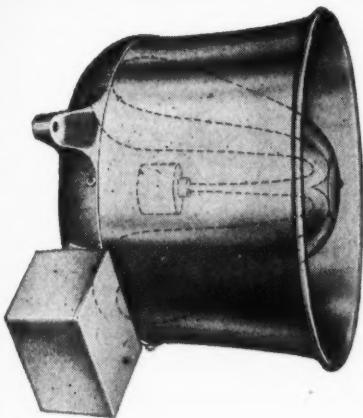


**CBC-0**

Where utmost in stability requires constant temperature control.

Write today for complete "Crystionics" data





Left—**MARINE SPEAKER**; approved by the U. S. Coast Guard, for all emergency loudspeaker systems on ships. Re-entrant type horn. Models up to 100 watts. May be used as both speaker and microphone.



Right—**RE-ENTRANT TRUMPET**; available in 2½-3½-4½-6 ft. sizes. Compact. Delivers highly concentrated sound with great efficiency over long distances.



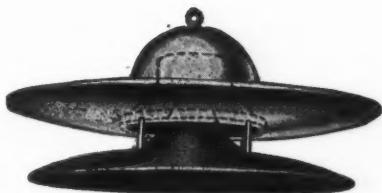
Left—**RADIAL HORN SPEAKER**; a 3½' re-entrant type horn. Projects sound over 360° area. Storm-proof. Made of RACON Acoustic Material to prevent resonant effects.



Right—**AEROPLANE HORNS**; super-powerful and efficient P. A. horns for extreme range projection. 9-4 and 2 unit Trumpets available.



Left—**PAGING HORN**; extremely efficient 2' trumpet speaker for use where highly concentrated sound is required to override high noise levels. Uses P.M. unit.



Right—**RADIAL CONE SPEAKER**; projects sound over 360° area. Cone speaker driven. Will blend with ceiling architecture. RACON Acoustic Material prevents resonant effects.

SEND FOR CATALOG



# RACON

**RACON ELECTRIC CO. 52 EAST 19th ST. NEW YORK, N. Y.**

# POWER STAMINA LONG-LIFE

**SM Fractional H.P. Motors  
for dependable performance**



With a SM motor, you get a unit designed for a specific job, engineered to your exact performance requirements, precision-built to your specifications, produced in volume for your needs. SM fractional H.P. motors are made to order with speeds from 3,500 to 20,000 R.P.M. — 1/10th to 1/200th H.P. — voltage from 6 to 220 AC-DC. Illustrated is the famous SM-2 Blower Motor; many thousands have been made for military purposes. Other SM motors have been designed and produced in large volume for a wide variety of radio, aircraft and other applications where rugged power, stamina, long life and dependable performance were primary requisites. What are your requirements?

**Small Motors, Inc.**  
1308 ELSTON AVE., CHICAGO 22, ILLINOIS

DEPT. 30

Manufacturers of special small universal, fractional H.P. motors, dynamotors, shaded pole motors, heater motors, generators.

Design • Engineering • Production

ternal detector at the upper right hand binding posts. This permits substitution of another galvanometer on d-c measurements or suitable null indicator on a-c measurements. The center position connects up the internal galvanometer (with shunt) for rough adjustments and the third position provides the galvanometer alone for fine adjustments.

Galvanometers for use in the bridge can be obtained with different values of internal resistance. Those having an internal resistance of approximately fifty ohms will give a very sharp balance indication when measuring low values of resistance. However, they become less sensitive as higher values of resistance are being measured. Since one

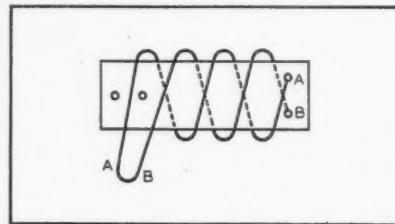


Fig. 3. Method of winding non-inductive resistance standards

cannot have everything in a general purpose instrument, a compromise is in order. The trend is toward a galvanometer with an internal resistance of approximately 1000 ohms, as this type will have a greater sensitivity over a wider range of resistance measurement. By means of the switch  $S_3$  it is a simple matter to connect an external "low ohm" galvanometer on low ohm measurements. To increase the sensitivity on the high ohm range an external battery of  $22\frac{1}{2}$  volts may be used.

The "Generator" switch  $S_4$  adds greatly to the flexibility of the bridge. In the "1 KC" position the oscillator A+ and B+ circuits are completed and the 500-ohm output of the oscillator is connected to the bridge. In the center position, provision is made for use either of an external battery for d-c measurements or an external signal source for a-c measurements. The third position "DC" picks up an internal source of six volts. "Generator" binding posts are at the lower right.

#### 1000-Cycle Oscillator

In balancing a bridge it is desirable to obtain a complete null balance for only by so doing can the maximum precision of balance be realized. Since the balance depends to a greater or lesser extent on the wave form of the signal source, the presence of harmonics will prevent a complete null balance.

General Radio uses a "microphone hummer" as a signal source in the GR 650-A Bridge. This is an electro-mechanical oscillator whose frequency is determined by a tuned reed. A microphone button mounted near the reed



## MEASURES QUANTITIES

with greater sensitivity & range than ever before accomplished



PATS. APP. FOR

#### TECH LAB MICROOHMMETER

... gives direct and instantaneous readings of resistance values down to 5 microhms and up to 1,000,000 megohms. Accuracy in all measurements to better than 2%. Output is sufficient to drive recorder. Entirely AC operated. Furnished in two models. Reasonably prompt deliveries. For complete data regarding other applications write for Bulletin No. 432.



Quality manufacturer's of at-tenuators and other electrical resistance instruments. For complete data write for Bulletin No. 431.



13 LINCOLN STREET  
JERSEY CITY 7, N. J.



**FOR A JOB**

*Well Done...*

THIS button, soon to be worn by thirteen million men and women—honorable discharged members of the Armed Forces of the United States—is a symbol of honor, an insignia of respect.

Wherever it is worn, it eloquently proclaims a victorious fight for Country and principles. It is indeed the chevron of service—the reward for a job done well.



**Jensen**  
SPEAKERS WITH ALNICO 5

*Specialists in Design and Manufacture of Acoustic Equipment*

JENSEN RADIO MANUFACTURING COMPANY • 6601 SOUTH LARAMIE AVENUE, CHICAGO 38, ILLINOIS



## THERMOSTATIC METAL TYPE DELAY RELAYS PROVIDE DELAYS RANGING FROM 1 TO 120 SECONDS

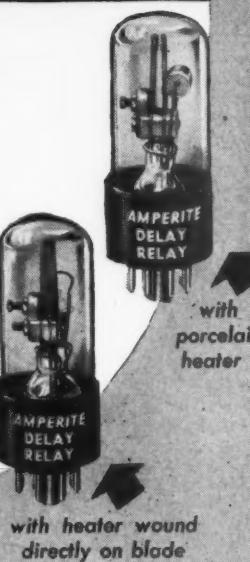
**Other important features include:**

1. Compensated for ambient temperature changes from  $-40^{\circ}$  to  $110^{\circ}\text{F}$ .
2. Contact ratings up to 115V-10a AC.
3. Hermetically sealed — not affected by altitude, moisture or other climate changes . . . Explosion-proof.
4. Octal radio base for easy replacement.
5. Compact, light, rugged, inexpensive.
6. Circuits available: SPST Normally Open; SPST Normally Closed.

**WHAT'S YOUR PROBLEM?** Send for "Special Problem Sheet" and Descriptive Bulletin.

**AMPERITE CO.** 561 BROADWAY  
NEW YORK 12, N.Y.

In Canada: Atlas Radio Corp., Ltd.  
560 King St. W., Toronto



picks up energy for continuing the oscillations.

A carefully adjusted high frequency buzzer with filtered output can also be used. The buzzer frequency can be checked with sufficient accuracy by matching it up with the second B above middle C on a correctly tuned piano.

The "hummer" or buzzer presented sound insulation problems, so a tube oscillator was employed.

The oscillator shown in the photograph is not the one now in use. This one tube oscillator was rejected for two reasons: leakage and insufficient signal after filtering. The present oscillator (Fig. 1) uses two 1S4s, triode connected, as an oscillator-amplifier. This arrangement provides sufficient gain to permit adequate filtering. The transformer  $T$  is a Stancor "Victory" Model" interstage type with the core removed, while the output transformer is a UTC S-14, the 500 ohm output going to the bridge through  $S_4$ . The entire oscillator is placed in a metal box but left floating, i.e. not grounded in any way to the bridge ground.

## METALS

[Continued from page 40]

strengthening for the chassis where large parts are mounted are also highly recommended; they permit making the chassis from a lighter gage material.

The effects of vibration can be minimized by the use of materials such as rubber, cork and even steel (springs). Rubber becomes harder as the load increases, cork becomes softer under similar conditions and steel springs deflect linearly with load.

The most promising of these appears to be rubber (for our specific applications) since it provides a fair degree of isolation under normal conditions and, when subjected to a severe shock, the deflection is not greatly magnified. In other words, it behaves somewhat like a limiter stage in an FM type receiver. Similarly, cork can be likened to a square law amplifier, while springs behave as a linear amplifier since the greater the load, the greater the deflection. Therefore large deflections must be provided for to afford protection against severe shocks.

Rubber may be used either in shear or compression (see Fig. 1) depending upon the load, required efficiency and the physical space available. It is generally used in compression (grommets) in most home radio applications since it requires little physical space. While the efficiency is not as high as rubber-in-shear it is satisfactory for most purposes.

Rubber will bulge when in compression so allowances must be made for



**For 110 volt Circuits  
or 220 if Desired**



**SOCKET AND JEWEL LIGHT ASSEMBLIES**

**DRAKE MANUFACTURING CO.**

1713 WEST HUBBARD ST., CHICAGO 22, U.S.A.

os-  
nacy  
be  
be  
by  
by  
ove  
o.  
ated  
tube  
  
oto-  
This  
two  
ignal  
ator  
con-  
This  
n to  
trans-  
"del"  
ved,  
UTC  
the  
ator  
oat-  
y to

here  
oughly  
the  
al.  
mini-  
n as  
(gs).  
in-  
mini-  
flect

ears  
licatio-  
ee of  
and,  
the  
In  
like  
iver.  
o a  
be-  
the  
de-  
ions  
otec-

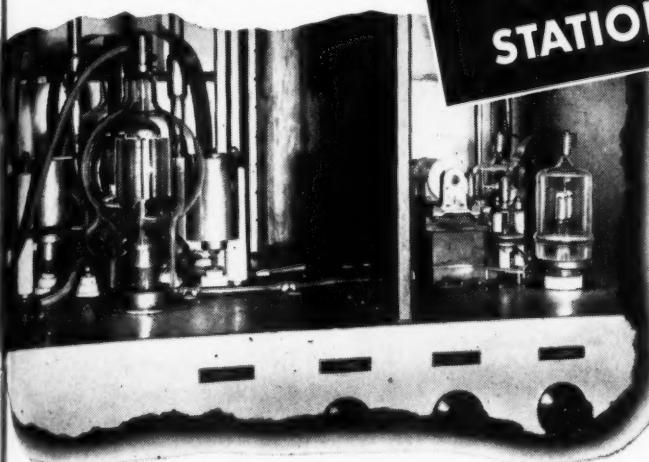
hear  
ding  
and  
gen-  
(nets)  
since  
While  
ober-  
pur-  
pres-  
for



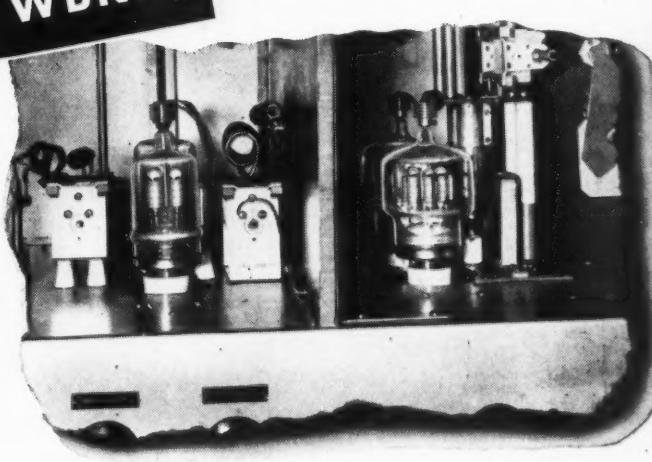
A. H. Brolly . . . Chief Engineer of Television Station WBKB, Chicago, adjusts the grid circuit of the Eimac 304-TL's in the Class B linear stage of the video transmitter.

IT'S EIMAC AGAIN!  
FIRST CHOICE FOR  
THE KEY SOCKETS  
AT TELEVISION  
STATION WBKB

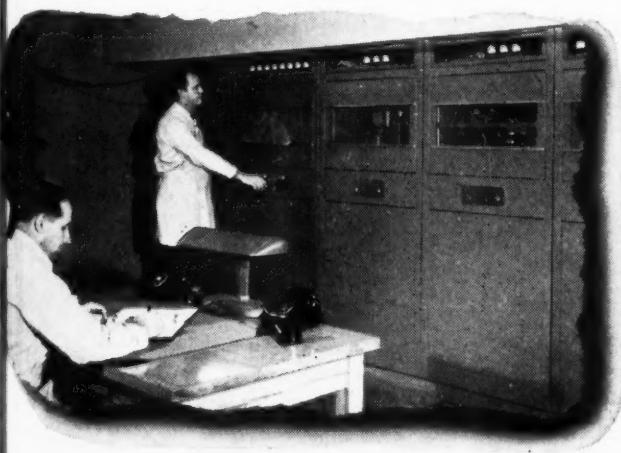
Mr. Brolly calls attention to the Eimac 1000-T's in the final stage of the Audio FM Transmitter which operates at 65.75 megacycles. It is a very stable amplifier of good efficiency.



The video transmitter operates at 61.25 megacycles; peak power output is 4 KW which provides a television service throughout metropolitan Chicago and reaches suburbs out to 35 miles or more.



Eimac 152-T's are used in the modulated stage and 304-T's in the first Class B linear amplifier of the video transmitter.



E. F. Cawthon and W. R. Brock are operating the station which has been broadcasting television programs with the present equipment since 1942 and began operation on a commercial schedule in October, 1943.

Grid modulation is employed at WBKB and a broad band of frequencies must be passed in all stages following the modulated amplifier. Multiple-tuned resistance loaded coupling circuits are used between stages.

Performance, stability, dependability are good reasons why Eimac tubes are to be found in the key sockets of the outstanding new developments in Electronics. Balaban & Katz, owners of television station WBKB of Chicago, offer potent confirmation of the fact that Eimac tubes are first choice of leading Electronic Engineers the world over.

FOLLOW THE LEADERS TO

**Eimac**  
REG. U. S. PAT. OFF.  
TUBES

EITEL-MCCULLOUGH, INC., 1032 San Mateo Ave., San Bruno, Calif.  
Plants located at: San Bruno, California and Salt Lake City, Utah  
Export Agents: Frazar & Hansen  
301 Clay Street, San Francisco 11, California, U.S.A.

**HI-Q**

## CERAMIC CAPACITORS

## WIRE WOUND RESISTORS

## CHOKE COILS

## ELECTRICAL REACTANCE CORPORATION FRANKLINVILLE, N.Y.

this in the design. This presents no problem with the use of rubber grommets since allowances must be made for clearances in assembly which ordinarily will take care of any bulge effect.

Without question, a rubber-in-shear type mounting will give the most satisfactory results, but because of the additional cost and physical space required it is very seldom used for home radio equipment. Where these factors are not too important, such as in communications equipment, the rubber-in-shear type mounting is recommended.

#### Underwriters Requirements

Certain requirements have been set down by the Underwriters Laboratories, Inc., which, when followed, make the operation of a radio appliance fairly safe from a shock or fire hazard standpoint. Since these requirements have a bearing on the mechanical design of the equipment, a brief summary of the applicable points will be given.

All live or current-carrying parts which involve shock or fire hazard, other than cords or cables shall be suitably protected. The enclosure shall be substantially constructed and in the case of metal enclosures shall be suitably corrosion resistant. Metals of at least 0.015" in thickness, asbestos of at least 1/32" or molded phenolic of 1/8" may be used for the enclosure provided the part has adequate mechanical strength.

In the case of parts conductively coupled to the power line through less than 120,000 ohms impedance, the part or parts must not be exposed within three times the minor axis of irregular holes or within three times the diameter of holes larger than 1/4". When the current exceeds 5 ma with a 1500 ohm load, parts connected to secondary circuits of over 25 volts are also considered shock hazards and must be protected with suitable barriers or enclosures.

Openings are permitted for ventilation if protected by a fine mesh metal screen. Openings may be provided for cables or other conductors if they are small in size and few in number. Circuit adjustment holes are allowable if their diameters are less than 9/32" and the adjustment screws are not more than 1/4" behind the openings. Openings may be provided for manufacturing purposes if they do not exceed 3/16" diameter or equivalent area. (Slots having a width of 1/16" or less are excepted.)

For complete information on Underwriters requirements see the latest edition of "Requirements for Power Operated Radio Receiving Appliances", published by the *Underwriters Laboratories, Inc., N.Y.*

#### Finish — Resistance to Corrosion

The specification of finish or protec-



● **Aerovox** molded in-bakelite mica capacitors are available in voltage ratings up to 10,000. Also in widest choice of mountings, terminals, meter-mounting brackets, with ceramic mounting washers, etc. Intended for heavy-duty service such as in low-power transmitters, buffer stages, laboratory assemblies, power amplifiers, continuous-service electronic equipment, etc.

Greater bulk because of augmented dielectric materials. Greater safety factor. Non-magnetic parts to reduce r.f. losses. Heavy terminals for minimum r.f. and contact resistance. 1445 and 1455 series in 1000 to 5000 v.D.C. test. Available with meter brackets (illustrated).  
1650 series in 1000 to 10,000 v. D.C. test. Slip-through holes for mounting or stacking, or with threaded holes and terminal screws. Brown bakelite standard. Al-o available in low-loss (yellow) XM bakelite.  
Units can be sealed for immersion. Also heat-treated for stability.  
10% standard tolerance, 5%, 3% or 2% on special order.

#### ● See Our Jobber . . .

Consult him regarding your capacitor requirements. Ask for latest catalog. Or write us direct.

**AEROVOX**  
*Capacitors*  
INDIVIDUALLY TESTED  
AEROVOX CORP., NEW BEDFORD, MASS., U.S.A.  
In Canada: AEROVOX CANADA LTD., HAMILTON, ONT.  
Export: 13 E. 40 St., NEW YORK 16, N.Y. Cable: ARLAB

tive coating on metal radio parts depends upon their function, what climatic conditions they must withstand, and to what degree protection from corrosion is desired.

It is practically impossible to apply a finish to a component which will withstand a severe salt spray test without some evidence of discoloration or other deleterious effects so unless these effects interfere with the actual operation of the part, either mechanically or electrically, it is common sense to tolerate them. The following discussion is based on this premise, since designers are interested in reliable operation and not theoretical considerations.

First, let us consider what constitutes corrosion. It is well known that most metals and alloys are attacked by climatic conditions, particularly when water or other aqueous solutions are present. Such corrosion, as it is called, is a result of the formation of an oxide, carbonate, sulfide or other corrosion product of the metal. Usually the newly formed product is insoluble in the environment under which it was formed and sometimes will act as a protective coating which inhibits further corrosion. Such a protective film must be very thin and complete in order to passify the metal. Should the film grow due to high temperatures and/or humidity, it is likely to crack or scale which permits further oxidation and corrosion with time. It is this protective air-formed film which accounts for the relative permanence of some metals under dry atmospheric conditions. Unfortunately these ideal conditions do not often exist and for this reason an artificial protective coating is required.

Table 2 shows most of the commonly used electroplated and chemical finishes ordinarily specified on radio equipment. The extent of protection each affords, together with recommended thickness, has been given. This table does not take into account corrosion caused by electrochemical action (galvanic corrosion).

It is this galvanic effect (similar to the generation of current in an ordinary dry cell battery) that increases the corrosive action over its normal rate. The metal which is attacked is called the anode while the metal which is "protected" is called the cathode. These in conjunction with the aqueous solution complete the galvanic couple or cell. The extent of the reaction or corrosion when the two dissimilar metals contact one another in the presence of an aqueous solution may be determined from the position of the two metals in the galvanic series and the relative areas of each metal.

For example, if stainless steel is to be in contact with aluminum or any other metal above stainless steel in the

**Toroids..**

by

**DX**

Doughnut Coils for electronic and telephone purposes. High Permeability Cores are hydrogen annealed and heat treated by a special process developed by DX engineers. Send us your "specs" today—ample production facilities for immediate delivery.

**DX RADIO PRODUCTS CO.**

GENERAL OFFICES 1200 N. CLAREMONT AVE., CHICAGO 22, ILL., U.S.A.

"the heart of a good receiver"

**RADIO** ANOTHER PUBLICATION BY THE EDITORS OF

**CQ** The Radio Amateurs' Journal

If you are or intend to be a "ham" — or if your work entails radio communications —you'll like CQ. Subscribe now!

12 issues .....	\$2.50
24 issues .....	4.00
36 issues .....	5.00

In U.S.A. & Possessions Elsewhere \$3.50 per year

(Not sold on newsstands for the duration).

**CQ-RADIO MAGAZINES, INC.**  
342 MADISON AVE., NEW YORK 17, N.Y.

Sirs: Here is my  check (or  money order) for \$..... Send me ..... issues of CQ.

Name .....  
Address .....  
City ..... State .....  
Occupation ..... Call Letters .....

electromotive series, the corrosion products formed would attack the aluminum or other metal and protect the stainless steel. Likewise, if silver or any metal more noble than the steel were to be in contact with one another the corrosion product would form on the stainless steel. This effect can be minimized by the choice of a plating which lies between the two dissimilar metals in the series. See Table 3.

In other words, any metal above another in the series will be anodic or less noble to the lower metal and the greater the separation between the metals in the series the more serious the likeli-

hood for corrosion. It should be noted that the various metals are arranged in groups within the series. Metals within the same group are relatively free from corrosion when in contact with one another, unless the areas of the two metals are substantially different. In fact, the ratio of the areas is nearly proportional to the intensity of the corrosion if the area of the more noble (cathodic) metal is much larger than that of the less noble (anodic). It is therefore wise to avoid couples wherein a metal that is low in the series (copper, for instance) has a much greater exposed area than that of a higher metal such as aluminum, because corrosion will be accelerated since the anodic metal which is always attacked is small.

The following general rules should be followed to lessen the effects of galvanic corrosion:

1. Do not join metals far apart in the galvanic series, especially with threaded fastenings. If it is necessary to use materials widely separated in the series, the joint should preferably be made by brazing, in which case the brazing material should be more noble than at least one of the materials no joined.

2. Designs should use the less noble metals for the large areas with all small fastenings of a more noble material.

3. Whenever practical insulate the dissimilar metals by coating both the anodic and cathodic elements. This increases the resistance between the couple and results in less current flow and consequently less corrosion.

Three general classes of coatings are used: metallic, inorganic, organic or combinations thereof. A metallic coating may be produced by electroplating, hot-dipping, spraying and cementation to mention a few of the more common methods. A common non-metallic protective coating is known as "anodizing" and is formed by electrolytic means on aluminum. The organic coatings are represented by the paints, enamels and lacquers.

Since fewer metals are used in fabricating radio components than there are protective coatings or finishes, only those commonly employed on the metals with which we are interested will be discussed.

#### Steel

Parts made of steel are usually electroplated with cadmium and zinc. If the surface is to be painted (no electrical contact required) zinc is ordinarily used and supplemented by a Bonderizing (phosphate) treatment. When the part requires no painting, a chromate finish, Cronak, or Iridite is sometimes applied. The chromate acts as a protection to the underlying plating and will usually withstand at least 200 hours of salt spray before any corrosion products appear. When a chromate finish is applied over cadmium or zinc the initial finish need not exceed a thickness of 0.0002". The

electrical resistance of both Cronak and Iridite is negligible.

In applications where steel is in contact with aluminum, cadmium is recommended instead of zinc. Both are anodic toward iron and steel and therefore give galvanic protection to any exposed base metal. Cadmium has a lower electromotive potential difference and will not give as much galvanic protection as zinc, although the difference is relatively small. This galvanic protection is very desirable, because small breaks in the plating caused by staking operations or scratches due to handling do not seriously impair the protective coating. A disadvantage to cadmium

TWO BOOKS EVERY ENGINEER NEEDS

**THE CATHODE RAY TUBE AT WORK**

By John F. Rider

To use the Cathode-Ray Tube to its full-est capabilities, it is necessary to understand its theory and functioning. This book explains the various types and what role each element plays.

More than half the book is devoted to the practical applications illustrated with oscillograms.

450 ILLUSTRATIONS.  
338 PAGES. \$4.00

**A-C CALCULATION CHARTS**

Faster than a slide rule. It covers all A-C calculations in series circuits, parallel circuits, series-parallel and mesh circuits, at frequencies from 10 cycles to 1000 megacycles.

146 Charts—7" x 11"  
Two colors \$7.50.

**JOHN F. RIDER Publisher, Inc.**

404 FOURTH AVENUE, NEW YORK 16, N.Y.  
EXPORT DIV. ROCKE INTERNATIONAL ELEC CORP  
13 E. 40TH STREET, NEW YORK CITY CABLE ARLAB

## OPENINGS FOR

### RADIO

### ENGINEERS

### ELECTRICAL

### ENGINEERS

### MECHANICAL

### ENGINEERS

In the development and production of all types of radio receiving and low-power transmitting tubes. Excellent post-war opportunities with an established company in a field having unlimited post-war possibilities.

Apply in person or in writing to:

Personnel Manager

**RAYTHEON  
MANUFACTURING  
CO.**

Radio Receiving Tube Div.  
55 Chapel St., Newton, Mass.

# "GREATNESS IS NOTHING BUT MANY SMALL TRIFLES"

Old Proverb

The precision required of Connecticut Telephone & Electric Division's production keeps us on our toes . . . developing new and better manufacturing methods . . . devising improved techniques of quality control. One example is the crystal tester developed by our engineers which gives us a quality check in quantity.

This is one of many special instruments in Connecticut Telephone & Electric Division's plants. Each is designed to assure our armed forces of better products. Each one contributes its trifle of greater dependability and higher accuracy to the electronic and communications equipment you will use after the war.



#### Eliminating the element of human error

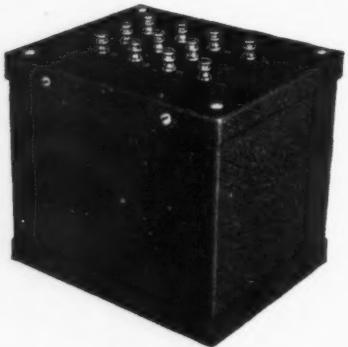
To meet modern standards of manufacturing, random spot checks are not enough. At the left is a sweep balance recorder, recently developed in our engineering department, for making 100% production tests of radio crystals. It makes a permanent and simultaneous record of frequency deviation and activity vs. temperature. It plots 71 two-curve diagrams with a total of 4,000 measurements, in less than an hour. This instrument is adaptable to diversified industrial applications which require the recording of two sets of variables.



**CONNECTICUT TELEPHONE & ELECTRIC DIVISION**  
GREAT AMERICAN INDUSTRIES, INC. • MERIDEN, CONNECTICUT



Acme electronic transformers are made-to-measure, for each application. That's why independent, unbiased tests give Acme first choice in performance. Acme engineers combine exact electrical specifications with mechanical limitations into precision-made transformers that provide for maximum performance of the electronic device.

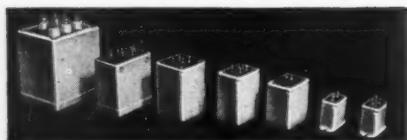


#### POWER OR FILAMENT TRANSFORMERS

Acme case designs require minimum mounting area. May be mounted on bottom, or suspended from top or side. Produced to specifications in sizes from 50 VA to 500 VA.

#### FILAMENT TRANSFORMERS

Type T-7025  
Acme Filament Transformer for 2  
—866 Rectifier Tubes. Requires minimum mounting space; mounting centers for 25 VA, only 3" x 3 1/4", height 3 3/4". Precision-made to specifications in production quantities in ratings from 25VA to 1 1/2 KVA.



#### MINIMUM WEIGHT AIR-BORNE TRANSFORMERS

Acme compound-filled, sealed case Audio, Driver, Interstage transformers, Reactors and Microphone input transformers are built to withstand and satisfactorily perform under extreme temperature variations. Bulletin 159 tells why. Write for your copy today.

**THE ACME ELECTRIC & MFG. CO.**  
55 WATER ST. CUBA, N. Y.



plating is its tendency to grow "whiskers" when in contact with phenolic materials having traces of free organic acids.

Nickel is rather unsatisfactory on steel because it is more noble and is quite porous unless a very heavy coating is applied.

#### Brass — Phosphor Bronze

These metals seldom require plating, unless sulphur or ammonia are present, the parts are to be soldered or a better electrical contact is required. Another reason for specifying plating is because both brass and phosphor bronze are negative with respect to most metals in the electromotive series. Thus, if brass or phosphor bronze are to contact cadmium plated steel for instance, severe corrosion products are likely to be formed on the latter while the brass will remain relatively clean.

Nickel is probably the most common plating used on brass, although cadmium, zinc and tin can be employed. As with steel, if the brass is to contact aluminum it is preferable to cadmium plate rather than use zinc. The plating of brass parts with cadmium must be carefully specified otherwise the plating will gradually tend to be absorbed into the brass. For this reason the plating should be over 0.0002" thick.

An exception to cadmium plating is

where phosphor bronze is used for springs. For such applications, tin is recommended.

#### Aluminum

Silver-plated parts should not be used in contact with aluminum or its alloys, depending upon the requirements at hand. Anodizing, which produces a very hard layer of aluminum oxide by electrolytic means, is extremely corrosion resistant. Its main disadvantage lies in the fact that aluminum oxide is a particularly good insulator electrically and therefore cannot be used where a good electrical contact is required.

A chemical oxide finish on the other hand does not impair the electrical conductivity of the aluminum and when properly applied will withstand over 200 hours salt spray without aluminum corrosion products being formed. Unfortunately this method does not result in a very durable finish and is easily damaged by scratching, etc. It makes an excellent base for the application of organic coatings however, and is therefore extensively used when the exterior surface is to be painted.

#### Organic Coatings

Before any of the commonly used organic coatings such as paint, enamel or lacquer can be applied to a part, the

[Continued on page 74]

## Look Here...

for Radio Parts

for specialized equipment

for Industrial and Professional Use

Transformers and other Audio Components.

Resistors, condensers and thousands of other hard-to-get

parts immediately available on priorities.

Phone, wire or write us your requirements.

Selections made and shipped same day your order is received.

## RADIO WIRE TELEVISION INC.

World's Largest Radio Supply House • Known since 1922 as reliable jobbers, wholesalers and manufacturers of radio and electronic equipment

100 SIXTH AVENUE, Dept. Q-7, NEW YORK 13  
BOSTON, MASS. • NEWARK, NEW JERSEY

ORIGINATORS AND PEACETIME MARKETERS OF THE CELEBRATED

Lafayette Radio

## BIBLIOGRAPHY

[Continued from page 53]

—*Proc. IRE*, Vol. 23, No. 2, February, 1935, p. 112.

Effect of Space Charge and Transit Time on the Shot Noise of Diodes—A. J. Rock—*Bell Sys. Tech. Jour.*, Vol. 17, pp. 592-619; October, 1938.

Sectionalized Magnetron—K. Owaki and T. Suzuki—*Electrotech. Jour.* (Japan), Vol. 2, pp. 257-260, November 1938.

On the New Vacuum Tubes Sentron for Ultra-Short Waves—S. Uda, H. Ultida, and H. Sekimoto—*Nippon Elec. Comm. Eng.*, pp. 171-177; April, 1938.

Ultra-High-Frequency Oscillations Obtained by Sentron Tubes—*Electrotech. Jour.* (Japan), Vol. 2, pp. 266-267; November, 1938.

Production of Large Power at Decimeter Wavelengths—H. Gutton and S. Berlin—*Jour. de Phys. et le Radium*, Vol. 9 supplement, pp. 10-11; January, 1938.

Electron Transit Time Effects in Multi-grid Valves—M. J. O. Strutt—*Wireless Eng.*, Vol. 15, pp. 315-321; June, 1938.

Phase Focusing of Electrons in Rapidly Fluctuating Electric Fields—E. Pruche and A. Rechnagel—*Zeit für Phys.*, Vol. 108, Nos. 7-8, pp. 459-482; 1938.

The Resotank, a New Generator for Microwaves—A. Allerding, W. Dallenbach, and W. Kleinsteuber—*Hochfrequenz und Elektroakustik*, Vol. 51, pp. 96-99, March, 1938.

An Oscillator for Ultra-High Frequencies—W. L. Barrow—*Rev. Sci. Instr.*, Vol. 9, pp. 170-174; June, 1938.

Theory of the Klystron—V. Guljaev—*Jour. Phys.* (U.S.S.R.), Vol. 4, No. 1-2, pp. 143-146; 1941.

Zur Theorie der Trifrohren (On the theory of drift Tubes)—H. E. Hollmann and A. Thoma—*Hochfrequenz und Elektroakustik*, Vol. 56, pp. 181-186; December, 1940.

Geschwindigkeitsgesteuerte Laufzeitrohren. Beitrag zur Theorie (Velocity-Controlled Transit-Time Tubes. Contribution to their theory)—B. Kockel—*Zeit. für Tech. Phys.*, Vol. 22, No. 2, pp. 77-85; 1941.

Velocity Modulation. Results of Further Considerations—R. Komppner—*Wireless Eng.*, Vol. 17, pp. 478-488; November, 1940.

Über Einen Neuartigen Ultrakurzwellen-generator mit Phasenfocussierung (On a new type of ultra-short-wave generator with phase focusing) — F. Ludi—*Helv. Phys. Acta*, Vol. 13, No. 6, pp. 498-522; 1940.



## SLIDE RULE or SCREWDRIVER ... which will YOU be using 2 years from now!

Add CREI technical training to your present experience—then get that better radio job you want—make more money—enjoy security

Thousands of new men have joined the ranks of the radio industry during the war. But now, and after final peace, even more thousands will return from the armed forces. War production will settle down to supplying civilian needs. Where will you fit into this picture?

If you are wise, you will look ahead and prepare for the good-paying jobs in radio-electronics and industrial electronics. Every man in radio today has the opportunity to see the amazing developments that are taking place, as well as the unlimited opportunities available to men with modern technical training.

It is up to you to decide if you will be a "screwdriver" mechanic or a real technician in a responsible engineering position.

CREI can help you prepare by providing you with a proved program of home study training that will increase your technical ability and equip you to advance to the better-paying radio jobs that offer security and opportunity. The facts about CREI and what it can do for you are printed in a 36-page booklet. It is well worth your reading. Send for it today.



WRITE FOR  
FREE 36-PAGE  
BOOKLET

"Your Opportunity in the New World of Electronics"

If you have had professional or amateur radio experience and want to make more money, let us prove to you we have something you need to qualify for a better radio job. To help us intelligently answer your inquiry—  
PLEASE STATE  
BRIEFLY YOUR  
BACKGROUND OF  
EXPERIENCE, EDUCATION AND  
PRESENT POSITION.

## CAPITAL RADIO ENGINEERING INSTITUTE

Home Study Courses in Practical Radio-Electronics  
Engineering for Professional Self-Improvement

Dept. RA-7, 3224 - 16th Street, N. W., Washington 10, D. C.

Contractors to U. S. Navy—U. S. Coast Guard—Canadian Broadcasting Corp.  
Producers of Well-trained Technical Radiomen for Industry.

## METALS

[Continued from page 72]

surface of the part must be suitably prepared. This is particularly true where the surface to be coated has a tendency to oxidize. The preparation of the surface should result in a fine etch which allows the organic coating to obtain a "grip" on the surface. Several methods for readying the surface are used, such as Bonderite for zinc, Parkerize or Bonderize for steel, Lithoform on hot galvanized parts and chemical oxide chromodizing or phosphatizing on aluminum.



### Great Time Saver

Burstein-Applebee of Kansas City offers you this great convenience FREE. Easy to work. Solves many problems in a jiffy. FREE to Radio men, electronic engineers and others in the business. Attach coupon to your letterhead.

### MAIL COUPON NOW



BURSTEIN-APPLEBEE CO.  
1012 McGEE ST.  
KANSAS CITY 6, MO.

Send me FREE Color Code and Ohms Law Calculator along with latest catalog.

I am

STATE CONNECTION IN INDUSTRY

NAME

ADDRESS

TOWN

STATE

## Conclusion

The finishing of metal is a very exacting procedure and it is not the intention of this article to present a detailed description of the process. It is hoped however that the above will provide sufficient information for the radio engineer to fulfill his requirements.

## Bibliography

- Properties of Metals and Alloys—Mott & Jones—Oxford 1936.
- Properties of Some Metals and Alloys—International Nickel Company, N.Y.C.
- Modern Uses of Non-ferrous Metals—Gann—American Institute of Mechanical Engineers Publication—N. Y.
- Metals Handbook—American Society for Metals—Cleveland, O.
- SAE Handbook—Society Automotive Engineers, Inc., N.Y.C.
- Mechanical Engineers' Handbook—Kent—John Wiley & Sons, N. Y.
- Protective Coatings for Metals—Burns and Schuh—Reinhold Publishing Corporation, New York.

## OSCILLATORS

[Continued from page 35]

This eliminates the fuzzy figures due to noise and the combined 440 and 4000-cycle frequencies when the receiver output is viewed directly. The 440 cycle and the 4000 cycle signals can be separated by a simple filter arrangement as shown in Fig. 8. Separation of these frequencies can also be partially accomplished by tuning, when the receiver is tuned to the carrier frequency the 400 cycles predominates, if tuned "off center" the 4000 cycles can be made to predominate.

If necessary a complete calibration can be made from the 60 cycle power line as standard. This can be used to synchronize the oscilloscope sweep circuit with the unknown frequency on the vertical plates. The author finds the resulting figure less confusing than the regular Lissajou patterns. The ratio of the unknown frequency to the 60 cycle sweep equals the ratio of the number of "peaks" to number of "tails" as shown in Fig. 9, which shows the figure for

90 cycles, or 3/2 of 60. Fig. 10 shows a table of ratios and corresponding frequencies covering points on two ranges 60-210 and 200-700. In observing the

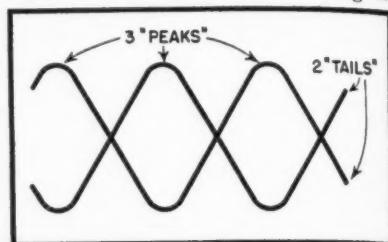


Fig. 9. Oscilloscope figure with the horizontal sweep at 60 cycles and an oscillator frequency equal to 3/2 of 60, or 90, on the vertical plates

higher ratios it is difficult to count the "peaks" and this need not be done if the "tails" are counted; the number of peaks can be deduced from the position of the dial, which will have already been marked for the major points indicated by the lower ratios as shown in the second and sixth columns of the table. Of course if difficulty is experienced

## ENGINEERS WANTED

Here's an opportunity to join one of America's largest manufacturers of electronic and communications equipment.

**Radio**  
**\*Electrical**  
**Electronic**  
**Industrial**  
(Job evaluation)  
**\*Mechanical**  
**\*Factory Planning**  
**Materials Handling**  
**Manufacturing Planning**

Work in connection with the manufacture of a wide variety of new and advanced types of communications equipment and special electronic products.

Write giving full qualifications,  
or apply to:

R. L. D., EMPLOYMENT DEPT.

**Western Electric Co.**

100 CENTRAL AV. KEARNY, N. J.

\*Also: C. A. L.

Locust St. Haverhill, Mass.

Applicants must comply with WMC regulations

**SYNONYMOUS THOUGHTS:  
THORDARSON and TRANSFORMERS**

**TO SUPPLY  
EVERY KNOWN  
NEED!**

**Transformer Specialists Since 1895  
... ORIGINATORS OF TRU-FIDELITY AMPLIFIERS**

**THORDARSON**

TRANSFORMER DIVISION  
THORDARSON ELECTRIC MFG. CO.  
500 WEST MURON STREET, CHICAGO, ILL.

**• Ted McElroy**

World's Largest Manufacturer of  
Wireless Telegraphic Apparatus

COMPLETE CENTRAL OFFICE EQUIPMENT

**McElroy Manufacturing Corp.**  
82 Brookline Avenue • Boston, Massachusetts

with the higher ratios, intermediate points can be interpolated fairly accurately with draftsman's dividers.

If other ranges do not quite conform to the calibration of the above two ranges, corrections can be made by varying the resistors  $R_{1-8}$  slightly by means of shunts of high resistance or low series resistances. The slight changes necessary to correct the scale extremities do not upset the rest of the scale appreciably and it is generally not necessary also to adjust resistors  $R_{11-18}$ .

FREQ.	RATIOS	FREQ.	RATIOS
60	1	—	—
65	—	13/12	220
70	7/6	—	230
75	—	15/12	240
80	4/3	—	250
85	—	17/12	260
90	3/2	—	280
95	—	19/12	290
100	5/3	—	300
105	—	21/12	320
110	11/6	—	340
115	—	23/12	360
120	2	—	380
125	—	25/12	400
130	—	13/6	420
135	—	27/12	440
140	7/3	—	460
145	—	29/12	480
150	5/2	—	500
155	—	31/12	520
160	8/3	—	540
165	—	33/12	560
170	—	17/6	580
175	—	35/12	600
180	3	—	620
185	—	37/12	640
190	—	19/6	660
195	—	39/12	680
200	10/3	—	700
210	—	21/6	720

Fig. 10. Table of oscilloscope figures for frequencies calibrated against 60 cycles. Ratios shown are for vertical peaks to horizontal tails (or horizontal peaks for Lissajou figures)—see Fig. 9

except perhaps on the highest frequency range. The highest frequency range does not readily conform to the scale for the other ranges and it is generally necessary to use a table of correction for this range.

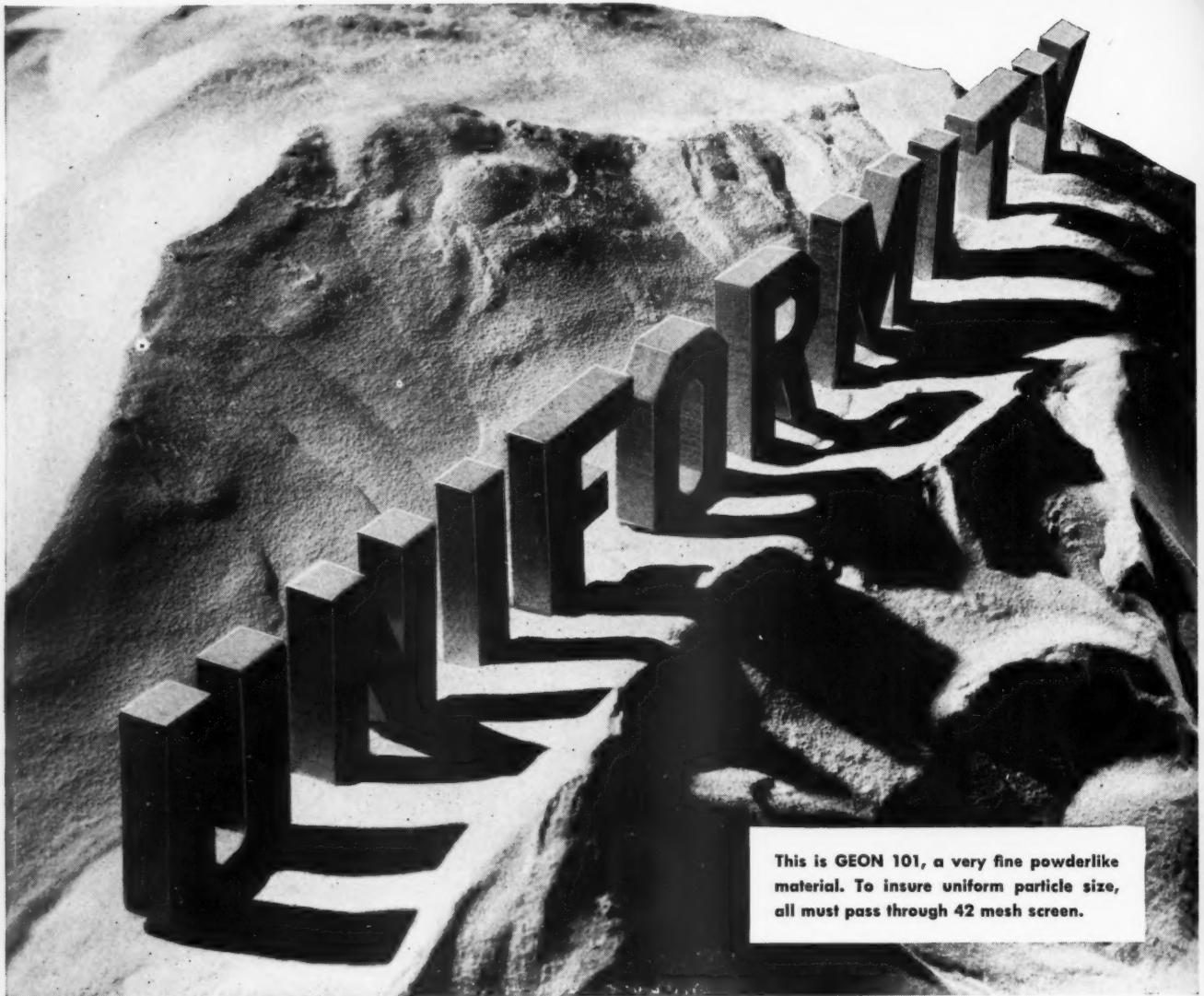
The terminal marked 60 cycles is a convenient source of voltage for spot checking calibration at any time. By connecting a low voltage a-c voltmeter between this terminal and the output (set at "Lo") "beats" can be observed when the oscillator is set close to the principal harmonics and sub-harmonics of 60 cycles. These two terminals can also be connected in parallel for the observation of beats on a vacuum tube voltmeter or other grounded indicator.

#### References:

- <sup>1</sup>The Improved Wide Range Audio Oscillator, Ray L. Dawley, RADIO, December, 1940
- <sup>2</sup>Geometric Solutions for Resonant Impedance-Transforming Networks, Robert C. Paine, RADIO, October, 1943
- Some Graphic Solutions of Parallel Circuits, Robert C. Paine, Electronics, December, 1942

## ADVERTISING INDEX

ADVERTISER	PRODUCT	PAGE
Acme Elec. & Mfg. Co. ....	Transformers .....	72
Aerovox Corporation ....	Capacitors .....	68
Albion Coil Company ....	Coils .....	22
Allied Radio Company ....	Electronic Equipment .....	25
Altec-Lansing Corporation ....	Loudspeakers .....	26
American Phenolic Corporation ....	Plugs, Cables, Connectors, Sockets .....	5
Amperite Co. ....	Relays .....	66
Arnold Engineering Co. ....	Engineering Equipment .....	20
Bell Telephone Labs. ....	Institutional .....	27
Biley Electric Co. ....	Quartz Crystals .....	2
Bridgeport Mfg. Company ....	Coils .....	61
Burstein-Applebee Co. ....	Electronic Equipment .....	74
Cambridge Thermionic Corp. ....	Terminal Lugs .....	Cover 3
Capitol Radio Engineering Inst. ....	Educational .....	73
Concord Radio Corporation ....	Electronic Equipment .....	31
Conn. Tel. & Elec. Div. ....	Electronic Equipment .....	71
Drake Mfg. Co. ....	Neon Light Assemblies .....	66
D-X Radio Products Co. ....	Coils .....	69
Etel-McCullough, Inc. ....	Tubes .....	67
Electrical Reactance Corp. ....	Capacitors .....	68
Electronic Mechanics, Inc. ....	Insulation Materials .....	1
Federal Tel. & Radio Corp. ....	Cable, Wire .....	8, 16
Formica Insulation Co., The ....	Laminated Plastics .....	9
Foster Co., A. P. ....	Transformers .....	28
Goodrich Co., The B. F. ....	Insulation Material .....	76
Guardian Electric Co. ....	Relays .....	21
Hallcrafters Co., The ....	Communications Equipment .....	59
Harvey Radio Co. ....	Radio & Electronic Equip. ....	62
Heintz & Kaufman Ltd. ....	Transmitting Tubes .....	10
Hytron Corporation ....	Tubes .....	24
International Resistance Co. ....	Resistors .....	14
Jefferson Electric Co. ....	Transformers .....	4
Jensen Radio Mfg. Co. ....	Acoustic Equipment .....	65
Johnson Co., E. F. ....	Transmitter Components .....	11
Kaar Engineering Co. ....	FM Apparatus .....	17
Kyle Corp. ....	Transformers .....	Cover 2
Link, Fred M. ....	FM Apparatus .....	Cover 4
McElroy Mfg. Co. ....	Wireless Tel. Apparatus .....	74
Mycalex Corp. of America ....	Insulating Materials .....	32
National Union Radio Corp. ....	Electronic Tubes .....	29
Racon Electric Co. ....	Speakers .....	63
Radex Corporation ....	Small Motors .....	64
Radiart Corp. ....	Vibrators .....	13
Radio Wire Television ....	Electronic Equipment .....	72
Raytheon Manufacturing Corp. ....	Tubes .....	19, 70
Rider, John F. Publ. Inc. ....	Technical Books .....	70
Russell Electric Co. ....	Record Changers, Motors, Drives .....	15, 18, 23
Sprague Electric Co. ....	Resistors .....	12
Surprenant Elec'l Insulation Co. ....	Plastic Insulations .....	60
Sylvania Electric Products Co. ....	Tubes .....	7
Tech Laboratories ....	Attenuators .....	64
Thordarson Elec. Mfg. Co. ....	Transformers .....	74
Triplette Elec. Instru. Co. ....	Portable Instruments .....	60
Turner Co., The ....	Microphones .....	30
Valpey Crystal Corp. ....	Quartz Crystals .....	62
Western Electric Co. ....	Help Wanted .....	74
Wrigley Jr., Co., Wm. ....	Institutional .....	58



This is GEON 101, a very fine powderlike material. To insure uniform particle size, all must pass through 42 mesh screen.

## An important advantage offered by GEON polyvinyl resins for electric wire and cable insulation

NEW users of GEON polyvinyl materials are invariably delighted to discover that these resins provide definite processing advantages resulting directly from the *uniformity* of the raw material. This basic uniformity means that foot after foot, mile after mile of wire insulation made from GEON will be of continuous high quality.

With GEON resins it isn't necessary to mix several batches together in an effort to get uniformity in the base material. Nor is there any need to adjust processing machinery frequently to compensate for batch-to-batch variations of the plasticized product. The formula used yesterday with one batch of GEON can be used today and tomorrow with new batches. And the finished insulation will be uniform—electrical and all other properties always the same. That means satisfied customers, fewer rejects.

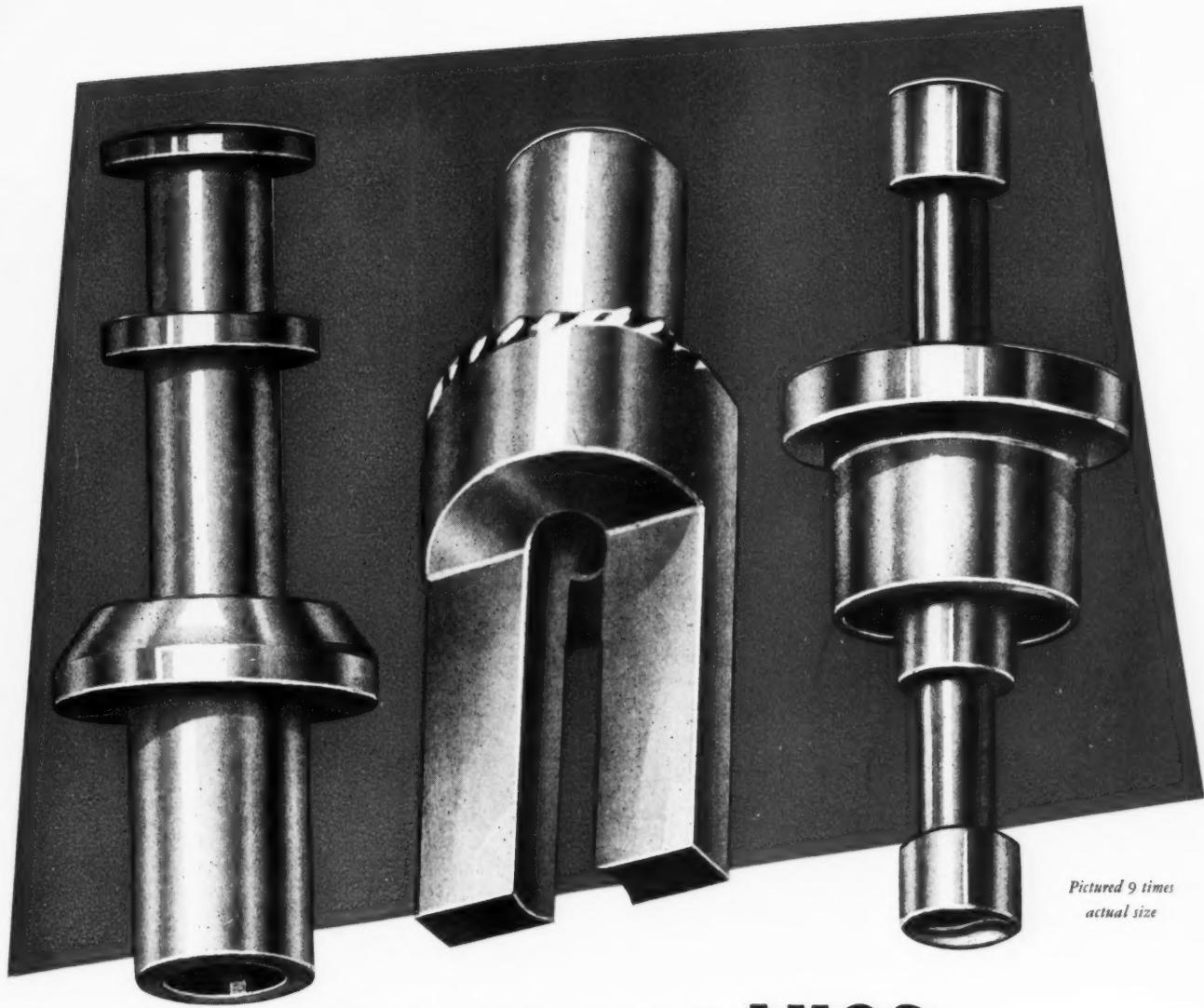
All this is true because manufacturing methods for GEON result in a material that is *uniform*—batch after batch after batch are all alike within close tolerances controlled by rigid specifications. For example, specific viscosity limits for GEON 101 are .52—.57. To control particle size, 100% must pass through 42 mesh screen.

Another important advantage of GEON is that the right *combination* of properties for your insulating material can be selected to meet the specific conditions of end use. These properties include resistance to water, heat, cold, aging, wear, abrasion, sunlight, chemicals, and many other normally destructive factors. For more information write Department WW-7, B. F. Goodrich Chemical Company, Rose Building, Cleveland 15, Ohio.



## B. F. Goodrich Chemical Company

A DIVISION OF  
THE B. F. GOODRICH COMPANY



Pictured 9 times  
actual size

## MEET THREE "BIG" LUGS

Reading from left to right they are C.T.C.'s Turret Terminal Lug, C.T.C.'s Split Terminal Lug and C.T.C.'s Double End Terminal Lug and we're willing to wager that once you've made their acquaintance you'll be very glad you've joined their ever-widening circle of friends who find in them a better, faster, more economical way to get firm, quick soldering terminal posts.

*C.T.C. TURRET TERMINAL LUGS* are firmly anchored to terminal boards by a

simple swaging operation. Two soldering spaces permit two or more connections without superimposing wires — insure good contact, neat appearance. Made of brass, heavily silver plated, to fit  $1/32"$ ,  $2/32"$ ,  $3/32"$ ,  $4/32"$ ,  $6/32"$  and  $8/32"$  terminal board thicknesses.

*C.T.C. SPLIT TERMINAL LUGS* have a  $.050"$  hole through their shaft which makes them ideal for use on transformers or other potted units that require soldering after potting and on terminal boards

that should be wired from top or bottom side of board without drilling. Made of heavily silver plated brass to fit  $3/32"$  terminal boards.

*C.T.C. DOUBLE END TERMINAL LUGS* provide twin terminal posts in one simple swaging operation. They may be wired from top or bottom and electrical connection is perfect because both posts are part of the same lug. Stocked in  $3/32"$  terminal board thicknesses.



### THE NEW C.T.C. CATALOG

**NO. 100** contains complete information on C.T.C. LUGS, *All-Set* TERMINAL BOARDS, SWAGING TOOLS, X-RAY ORIENTED CRYSTALS and I-F TRANSFORMERS. Get your free copy.



**CAMBRIDGE THERMIONIC CORPORATION**

454 Concord Avenue

• Cambridge 38, Mass.

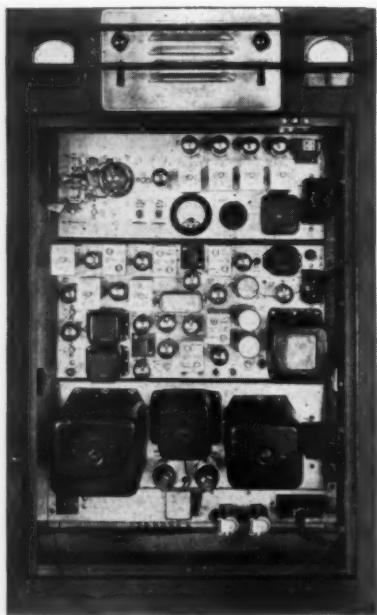
# Link IS FIRST AGAIN

With time tested and proved FM Radio Communication Units for the NEWLY ASSIGNED



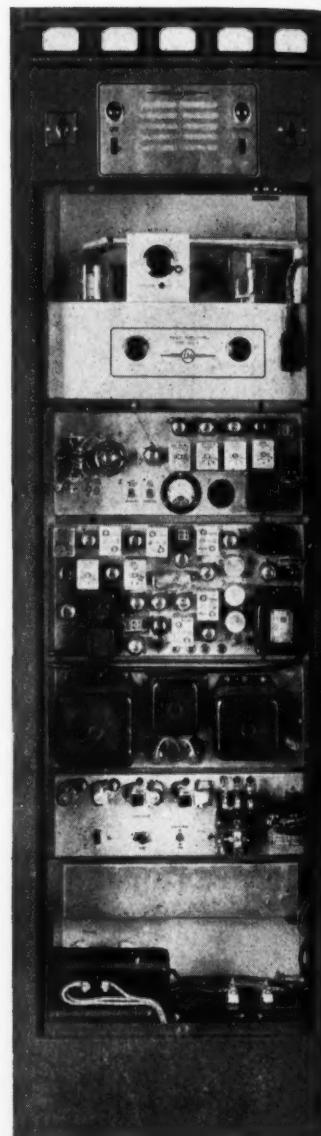
72-76 mc BAND

LINK TYPE 1498



More than 3000 Link designed and built units for use in this range have been in routine operation for 3 years.

LINK TYPE 1505



## RELAY, REPEATER AND MAIN STATION EQUIPMENT

250 Watt — Type 1505

50 Watt — Type 1498

Remote Control — Type 1504

## MOBILE EQUIPMENT

Transmitter-Receiver

Type vhf FMTR

LINK TYPE vhf FMTR



SPECIFY LINK AND OBTAIN THE FINEST FOR YOUR COMMUNITY

ENGINEER • MANUFACTURER

# Fred M. Link

125 WEST 17th STREET

NEW YORK 11, N. Y.

PREFERRED FM RADIO  
COMMUNICATION EQUIPMENT

MANUFACTURED UNDER LICENSE OF THE  
ARMSTRONG PHASE SHIFT MODULATION PATENTS